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TRACK PARAMETER EXTRACTION USING MULTIPATH DELAY AND
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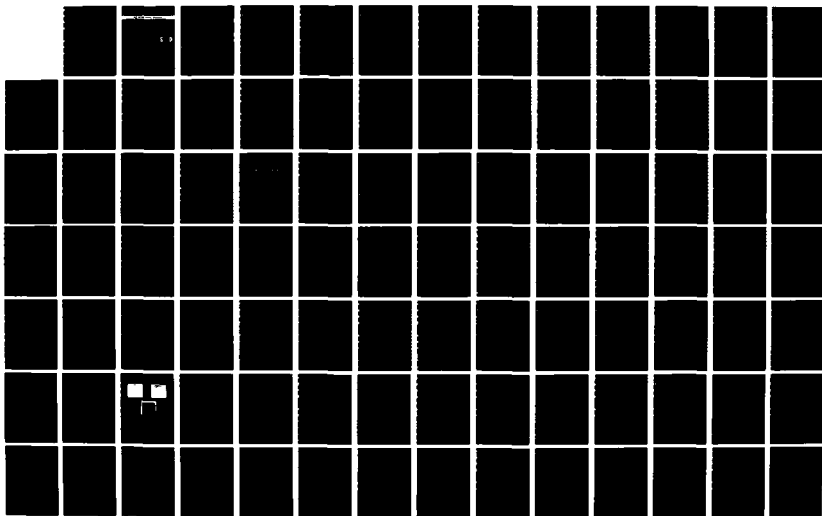
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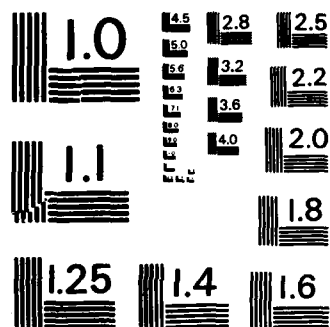
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AD-A166 044

TRACK PARAMETER EXTRACTION USING MULTIPATH DELAY
AND DOPPLER INFORMATION

FINAL REPORT 5517

Contract No. N00014-84-C-0408

FEBRUARY 1986

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DISTRIBUTION STATEMENT A

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SUMMARY

This final report summarizes the work performed under contract No. N00014-84-C-0408 to Office of Naval Research and is accompanied by the software listings of the developed code.

The goal of the multipath project is to develop techniques to make use of the multipath reflections of acoustic signals travelling in the ocean to localize and track radiating sources. There have been two main areas of study under this contract. First area concentrates on the detection and estimation of the multipath (or differential) delays in the received signals; the second is the development of localization and tracking algorithms.

Previous work on the multipath project included the development of differential delay estimation algorithms as well as theoretical studies resulting in bounds on the variance of estimating multipath delay. Bounds were also placed on the accuracy of estimating various so-called track parameters -- speed, depth, and range at closest approach of the target to the sensor array.

Under the present contract, software was developed to estimate multipath delay using real or simulated data as input. Also under the present contract, tracking algorithms were developed. More specifically the following are accomplishments of this phase.

1. A real data processing system was developed for the purpose of estimating multipath delay as a function of time. This system was composed of a correlogram generator and a line tracker. A correlogram is a picture whose rows consist of normalized correlation functions at different time instances. The correlation functions peak at the value of the differential delay and align to form tracks in the correlogram. The line tracker pulls the differential delay curves out of the correlogram. The correlogram generator produces SCOT, ML-, PHAT- and un-normalized correlograms. The line tracker uses the ADEC line tracking algorithm. This software was developed on the AP120B array processor on VAX 11/780 for high speed

computation.

2. Two types of track parameter estimation methods were developed. The first makes use of the measured value and functional form of the delay curve at various points in time. The other fits an estimated delay curve to the measured delay curve, and estimates the track parameters as those giving the best fit to the data. Target is assumed to travel along a constant-depth, constant-velocity straight-line course, and the parameters of the target's path -- depth, velocity, and closest point of approach -- are estimated, thereby localizing the target. The tracking algorithms were implemented in FORTRAN 77 and evaluated using the real data provided by ONR. The results are encouraging in that these methods allow tracking of real underwater targets.

TRACK PARAMETER EXTRACTION USING MULTIPATH DELAY AND DOPPLER INFORMATION

0. INTRODUCTION

Acoustic waves propagating in the ocean undergo various reflections and refractions [1]. Because of this multipath propagation, acoustic surveillance systems receive several different delayed and doppler shifted versions of the source's signal. The relative delays and doppler shifts contain valuable information which can help localize and track a target [2]. Consider, for example, a single multipath reflection depicted in Figure 0.1. The time delay between the signals propagating in the direct and reflected paths is a function of the target/sensor range and target and sensor depths. Similarly, the doppler shifts of the direct and multipath signals are functions of the velocity and range of the target. Therefore, a history of the delay and doppler shifts can lead to knowledge of the so-called track parameters -- speed, range of closest approach, and depth.

In this report, techniques for extracting track parameters from delay and doppler information are presented. Bounds are placed on the accuracy of these estimates as well as the accuracy of the delay and doppler measurements. Cases with one target, one and two sensors with and without multipath are treated in detail.

The structure of this report is as follows: Chapter one details the geometry and signal equations for a single sensor and target. This chapter also discusses the measurement of the delay and doppler shifts from the raw data. Chapter two presents the delay and doppler formulas for a single sensor and single target in the presence of a surface reflection. The accuracy of track parameter estimators using delay and doppler information is also discussed in Chapter two. Chapters three and four develop methods for extracting the track parameters from delay and doppler information for several sensor geometries; and chapter five contains some concluding remarks.

There are four appendices: appendix one discusses the effect

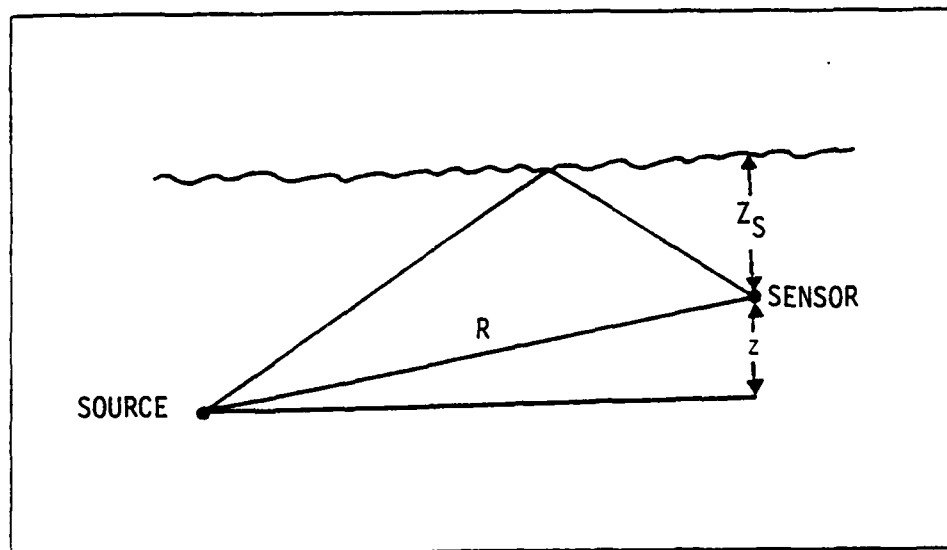


Figure 0.1 Illustration of multipath due to a surface bounce for the case of a single source and sensor. $D = (1/C) [(R^2 + 4z_s^2 + 4z_s z)^{1/2} - R] =$ multipath delay. C is the velocity of sound in water.

differential doppler has on the measurement of differential delay. Appendix two presents an example of track parameter estimators applied to a real data set. Appendix three discusses the accuracy of depth estimation using multipath delay. Finally, appendix four contains software listings.

1. MULTIPATH PARAMETERS FROM RAW DATA

In this chapter, the extraction of delay and doppler information from raw data is discussed. We consider here the case of a single multipath reflection (Fig. 1.1). The signal at the sensor will be roughly given by

$$y(t) = x(\alpha_d(t) \cdot t - D_d(t)) + g(t)x(\alpha_m(t) \cdot t - D_m(t)) + e(t) \quad (1.1)$$

where

$y(t)$ is the signal at the sensor

$\alpha_d(t)$ is the doppler shift in the direct signal

$\alpha_m(t)$ is the doppler shift in the multipath signal

$D_d(t)$ is the delay in the direct signal

$D_m(t)$ is the delay in the multipath signal

$g(t)$ is the gain of the reflected signal

$e(t)$ is the sensor noise

$x(t)$ is the target signal

It is assumed that e is uncorrelated with x ; the doppler shifts are small:

$\alpha_d, \alpha_m \sim 1$; and the delays, doppler shifts and gains are slowly changing with time: $|\frac{\partial D}{\partial t}|, |\frac{\partial \alpha}{\partial t}|, |\frac{\partial g}{\partial t}| \ll 1$; and $0 < |g| < 1$.

1.1 DELAY

Assuming $\alpha_d = \alpha_m = 1$, the Cramer-Rao lower bound on the variance of the minimum variance estimator of the differential delay, $D = |D_d - D_m|$, is reasonably small for signals with a large bandwidth-delay product [3]. When x

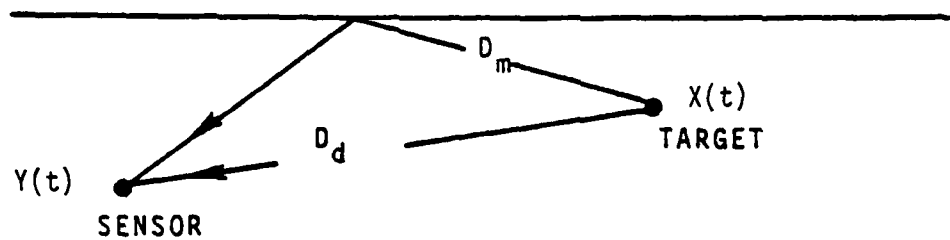


Figure 1.1 The received sensor signal in the presence of a multipath reflection.

and e are uncorrelated lowpass white noise processes with bandwidth w , the variance in estimating D from the signal $y(t) = x(t) + g \cdot x(t-D) + e(t)$ is bounded by,

$$\text{Var}(D) > \frac{3\pi}{Tw^3g^2} \frac{1}{\text{SNR}^2}, \quad \text{SNR} \ll 1, \text{WD} \gg 1 \quad (1.2a)$$

$$\text{VAR}(D) > \frac{3\pi}{w^3g^2}(1-g^2), \quad \text{SNR} \gg 1, \text{WD} \gg 1 \quad (1.2b)$$

where the signal-to-noise ratio (SNR) is the ratio of the power contained in the signal and noise. The maximum likelihood (ML) estimator achieves this bound, but involves a computationally intensive minimization of a complicated cost function [2].

Maximizing a simplified version of the ML cost function results in the autocorrelation method of multipath delay estimation: the delay is chosen as the value of τ which maximizes $|R_{YY}(\tau)|$, the absolute value of the autocorrelation function [2]. The autocorrelation function is relatively easy to compute, and is commonly used for delay estimation [4].

The variance and bias in estimating delay using the autocorrelation method based on data over a time period, T are given in [2] by

$$\text{Var}\{D^*\} = - \frac{3\pi}{Tw^3g^2} \left(\frac{1}{\text{SNR}}\right)^2, \quad \text{SNR} \ll 1, \text{WD} \gg 1 \quad (1.3a)$$

$$\text{BIAS} = < \frac{3}{w^2D} \sqrt{\frac{1}{4} + \left(\frac{1}{g} + g + \frac{S_e}{gS_x}\right)^2} \quad (1.3b)$$

Note that for low SNR, the ML estimator and the autocorrelation estimator have essentially the same variance. Therefore, for sufficiently large bandwidth, low SNR signals, as is usually the case in underwater acoustic surveillance, the correlation estimator will perform almost optimally.

Tracking Differential Delay D(t)

For $\dot{D}(t) \ll 1$, and $\alpha_m = \alpha_d = 1$, the autocorrelation function and power spectrum of $y(t)$ are given by

$$R_{YY}(\tau) = (1+g^2)R_{XX}(\tau) + gR_{XX}(\tau-D) + gR_{XX}(\tau+D) + R_{ee}(\tau) \quad (1.4a)$$

$$S_{YY}(\omega) = (1 + g^2 + 2g\cos\omega D)S_{XX}(\omega) + S_{ee}(\omega) \quad (1.4b)$$

From (1.4), it is easily seen that when the width of $R_{XX}(\tau) \ll 1$, peaks of $R_{YY}(\tau)$ will occur at the value of the multipath delay as well as at zero delay.

When the SNR is low, and $D(t)$ is slowly changing with time, $D(t)$ is most often found using a correlogram -- a 2-D gray level image whose i -th row is the correlation function taken at t_i , $E(Y(t_i)Y(t_i+\tau))$. See Figure A3.1 for example. Peaks in the correlation functions comprising a correlogram will merge to form lines tracing the history of $D(t)$.

Doppler Effects

Since the direct and multipath signals are arriving from different directions, a moving target will cause a relative doppler shift between the two signals. The autocorrelation of the sensor signal will become

$$\begin{aligned} R_{YY}(t, \tau) = & R_{XX}[(t-\tau)\alpha_d] + g^2 R_{XX}[(t-\tau)\alpha_m] \\ & + gR_{XX}[\alpha_d t, \alpha_m \tau - D] + gR_{XX}[\alpha_d t, \alpha_m \tau + D] + R_{ee}(t-\tau) \end{aligned} \quad (1.5)$$

where

$$R_{XX}[a, b] = E[X(a)X(b)] , \text{ and } R_{XX}[\tau] = E[X(t)X(t+\tau)]$$

As shown in Appendix 1, the secondary peaks in $R_{YY}(\tau)$ which are used to estimate the delay are reduced as the differential doppler, $\alpha_d - \alpha_m$, increases. That is, the direct and multipath signals become decorrelated as a

result of target motion.

The differential doppler is greatest when the difference in the directions of arrival of the direct and multipath signals is greatest. This occurs at CPA, the point of closest approach of the target to the sensor array. The fading of the correlogram lines near CPA in Figure A2.1 is in part due to this differential doppler effect.

1.2 DOPPLER

Assuming $D_d = D_m = 0$, substituting $t' = \log t$ into (1.1) gives

$$Y(t') = X(t' + \log \alpha_d) + X(t' + \log \alpha_m) + e(t') \quad (1.6)$$

Note that since $e(t)$ is white gaussian noise, so is $e(t')$. Therefore, estimating differential doppler in the absence of delay is equivalent to estimating differential delay in the absence of doppler.

The ML estimator of doppler shift achieves the C-R bound of

$$\text{Var}(\log \frac{\alpha_d}{\alpha_m}) = \frac{3\pi}{W' 3g^2} \frac{1}{\text{SNR}^2}, \quad \text{SNR} \ll 1 \quad (1.7a)$$

$$\text{Var}(\log \frac{\alpha_d}{\alpha_m}) = \frac{3\pi}{W' 3g^2} (1-g^2), \quad \text{SNR} \gg 1 \quad (1.7b)$$

where W' is the bandwidth of the log sampled signal, $X(t')$. The autocorrelation method of determining differential delay estimation, looking for the peak of $E(Y(t')Y(t'+\log \alpha))$, i.e., the peak of $E(Y(t)Y(\alpha t))$, has variance

$$\text{Var}(\log \alpha) = \frac{3\pi}{W' 3g_0^2} \frac{1}{\text{SNR}^2}, \quad \text{SNR} \ll 1 \quad (1.8)$$

where it is assumed that $\log \alpha \cdot W' \ll 1$.

Tracking $\alpha(t)$

The doppler ratio, $\alpha = \frac{\alpha_m}{\alpha_d}$ is often seen using dopplergram. Analogous

to a correlogram, a dopplergram is a 2-D image whose i -th row is $E(Y(t_i)Y(\alpha t_i))$. Lines in the dopplergram show the time history of $\alpha(t)$.

Delay Effects

As differential doppler decorrelated the multipath and direct linearly sampled signals, differential delay will decorrelate the multipath and direct log sampled signals:

$$E[Y(t)Y(\alpha^* t - D)] = g_{XX}(D) < g_{XX}(0) \quad (1.9)$$

where α^* is the correct value of the doppler ratio. Differential delay is greatest at CPA. Consequently, one would expect fading of differential doppler lines around CPA.

Absolute Doppler

As a final note, absolute doppler information can be obtained by following the motion of narrow band components in the spectrum of the received signal. A 2-D image made of spectra taken at different times, a spectrogram, is often used for this purpose.

2. DELAY AND DOPPLER EQUATIONS, AND ACCURACY ANALYSIS

This chapter develops basic delay and doppler formulas used in finding track parameters for measurements of differential delay and doppler; bounds are placed on the variance of track parameter estimators using these measurements. It is assumed here that the ocean is a homogeneous medium with a reflecting boundary at the surface ($z = 0$).

2.1 DELAY AND DOPPLER EQUATIONS

With a sensor at (X_s, Y_s, Z_s) and a target at (Vt, Y_T, Z_T) , the direct, multipath, and differential delay between direct and multipath signals are given by (see Figs. 1.1, and 2.1):

$$D_d(t) = [(X_s - Vt)^2 + (Y_s - Y_T)^2 + (Z_s - Z_T)^2]^{1/2}/C \quad (2.1a)$$

$$D_m(t) = [(X_s - Vt)^2 + (Y_s - Y_T)^2 + (Z_s + Z_T)^2]^{1/2}/C \quad (2.1b)$$

$$D(t) \triangleq D_m(t) - D_d(t) \quad (2.1c)$$

where C is the speed of sound in water. The differential delay rate and differential delay curvature are:

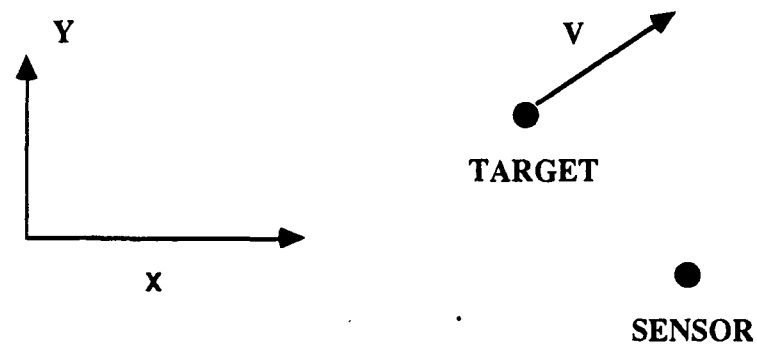
$$\frac{\partial D}{\partial t} = \frac{V}{C^2} (Vt - X_s) \left[\frac{1}{D_m} - \frac{1}{D_d} \right] \quad (2.2a)$$

$$\frac{\partial^2 D}{\partial t^2} = \frac{V^2}{C^2} \left[\frac{1}{D_m} - \frac{1}{D_d} \right] + \frac{(Vt - X_s)^2}{C^4} \left[\frac{1}{D_d^3} - \frac{1}{D_m^3} \right] \quad (2.2b)$$

The doppler shift of a source frequency, f_s is given by

$$f = f_s \left(1 + \frac{V_r}{C} \right) = f_s \cdot \delta \quad (2.3)$$

where f is the received frequency, and V_r is the velocity of the target along a line connecting the target and sensor, and δ is the doppler shift. The direct, multipath, and differential doppler shift between the direct and



TOP VIEW

Figure 2.1 View from above the ocean of the target and sensor. The target is located at $(X_T - Vt, Y_T, Z_T)$ and the sensor is located at, (X_S, Y_S, Z_S) .

multipath signals are given by

$$\delta_d(t) = 1 + \frac{V(Vt - X_s)}{c^2 D_d} = 1 + \frac{\partial D_d(t)}{\partial t} \quad (2.4a)$$

$$\delta_m(t) = 1 + \frac{V(Vt - X_s)}{c^2 D_m} = 1 + \frac{\partial D_m(t)}{\partial t} \quad (2.4b)$$

$$\delta(t) = \delta_m(t) - \delta_d(t) = \frac{\partial D(t)}{\partial t} \quad (2.4c)$$

The differential delay between direct paths from the target to two sensors is given by

$$D_{12} = D_{d1} - D_{d2}, \quad (2.5a)$$

where D_{d1} and D_{d2} are the delays between the target and the individual sensors. The differential doppler between the direct paths of the two sensors is again given by the differential delay rate:

$$\delta_{12} = \delta_{d1} - \delta_{d2} = \frac{\partial D_{12}}{\partial t} \quad (2.5a)$$

$$\frac{\partial \delta_{12}}{\partial t} = \frac{\partial^2 D_{12}}{\partial t^2} \quad (2.5b)$$

2.2 ACCURACY ANALYSIS

It is of interest to know how well the track parameters can be estimated from multipath delay information. The C-R bound can be used in conjunction with the above formulas to put a lower bound on the variance of any unbiased estimators of the track parameters.

C-R BOUND CALCULATION

It is assumed that data is available during the time period $(-T, T)$. Over this time period, the data are nonstationary. Since the C-R bound can be used

only with stationay data, for purposes of determining a bound on the variance of the track parameter estimates, it is assumed that estimates of track parameters are made from sub-intervals of time of length Δt (over which the data are assumed stationary) and linearly combined to form a single estimate of the track parameters. In this case the variance in estimating a track parameter, θ is given by,

$$\sigma_{\theta}^2 = \left(\sum_{i=-N}^N \frac{1}{\sigma_{\theta}^2(i)} \right)^{-1} \quad (2.6a)$$

and $\hat{\theta}$ is given by,

$$\hat{\theta} = \left(\sum_{i=-N}^N \frac{\hat{\theta}(i)}{\sigma_{\theta}^2(i)} \right) / \left(\sum_{i=-N}^N \frac{1}{\sigma_{\theta}^2(i)} \right) \quad (2.6b)$$

where the variances, $\sigma_{\theta}^2(i)$ are bounded below by the C-R bound,

$$\sigma_{\theta}^2(i) > \frac{1}{I_{\theta}(i)} \quad (2.7)$$

where, $I_{\theta}(i)$ is the Fisher information matrix element corresponding to the parameter θ at time t_i .

The variance in estimating θ from time delay measurements over the interval $(-T, T)$ is therefore bounded by,

$$\sigma_{\theta}^2 > \frac{1}{\sum_{i=-N}^N I_{\theta}(i)} \quad (2.8)$$

which can be approximated by,

$$\sigma_{\theta}^2 \gtrsim \left[\int_{-T}^T I_{\theta}(t) dt \right]^{-1} \quad (2.9)$$

for large N . The Fisher information matrix element, $I_{\theta}(i)$, can be evaluated exactly using methods described in Appendix 3. These expressions are algebraically complicated, and difficult to manipulate. If it is assumed that all track parameters but θ are known, then $I_{\theta}(t)$ is given simply by,

$$I_{\theta}(t) = \left(\frac{\partial D}{\partial \theta}\right)^2 I_D(t) \quad (2.10)$$

where $I_D(t)$ is the Fisher information matrix element for the delay, evaluated in section 1. Note that the Fisher information above is larger than that calculated assuming the other track parameters are unknown. Therefore, the resulting bounds on the variance of the track parameter estimates will not be tight.

Using (2.1), (2.10), and (2.9), a lower bound can be placed on the variance of track parameter estimates,

$$\sigma_{\theta}^2 \geq \left[\int_{-T}^T \left(\frac{\partial D(t)}{\partial \theta}\right)^2 I_D(t) dt \right]^{-1} \quad (2.21)$$

where, from (1.2a),

$$I_D(t) \sim w^3 g^2 \text{SNR}^2 / 3$$

for low SNR broadband signals.

DEPTH ESTIMATE VARIANCE

Assuming other track parameters are known, the Fisher information of the depth estimate based on delay measurements is given by (2.10) as,

$$I_{Z_T}(t) = \frac{1}{c^4} \left[\frac{(Z_T - Z_S)^2}{D_d^2} + \frac{(Z_T + Z_S)^2}{D_m^2} + 2 \frac{Z_S^2 + Z_T^2}{D_d D_m} \right] I_D(t) , \quad (2.12)$$

Using (2.21) and integrating,

$$\begin{aligned} \frac{1}{\sigma_{Z_T}^2} &\leq \left(\frac{w^3 g^2 \text{SNR}^2}{3c^3 V} \right) \cdot \left\{ \frac{(Z_T - Z_S)^2}{\alpha_d} \tan^{-1} \frac{\tau}{\alpha_d} + \frac{(Z_T + Z_S)^2}{\alpha_m} \tan^{-1} \frac{\tau}{\alpha_m} \right. \\ &\quad \left. + 2 \frac{Z_S^2 - Z_T^2}{\alpha_d} \tan^{-1} \frac{\tau}{\alpha_d} \right\} \Bigg|_{\tau=X_T-VT}^{\tau=X_T+VT} \end{aligned} \quad (2.13)$$

where

$$\alpha_d = (Y_T^2 + (Z_T - Z_S)^2)^{1/2}$$

$$\alpha_m = (Y_T^2 + (Z_T + Z_S)^2)^{1/2}$$

$$\alpha_+ = (Y_T^2 + Z_T^2 + Z_S^2)^{1/2}$$

In the case of,

$$X_T \pm VT \ll \alpha_d, \alpha_m, \alpha_+ \quad (2.14)$$

and,

$$Y_T^2 \gg Z_S^2, Z_T^2 \quad (2.15)$$

$\frac{1}{2\sigma_{Z_T}^2}$ reduces to,

$$\frac{1}{2\sigma_{Z_T}^2} \leq \left(\frac{w^3 q^2 \text{SNR}^2}{3C^4} \right) \cdot \left(\frac{4Z_S^2}{Y_T^2} \right) \cdot 2T \quad (2.16)$$

Notice that this expression is proportional to T, i.e. the more data available, the lower the variance. Also notice, as the depth of the sensor increases relative to the range at CPA, the minimum variance is decreased.

When (2.15) and,

$$|X \pm VT| \gg \alpha_d, \alpha_m, \alpha_+ \quad (2.17)$$

hold, i.e. most all of the delay curve is available,

$$\frac{1}{2\sigma_{Z_T}^2} \leq \left(\frac{w^3 q^2 \text{SNR}^2}{3C^4} \right) \left(\frac{\pi}{V} \right) \left(\frac{4Z_S^2}{Y_T} \right) \quad (2.18)$$

In this case, the variance in estimating the target depth is dependent on the sensor depth, the deeper the sensor, the better the depth estimate; and the target velocity and CPA range, closer slower moving targets give better depth estimates.

Y OFFSET

With (2.11) and (2.1), $\frac{1}{\sigma_{Y_T}^2}$ is, in the case of other track parameters known, given by,

$$\frac{1}{\sigma_{Y_T}^2} \leq \left(\frac{w^3 g^2 \text{SNR}^2}{3V} \right) \left(\frac{Y_T^2}{C^4} \right) \left\{ \frac{1}{\alpha_d} \tan^{-1} \frac{\tau}{\alpha_d} + \frac{1}{\alpha_m} \tan^{-1} \frac{\tau}{\alpha_m} - \frac{2}{\alpha_+} \tan^{-1} \frac{\tau}{\alpha_+} \right\} \bigg|_{\tau=X_T+VT}^{\tau=X_T-VT} \quad (2.19)$$

If only data near CPA is available, i.e. (2.14) applies, then under (2.15), $\frac{1}{\sigma_{Y_T}^2}$ reduces to,

$$\frac{1}{\sigma_{Y_T}^2} \leq \left(\frac{w^3 g^2 \text{SNR}^2}{3C^4} \right) (4T) \left(\frac{Z_S^2 Z_T^2}{Y_T^4} \right) \quad (2.20)$$

In other words, the $\sigma_{Y_T}^2$ is reduced for increasing Z_S , Z_T , and T and decreasing target CPA range.

When a lot of data are available, i.e. when (2.17) is applicable, $\sigma_{Y_T}^2$ becomes,

$$\frac{1}{\sigma_{Y_T}^2} \leq \frac{w^3 g^2 \text{SNR}^2}{3C^4} \cdot \frac{8}{V} \cdot \frac{Z_S^2 Z_T^2}{Y_T^3} \quad (2.21)$$

In this case, more data no longer significantly improves the estimate. Note here that the slower the target moves, the broader the delay curve, and the better the estimate.

X OFFSET

Using (2.10) and (2.11) the variance of the X offset can be bounded by,

$$\frac{1}{\sigma_{X_T}^2} \leq \frac{w^3 g^2 \text{SNR}^2}{3c^4 v} \left\{ -\alpha_d \tan^{-1} \frac{\tau}{\alpha_d} - \alpha_m \tan^{-1} \frac{\tau}{\alpha_m} + 2\alpha_+ \tan^{-1} \frac{\tau}{\alpha_+} \right\} \Bigg|_{\tau=X_T-VT}^{\tau=X_T+VT} \quad (2.22)$$

Under the conditions (2.14) and (2.15),

$$\frac{1}{\sigma_{X_T}^2} \leq \frac{w^3 g^2 \text{SNR}^2}{2c^4} \cdot \frac{4}{3} v^2 T^3 \left(\frac{Z_s^2 Z_T^2}{Y_T^6} \right) \quad (2.23)$$

Note here the heavy dependence of $\sigma_{X_T}^2$ on v, T , and Y_T : the more data available near CPA, and the more peaked the delay curve is, the easier it is to estimate $\sigma_{X_T}^2$.

When (2.27) applies,

$$\frac{1}{\sigma_{X_T}^2} \leq \frac{w^3 g^2 \text{SNR}^2}{3c^4} \cdot \frac{\pi}{v} \frac{Z_s^2 Z_1^2}{Y_T^3} \quad (2.24)$$

In this case, the estimate variance is no longer as dependent on the shape of the delay curve or the amount of data available.

VELOCITY

Again, using (2.10) and (2.11), a bound on the variance of the velocity estimate can be found as,

$$\begin{aligned} \frac{1}{\sigma_v^2} \leq & \frac{w^3 g^2 \text{SNR}^2}{3c^4} \cdot \frac{1}{v^3} \left[(\alpha_d^3 \tan^{-1} \frac{\tau}{\alpha_d} + \alpha_m^3 \tan^{-1} \frac{\tau}{\alpha_m} - 2\alpha_+^3 \tan^{-1} \frac{\tau}{\alpha_+}) \right. \\ & + 2\alpha_d^2 \left(\frac{\alpha_d^2}{2} \log(\alpha_d^2 + \tau^2) + \frac{\alpha_m^2}{2} \log(\alpha_m^2 + c^2) - \alpha_+^2 \log(\alpha_+^2 + \tau^2) \right) \\ & \left. + X^2 (-\alpha_d \tan^{-1} \frac{\tau}{\alpha_d} - \alpha_m \tan^{-1} \frac{\tau}{\alpha_m} + 2\alpha_+ \tan^{-1} \frac{\tau}{\alpha_+}) \right] \Bigg|_{\tau=X_T-VT}^{\tau=X_T+VT} \quad (2.25) \end{aligned}$$

When (2.14) and (2.15) are satisfied,

$$\frac{1}{\sigma_v^2} \leq \frac{w^3 g^2 \text{SNR}^2}{3c^4} \cdot (2v^5 T^5 + X_T^4 V^4 + \frac{2}{3} X_T^2 V^3 T^3) 2 \left(\frac{Z_s^2 Z_T^2}{Y_T^6} \right) \quad (2.26)$$

Again, the estimate variance is sensitive to V, T, Y_T ; lower variance estimates are obtained from data near CPA where the delay curve is more peaked.

If instead of (2.14), (2.15) is applicable, then

$$\frac{1}{\sigma_V^2} = \frac{2\pi W^3 g^2 \text{SNR}^2}{3c^4} \cdot \frac{(Z_S^2 Z_T^2)}{V^3 Y_T} \quad (2.27)$$

Notice, in this case, the variance of the velocity estimate increases with the "sharpness" of the delay, and not the "flatness" as was the case in (2.26).

SUMMARY

In summary, provided the delay estimates are good, i.e. the bandwidth of the signal is large enough, and provided the aperture size of the array is large, i.e. Z_S is large enough compared to the CPA range of the target, reasonably small lower bounds on the variance of the track parameter estimates are obtained.

Tighter bounds on the track parameter estimates as well as bounds for estimates based on inter-sensor and multipath delay information from two sensor arrays are presented in appendix 3.

3. POINT METHOD OF TRACK PARAMETER EXTRACTION

Techniques for extracting track parameters from correlograms, dopplergrams, and spectrograms are presented in this chapter. The parameters of interest are V , the velocity of the target; z_T , the depth of the target; R_{CPA} , the radius of closest approach to the sensor array; and θ , the bearing angle relative to the array.

3.1 SINGLE SENSOR

The case of a single sensor at $(0,0, Z_S)$ and a single target at (Vt, Y_T, Z_T) with one surface reflection is considered first. Figure 3.1 shows the correlogram for this case. Differential delay rate, estimated from the dopplergram is plotted in Figure 3.2. These measurements lead to estimates relating R_{CPA} , V , and Z_T . Measurements of the doppler shift of spectral lines give velocity as well as R_{CPA} estimates.

Delay Measurements

When the target is far away from the sensor, the differential delay becomes less dependent on the relative y-axis positions of the sensor and target. As $|t| \rightarrow \infty$, a relationship between z_T and V can be developed.

From (2.1) for $|t| \gg 1$,

$$D_d \sim [(Vt)^2 + Y_T^2]^{1/2} \left[1 + \frac{1}{2} \frac{(Z_S - Z_T)^2}{(Vt)^2 + Y_T^2} \right] / C,$$

$$D_m \sim [(Vt)^2 + Y_T^2]^{1/2} \left[1 + \frac{1}{2} \frac{(Z_S + Z_T)^2}{(Vt)^2 + Y_T^2} \right] / C,$$

$$D = D_m - D_d \sim \frac{2Z_S Z_T}{C [(Vt)^2 + Y_T^2]^{1/2}}$$

Since for $|t| \gg 1$, $(Vt)^2 \gg Y_T^2$,

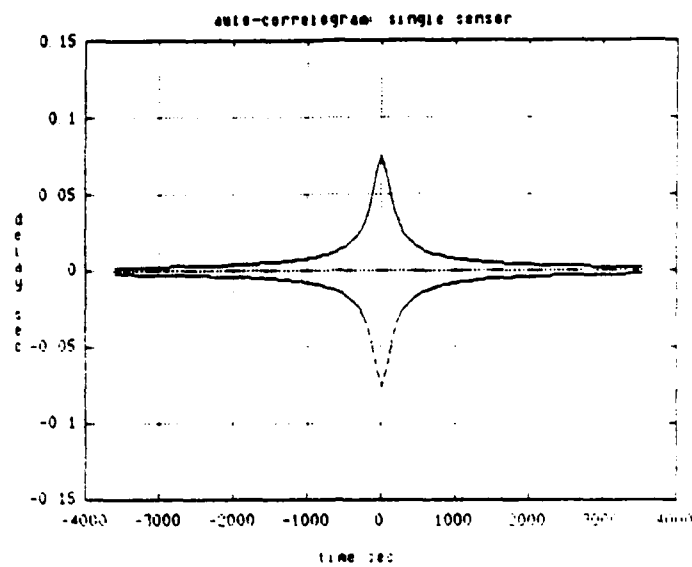


Figure 3.1 The autocorrelogram of a target at $(Vt, 0, Z_T)$ passing by a sensor at $(0, 0, Z_S)$ in the presence of a surface reflection.

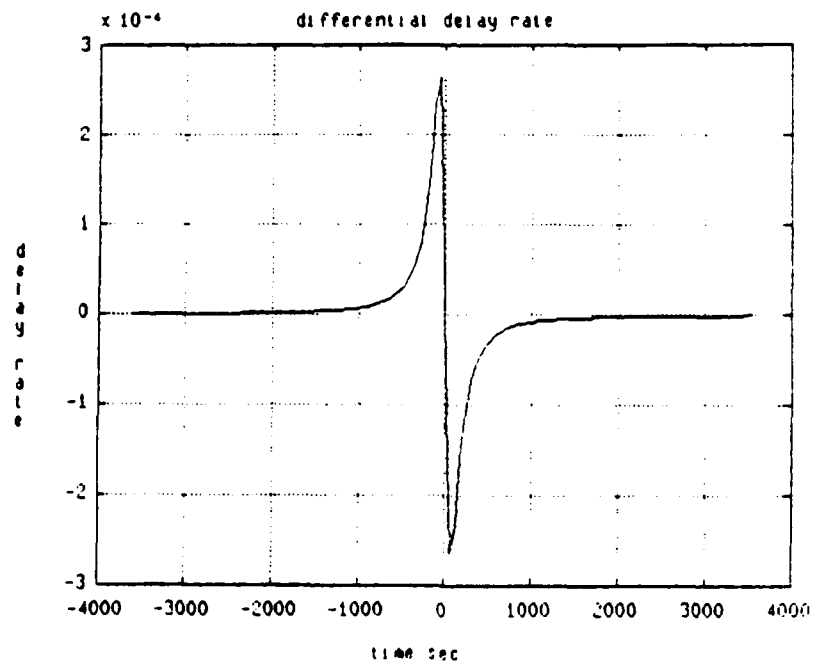


Figure 3.2 Differential delay rate (differential doppler between the direct and multipath signals for a target located at (V_t, D, Z_T) passing by a sensor at $(0, 0, t_s)$.

$$D \sim \frac{2Z_S Z_T}{C V t}, \quad |t| \gg 1 \quad (3.1)$$

Performing a least squares fit of ρ/t to the tails of the measured $D(t)$ yields the relationship:

$$\frac{Z_T}{V} = \hat{\rho} \frac{C}{2Z_S}, \quad (3.2)$$

where $\hat{\rho} = \min_{\rho} [D(t) - \frac{\rho}{t}]^2$ for $t \gg 1$.

A relationship between R_{CPA} and Z_T can be found by examining $D(0)$, a readily available quantity. From (2.1) and, $R_{CPA} = D_d(0) = [Y_T^2 + (Z_S - Z_T)^2]^{1/2}$,

$$CD(0) = [R_{CPA}^2 + 4Z_S Z_T]^{1/2} - R_{CPA} \quad (3.3)$$

Solving (3.3) for R_{CPA} ,

$$R_{CPA} = \frac{2Z_S Z_T}{CD(0)} - \frac{CD(0)}{2} \quad (3.4)$$

Using a velocity estimated by other means, R_{CPA} and Z_T can be obtained using (3.2) and (3.4) with a few measurements of $D(t)$.

Doppler Measurements

By following doppler shifts of lines in the spectrogram, V and R_{CPA} can both be estimated. Figure 3.3 shows the spectrogram of a constant velocity target emitting a single strong spectral line. Using (2.3) and (2.4),

$$f = f_s \left(1 + \frac{V_r}{C}\right) = f_s \left(1 + \frac{V(Vt - X_S)}{C^2 D_d}\right) \quad (3.5)$$

as $t \rightarrow -\infty$, $D_d \rightarrow D_m \frac{Vt - X_S}{C}$, and

$$f \rightarrow f_{\max} \triangleq \left(1 + \frac{V}{C}\right) f_s \quad (3.6)$$

Similarly, as $t \rightarrow +\infty$,

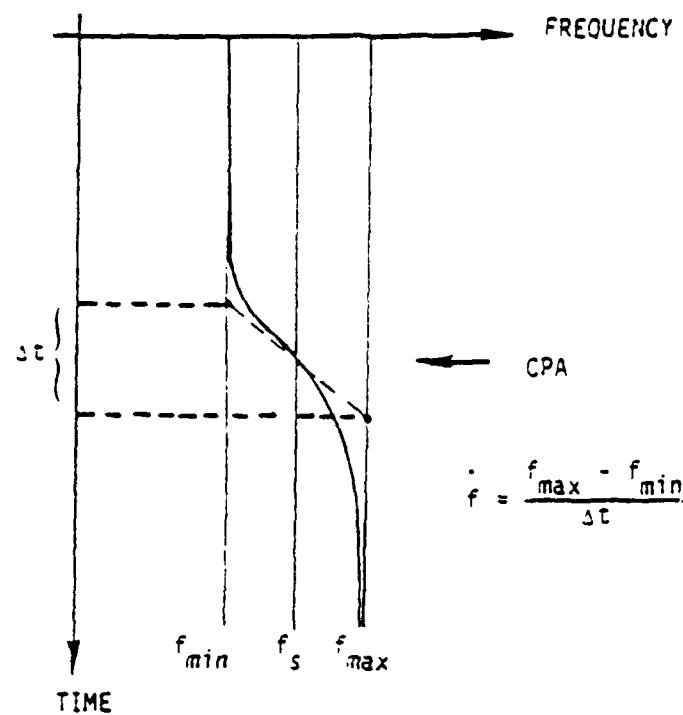


Figure 3.3 Doppler shift vs. time for a constant velocity source

$$f \rightarrow f_{\min} \triangleq (1 - \frac{V}{C}) f_s \quad (3.6)$$

from (3.6) and (3.7) an expression for the velocity is obtained,

$$f_s = \frac{1}{2} (f_{\max} - f_{\min}) \quad (3.8)$$

and

$$V = C \frac{f_{\max} - f_{\min}}{f_{\max} + f_{\min}} \quad (3.9)$$

Range information can be found by examining $\frac{\partial f}{\partial t}$ at CPA:

$$\left. \frac{\partial f}{\partial t} \right|_{\text{CPA}} = \frac{f_s}{C} \left. \frac{\partial V_r}{\partial t} \right|_{\text{CPA}} \quad (3.10)$$

from (3.7)

$$\left. \frac{\partial f}{\partial t} \right|_{\text{CPA}} = f_s \left. \frac{\partial^2 D_d}{\partial t^2} \right|_{\text{CPA}} = \frac{f_s}{C} \frac{V^2}{R_{\text{CPA}}} \quad (3.11)$$

The time of maximum differential doppler is easily obtained from the dopplergram, and relates the direct and multipath CPA ranges. The maximum differential doppler time, t^* , is given by (see (2.4)),

$$\ddot{D}(t) = \ddot{D}_m(t^*) - \ddot{D}_d(t^*) = 0 \quad (3.12)$$

Using (3.2)

$$D_m - D_d = \frac{V^2 t_*^2}{C^2} \left[\frac{D_m^3 - D_d^3}{D_m^2 D_d^2} \right]$$

$$D_m^2 D_d^2 = \frac{V^2 t_*^2}{C^2} (D_m^2 t + 3 D_m D_d)$$

Assuming $\frac{D_m^2}{D_m D_d} \ll 3$,

$$D_m D_d \sim 3 \frac{V^2 t_*^2}{C^2}$$

Therefore,

$$t_{\star}^2 = \frac{C^2}{3V^2} D_m(t_{\star}) D_d(t_{\star}) \quad (3.13)$$

$$\delta(t_{\star}) = \dot{D}(t_{\star}) = \frac{D(t_{\star})}{3t_{\star}} \quad (3.14)$$

Using (2.1), (2.2) and

$$R_d = Y_T^2 + (Z_S - Z_T)^2$$

$$R_m = Y_T^2 + (Z_S + Z_T)^2,$$

the time of maximum differential delay is given by,

$$t_{\star} = \frac{1}{4V} [R_d^2 + R_m^2 + (R_d^2 + R_m^2)^2 + 32R_d^2 R_m^2]^{1/2}]^{1/2} \quad (3.15)$$

Summary

To summarize, from the correlogram and spectrogram, all track parameters can be estimated.

$$\hat{V} = C \frac{f_{\max} - f_{\min}}{f_{\max} + f_{\min}} \quad (3.16a)$$

$$\hat{R}_{CPA} = \frac{1}{2} C \frac{(f_{\max} - f_{\min})^2}{f_{\max} + f_{\min}} \left(\frac{\partial f}{\partial t} \right)_{t_{R_{CPA}}}^{-1} \quad (3.16b)$$

$$\hat{\rho} = \underset{\rho}{\text{Min}} [D(t) - \rho/t]^2 \quad (3.17a)$$

$$\hat{Z}_T = \hat{\rho} \hat{V} \cdot \frac{C}{2Z_s} \quad (3.17b)$$

$$\hat{R}_{CPA} = \frac{2Z_s \hat{Z}_T}{CD(0)} - \frac{CD(0)}{2} \quad (3.17c)$$

where f_{max} , f_{min} , $\left. \frac{\partial f}{\partial t} \right|_{t=R_{CPA}}$, are measured from the spectrogram; $\hat{\rho}$ and $D(0)$ are measured from the correlogram.

3.2 TWO SENSOR TRACK PARAMETER ESTIMATION

With the addition of a second sensor, the track parameter estimation capability of an array is greatly improved. First, V, Z_T and R_{CPA} estimates from each sensor can be combined to form estimates of lower variance. Second, measurements of intersensor delay and doppler lead to further estimates of V, Z_T, R_{CPA} , and possibly θ - the bearing angle relative to the array.

Two commonly used two-sensor arrays are considered here, the vertical array and the horizontal array. The arrays are shown in Figure 3.4; theoretical correlograms in the presence of multipath are shown in figures 3.5 and 3.7.

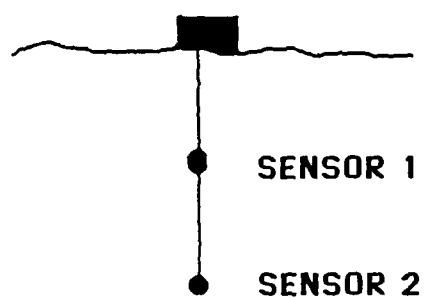
The Vertical Array

The vertical array depicted in Figure 3.4 has two sensors placed one above the other. This array is radially symmetric, and therefore can only estimate Z_T, V , and R_{CPA} . Separate estimates of these parameters can be made from multipath information at each sensor as well as inter-sensor delay and doppler shift data. Cross correlation and cross differential doppler are shown in Figure 3.5.

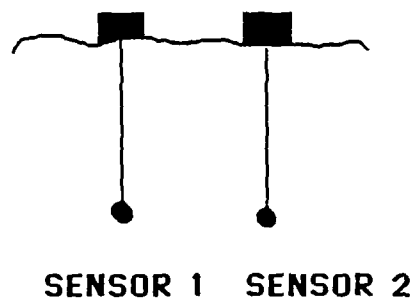
As can be seen in Figure 3.6, the delay between the direct and multipath propagation paths in the single sensor case is equivalent to the intersensor direct path delay in the 2-sensor vertical array. If the sensors of the vertical array are placed at

S1: $(0,0,Z_{s1})$

S2: $(0,0,Z_{s2})$



VERTICAL ARRAY



HORIZONTAL ARRAY

Figure 3.4 Vertical and horizontal 2-sensor arrays

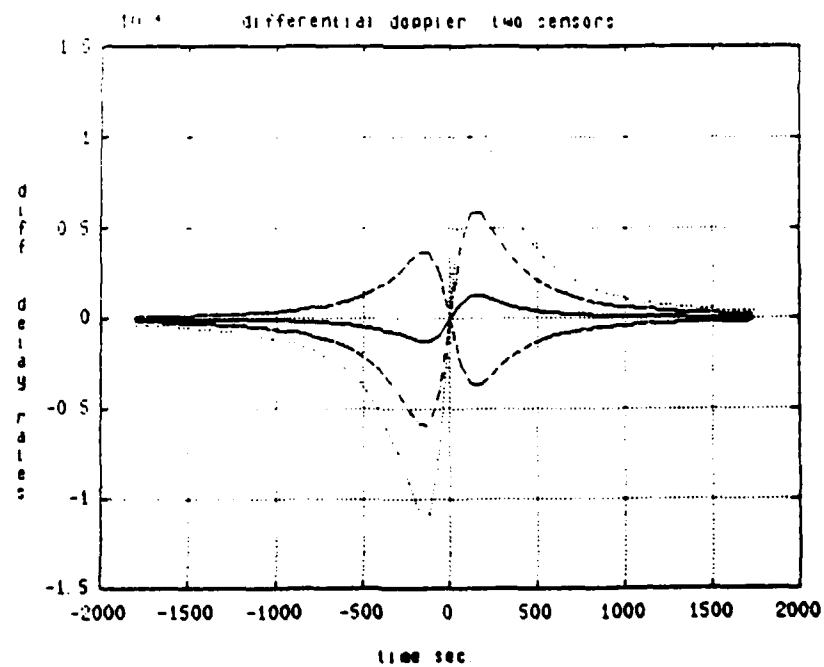
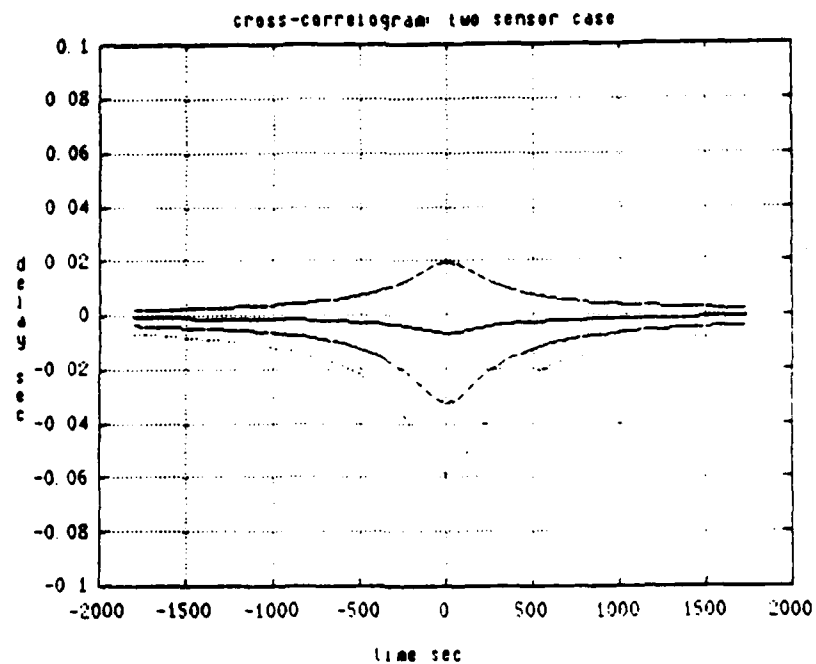


Figure 3.5 The cross-correlogram and differential doppler for a two sensor vertical array in the presence of a multipath reflection.

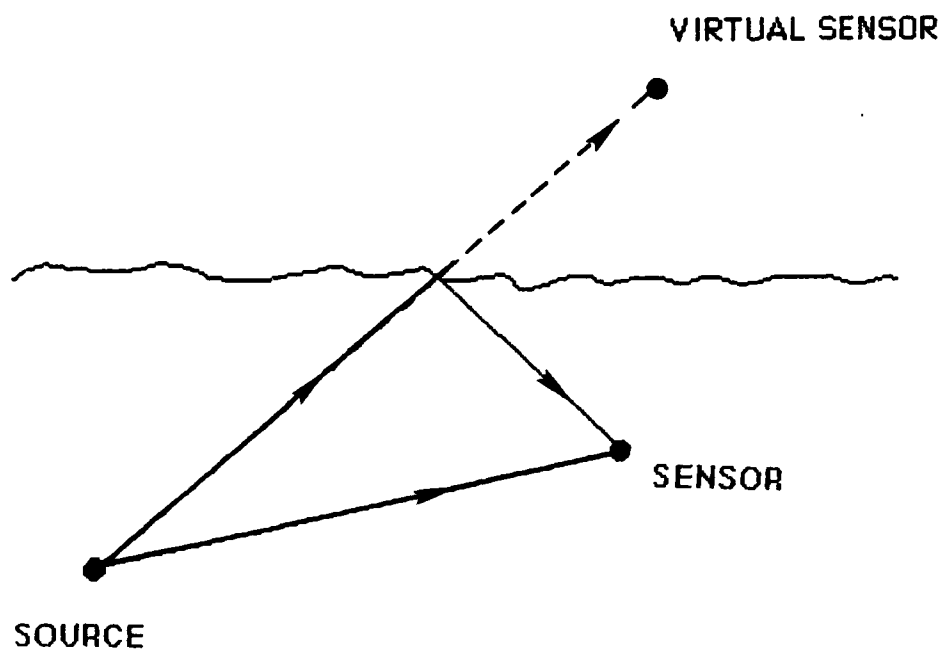


Figure 3.6 The equivalence of a two sensor vertical array in the absence of multipath and a single sensor array in the presence of multipath can be seen in the above diagram.

where $Z_{s2} > Z_{s1}$

then, making the substitution

$$Z_S = \frac{Z_{s2} - Z_{s1}}{2} \quad (3.18)$$

in (3.17) will result in track parameter estimates from inter-sensor delay and doppler estimates. Note that R_{CPA} in this case is measured as the distance of closest approach to the deepest sensor. Also note that Z_T is the depth relative to the midpoint between the sensors.

The various estimates of V , Z_T and R_{CPA} (sensor 1, sensor 2, and inter-sensor measurements) should be combined so as to minimize the variance of the final estimates. The method described in (2.6) is optimal over all linear combinations of the different estimates. In this case, more weight is given to the smaller variance estimates. If the multipath reflection is weak, the inter-sensor measurements are more important. Otherwise, the estimate made from the array with the larger aperture size will have the least variance and therefore more weight. (The aperture size is $2Z_{S_i}$ for the i^{th} sensor, and $Z_{S_i} - Z_{S_j}$ for inter-sensor measurements).

The Horizontal Array

The horizontal array, depicted in Figure 3.4, consists of two sensors at the same depth. As this array is not radially symmetric, intersensor multipath information leads to estimates of bearing angle as well as R_{CPA} and V . These estimates can be combined with estimates from data at individual sensors to form estimates of Z_T , the depth of the target; R_{CPA} , the radius of closest approach; V , the target velocity; X_C and Y_C , the X and Y axis crossings of the target; and θ , the bearing angle. Due to symmetries in the array, however, θ and Y_C can be only determined to within a sign.

The horizontal array has sensors located at

S1: $(-X_S, 0, Z_S)$

$$S_2: (X_s, 0, Z_s) .$$

The target is moving by the sensors at angle θ relative to the X axis, at a velocity V , and a depth of Z_T .

The position of the target is given by,

$$\text{Target: } (Vt\cos\theta + X_T, Vt\sin\theta + Y_T, Z_T) .$$

So the target is at CPA when $t=0$, define, $\text{ctn}\theta$

$$Y_T = X_T \text{ctn}\theta .$$

Note that a target travelling along this trajectory will have axis crossings of

$$X_C = X_T(1 + \text{ctn}^2\theta)$$

$$Y_C = Y_T(1 + \tan^2\theta)$$

From (2.5) the inter-sensor delay is given by

$$D_{12}(t) = [(Vt\cos\theta + X_T + X_S)^2 + (Vt\sin\theta + Y_T - Y_S)^2 - (Z_S - Z_T)^2]^{1/2} \\ - [(Vt\cos\theta + X_T - X_S)^2 + (Vt\sin\theta + Y_T - Y_S)^2 + (Z_S - Z_T)^2]^{1/2} \quad (3.19)$$

Figure 3.7 shows the cross-correlogram and differential doppler for this case.

By examining the far range behavior of (3.19), an estimate of θ can be obtained. When the target is far from the array, signals emitted from the target arrive at the array from essentially the same direction, θ -- the bearing angle. The intersensor time delay will then be

$$D(|t| \rightarrow \infty) = \pm \frac{2X_S}{C} \cos\theta ,$$

The bearing angle, θ can therefore be found as:

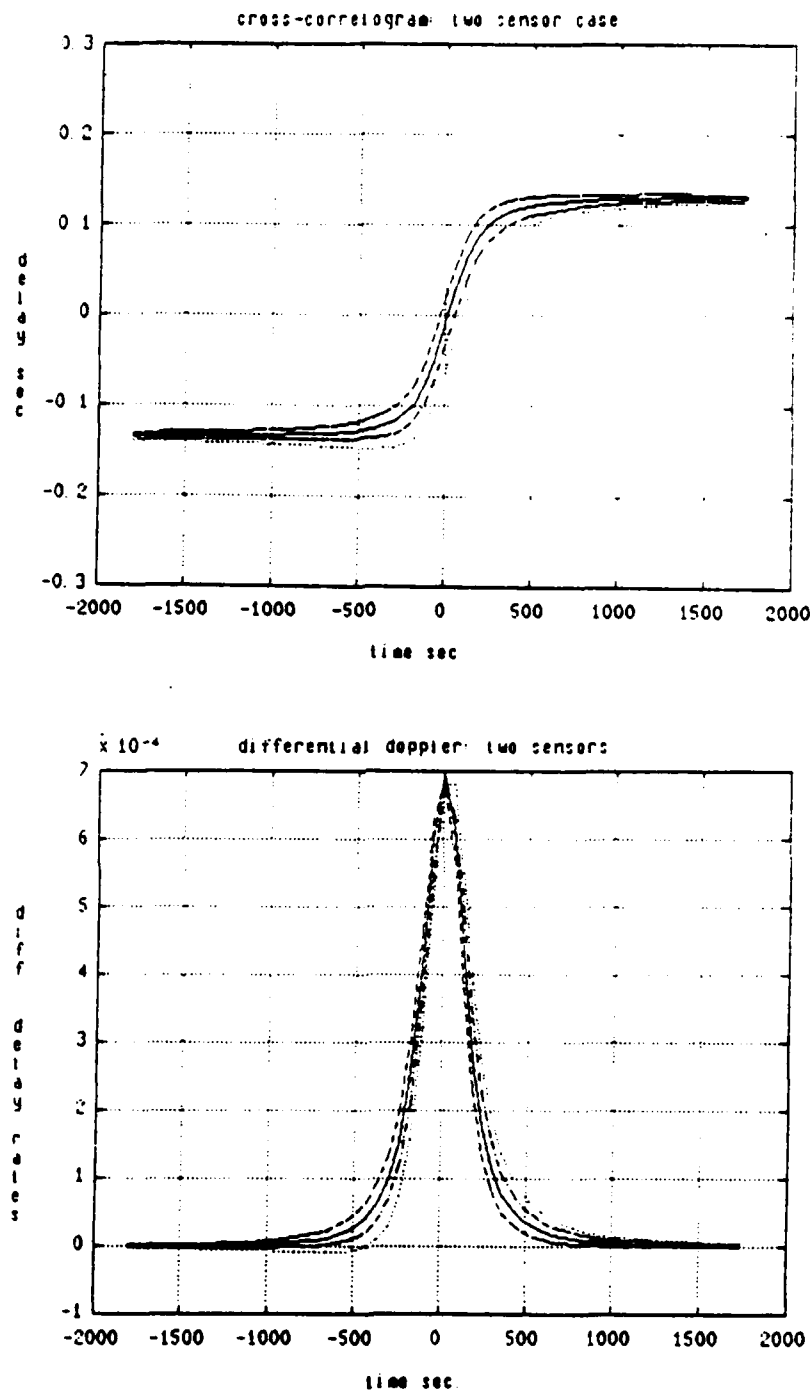


Figure 3.7 The cross-correlogram and differential doppler for a two sensor horizontal array in the presence of a multipath reflection. In this case the target is travelling along a line parallel to the line drawn between the sensors.

$$\cos\theta = \frac{CD(|t| \gg |)}{2X_S} \quad (3.20)$$

Examining the intersensor delay at CPA, (at $t=0$), yields an expression relating X_T and R_{CPA} . Recall,

$$R_{CPA} = (X_T^2 + Y_T^2 + (Z_T - Z_S)^2)^{1/2} \quad (3.21)$$

Using (3.17)

$$CD_{12}(0) = [R_{CPA}^2 + 2X_TX_S]^{1/2} - [R_{CPA}^2 - 2X_TX_S]^{1/2} \quad (3.22)$$

Solving for R_{CPA} ,

$$R_{CPA} = [(C^2 D_{12}^2(0) - 2X_TX_S)(C^2 D_{12}^2(0) - 6X_TX_S)]^{1/4} \quad (3.23)$$

When the relative sensor delay is zero, the target is between the sensors, at $(0, Y_C, Z_T)$. Examining the relative delay rate at this point yields an expression for Y_C . Define

$$t_{Y_C} \triangleq t: D_{12}(t) = 0 \quad (3.24)$$

Recall,

$$\begin{aligned} \frac{\partial D_{12}}{\partial t} &= \frac{V \cos\theta}{C^2 D_1} (V t \cos\theta + X_T + X_S) - \frac{V \cos\theta}{C^2 D_2} (V t \cos\theta + X_T - X_S) \\ &\quad + \frac{V \sin\theta}{C^2 D_1} (V t \sin\theta + Y_T - Y_S) - \frac{V \sin\theta}{C^2 D_2} (V t \sin\theta + X_T - X_S) \end{aligned} \quad (3.25)$$

where D_1 and D_2 are the delays from the target to sensor 1 and sensor 2. When $D_{12} = 0$, $D_1 = D_2$, and the target is at $(0, Y_C, Z_T)$. Therefore,

$$\begin{aligned} \left. \frac{\partial D_{12}}{\partial t} \right|_{t_{Y_C}} &= 2X_S \frac{V \cos\theta}{C^2 D_1}, \\ CD_1 &= \frac{2X_S \frac{V}{C} \cos\theta}{\dot{D}(t_{Y_C})} \end{aligned} \quad (3.26)$$

At t_{y_c} ,

$$c^2 D_1^2 = (Z_T - Z_S)^2 + y_c^2 + x_S^2$$

and, solving for y_c

$$y_c = [x_S^2 \left[\left(\frac{2V \cos \theta}{CD(t_{y_c})} \right)^2 - 1 \right] - (Z_T - Z_S)^2]^{1/2} \quad (3.27)$$

When the differential delay between sensors is at a maximum, the target is at $(x_c, 0, Z_T)$. Looking at $D_{12}(t_{x_c})$, where

$$t_{x_c} \triangleq \max_t |D_{12}(t)|, \quad (3.28)$$

yields an expression for x_c . At t_{x_c} , $D_{12}(t)$ is given by

$$CD_{12}(t_{x_c}) = [(x_S + x_c)^2 + (Z_S - Z_T)^2]^{1/2} - [(x_S - x_c)^2 + (Z_S - Z_T)^2]^{1/2} \quad (3.29)$$

Solving for x_c ,

$$x_c^2 = \frac{\frac{c^4 D_{12}^4(t_{x_c})}{4} + (x_S^2 + (Z_S - Z_T)^2) c^2 D_{12}^2(t_{x_c})}{4x_S^2 - c^2 D_{12}^2(t_{x_c})}$$

The sign of x_c can be determined by looking at the times of CPA of the individual sensors; x_c will have the sign of the sensor location that had the first CPA. Note, however, if $Z_S - Z_T$ or the bearing angle is close to 0, then $D_{12}(t_{x_c}) \sim \frac{2x_S}{c}$ and x_c cannot be determined accurately in this manner.

Velocity can be determined by measuring various times of CPA and axis crossings. Four position-time pairs can be fairly easily measured.

$$(x_c, 0, Z_T) \text{ at } t_{x_c} = \max_t D_{12}(t)$$

$$(0, y_c, Z_T) \text{ at } t_{y_c} = t: D_{12}(t) = 0$$

$$(\alpha, \beta, Z_T) \text{ at } t_{R_{CPA_1}} = \max_t D_1(t)$$

$$(\alpha + ZX_s \sin \theta \cos \theta, \beta + Z_X \cos^2 \theta, Z_T) \text{ at } t_{R_{CPA_2}} = \max_t D_2(t)$$

where $D_1(t)$ and $D_2(t)$ are the differential delays between the direct and multipath signals at sensor 1 and sensor 2; and α, β are constants. Two of the many estimates of velocity are,

$$V = (X_C^2 - Y_C^2)^{1/2} \quad (3.31a)$$

$$V = \frac{2X_s}{\cos \theta} \frac{1}{t_{R_{CPA_1}} - t_{R_{CPA_2}}} \quad (3.31b)$$

To summarize, estimates of $\theta, Y_C, X_C, R_{CPA}$, and V can be obtained as functions of the inter-sensor delay and doppler (delay rate), Z_T and sensor coordinates. These estimates, in combination with single sensor multipath data completely describe the track parameters of a target moving along a straight line past the array.

4. PARAMETRIC FIT METHODS OF TRACK PARAMETER ESTIMATION

The parameter extraction techniques presented in the previous chapter relied on knowledge of $D(t)$ and derivatives at specific points in time, namely $|t| \ll 1$ (near CPA) and $|t| \gg 1$ (far from CPA). Often times, $D(t)$ is not known accurately in these regions of time (see appendix 1 or section 1.1), and the parameter extraction techniques described in the previous chapter can not be used. This chapter develops parameter extraction techniques based on all available delay information, not just that near and far from CPA. Two different techniques are developed and applied to single sensor, two sensor vertical, and two sensor horizontal arrays.

As the functional form of the delay is known (see section 2), a parametric fit of a model \hat{D} can be made to the measured D . The parameter estimates would then be chosen as,

$$(\hat{X}_T, \hat{Y}_T, \hat{Z}_T, \hat{V}) = \min_{(X_T, Y_T, Z_T, V)} d(D, \hat{D}) \quad (4.1)$$

where, CD is the measured delay, and recall

$$CD = [(X_T - Vt)^2 + Y_T^2 + (Z_T - Z_S)^2]^{1/2} - [(X_T - Vt)^2 + Y_T^2 + (Z_T + Z_S)^2]^{1/2}$$

for some distance measure d .

The minimization (4.1) is over a cost function which is non-convex in the track parameters for common distance measures. Therefore, exhaustive search methods must be used in finding a solution. If each of the four parameters were quantized to be one of n values, and there were m data points available, the minimization (4.1) would require $O(mn^4)$ computations; about 25 hours compute time for $m=500$, $n=100$, on a 1 mflop computer. To overcome this computational burden, (4.1) can be reformulated so that functions of (X_T, Y_T, Z_T, V) appear as linear coefficients in a least squares minimization, requiring only $O(4m)$ computations, and less than one second compute time on the same computer. Two linear least squares formulations of (4.1) are developed below. The case of a single sensor listening to a target in the presence of a multipath reflection is considered first, and later generalized

to the case of two sensors.

4.1 EQUATION ERROR APPROACH

This method is an equation error-like approach. Recall,

$$D = P - Q, \quad (4.2)$$

where,

$$P = [(X_T - Vt)^2 + Y_T^2 + (Z_T + Z_S)^2]^{1/2} / C$$

$$Q = [(X_T - Vt)^2 + Y_T^2 + (Z_T - Z_S)^2]^{1/2} / C$$

What is desired is a relation in terms of D , P^2 , and Q^2 so that functions of track parameters appear as linear coefficients which can be fit using least squares techniques. Manipulating (4.2) yields the following relationships,

$$D^2 = P^2 + Q^2 - 2PQ \quad (4.3)$$

$$(D^2 - P^2 - Q^2)^2 = 4P^2Q^2 \quad (4.4)$$

$$\begin{aligned} (CD)^4 - 4V^2(CDt)^2 + 8VX_T(C^2D^2t) - 4(Y_T^2 + Z_T^2 + Z_S^2 + X_T^2)(CD)^2 \\ + 16Z_T^2 Z_S^2 = 0 \end{aligned} \quad (4.5)$$

With values of $D(t)$ specified at m time instances, solving for the coefficients of (4.5) which minimize,

$$P^* = \min_A \|\hat{f} - f\|^2, \quad \hat{f} = \Phi A \quad (4.6)$$

$$\Phi = \begin{bmatrix} (CD(t_1)t_1)^2 & C^2D(t_1)^2t_1 & C^2D(t_1)^2 & 1 \\ \vdots & \vdots & \vdots & \vdots \\ (CD(t_m)t_m)^2 & C^2D(t_m)^2t_m & C^2D(t_m)^2 & 1 \end{bmatrix}$$

is a standard linear least squares problem.

$$A = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix} \quad f = \begin{bmatrix} (CD(t_1))^4 \\ \vdots \\ (CD(t_m))^4 \end{bmatrix}$$

The optimal set of coefficients, A^* is given by,

$$A^* = (\Phi^T \Phi)^{-1} \Phi^T f \quad (4.7)$$

and the resulting track parameter estimates are,

$$\begin{bmatrix} V \\ X_T \\ Y_T \\ Z_T \end{bmatrix} = \begin{bmatrix} \frac{1}{4} \sqrt{a_1} \\ -\frac{1}{Y} a_2 / \sqrt{a_1} \\ \frac{1}{4} (a_3 - \sqrt{a_4} / 4Z_s - Z_s^2 + \frac{a_2^2}{a_1} \cdot \frac{1}{16})^{1/2} \\ \frac{\sqrt{a_4}}{4Z_s} \end{bmatrix} \quad (4.8)$$

SENSITIVITY ISSUES

Upon closer examination of (4.1) or (4.6), one finds that there are many sets of parameters (X_T, Y_T, Z_T, V) that result in roughly the same $D(t)$. Indeed, the differences in $D(t)$ between the case of a target moving slowly close by a sensor and the case of the target moving more quickly further from the sensor are subtle, and are small compared to the variance in estimating $D(t)$.

This ambiguity shows up in the eigen-structure of the matrix used in finding the track parameter estimates via (4.6). For typical values of the track parameters, the matrix,

$$\Phi^T \Phi$$

has an eigenvalue which is $o(10^{-4})$ smaller than the rest. The coefficient array, A , will therefore be very sensitive to any noise in $D(t)$.

The eigenvector corresponding to the troublesome eigenvalue is roughly,

$$ev = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Therefore, specification of V and an appropriate modification of (4.6) will result in track parameter estimates that are relatively insensitive to noise in the measurements of $D(t)$. With V specified, the modifications to (4.6) are,

$$A^* = \min_A \|\hat{f} - f\|^2, \quad \hat{f} = \phi A \quad (4.9)$$

$$\phi = \begin{bmatrix} C^2 D(t_1)^2 t_1 & C^2 D(t_1)^2 & 1 \\ \vdots & \vdots & \vdots \\ C^2 D(t_m)^2 t_m & C^2 D(t_m)^2 & 1 \end{bmatrix}$$

$$A = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix} \quad f = \begin{bmatrix} (CD(t_1))^4 & -4V^2(CD(t_1)t_1)^2 \\ \vdots & \vdots \\ (CD(t_m))^4 & -4V^2(CD(t_m)t_m)^2 \end{bmatrix}$$

The least squares solution for A is then given by,

$$A^* = (\phi^T \phi)^{-1} \phi^T f \quad (4.10)$$

and the track parameter estimates are,

$$\begin{bmatrix} X_T \\ Y_T \\ Z_T \end{bmatrix} = \begin{bmatrix} -a_1/8V \\ (a_2/4 + (a_1/8V)^2 - Z_s^2 - a_3/16Z_s^2)^{1/2} \\ \sqrt{a_3}/4Z_s \end{bmatrix} \quad (4.11)$$

4.2 TRANSFORM APPROACH

In this approach, a transformation, which is a function of a depth estimate, is applied to $D(t)$. When the depth estimate is accurate, $D(t)$ is transformed into a second order polynomial whose coefficients are easily fitted.

The transformation is given by,

$$T = (CD \pm \hat{Z}_T \frac{4Z_S}{CD})^2 \quad (4.12)$$

using (2.1) for $D(t)$,

$$T = \frac{(1+\alpha)^2}{4} [(X_T - vt)^2 + Y_T^2 + (Z_T \pm Z_S)^2] + \frac{(1-\alpha)^2}{4} [(X_T - vt)^2 + Y_T^2 + (Z_T \mp Z_S)^2] \\ + \frac{(1-\alpha)^2}{2} [(X_T - vt)^2 + Y_T^2 + (Z_T + Z_S)^2] [(Y_T - vt)^2 + Y_T^2 + (Z_T - Z_S)^2]^{1/2} \quad (4.13)$$

where

$$\alpha = \hat{Z}_T / Z_T$$

When $\alpha \sim 1$, i.e. $\hat{Z}_T \sim Z_T$, (4.13) reduces to,

$$T = (X_T - vt)^2 + Y_T^2 + (Z_T \pm Z_S)^2 + O(\alpha - 1) \quad (4.14)$$

Fitting a polynomial to (4.14), by least squares, for instance, gives,

$$\hat{v} = \sqrt{a_1} \\ \hat{X}_T = -\frac{1}{2\sqrt{a_1}} a_2 \\ \hat{Y}_T = (a_3 - (\hat{Z}_T \pm Z_S)^2 - \hat{X}_T^2)^{1/2} \quad (4.15)$$

where a_1, a_2, a_3 are chosen to minimize

$$\|a_1 t^2 + a_2 t + a_3 - T_{\hat{Z}_T}(D(t))\|^2,$$

and \hat{Z}_T is picked a priori.

The optimal value of \hat{Z}_T , and therefore $(\hat{X}_T, \hat{Y}_T, \hat{V})$, can be found by performing a line search over \hat{Z}_T , using the following as possible error criteria:

$$\text{error} = \sum_i [(a_1 t_i^2 + a_2 t_i + a_3) - T_{\hat{Z}_T}(D(t_i))]^2 \quad (4.16)$$

$$\text{or, error} = \sum_i (\hat{D}(t) - D(t))^2,$$

where $\hat{D}(t)$ is given by (2.1) using, $(\hat{X}_T, \hat{Y}_T, \hat{Z}_T, \hat{V})$.

SENSITIVITY ISSUES

As expected, the error, (4.16) achieves a minimum only for those cases where $D(t)$ is known very precisely (one part in ten thousand for typical values of the track parameters). Since V can be reliably determined from other measurements, a line search over \hat{Z}_T can be performed using,

$$\text{error} = (\hat{V}(\hat{Z}_T) - V)^2 \quad (4.17)$$

instead of (4.16) as an error criterion. As the transformation T results in a one to one relationship between \hat{Z}_T and V , there are no uniqueness problems in the determination of \hat{Z}_T . Knowledge of V , therefore, allows use of (4.12) and (4.17) in estimating the remaining track parameters from noisy measurements of $D(t)$.

4.3 TWO SENSOR EXTENSIONS

In this section, methods for adapting the above techniques to inter-sensor measurements in two sensor arrays are presented. In addition, methods for combining information from two sensors to resolve ambiguities in determining the track parameters are developed.

MODIFICATION FOR INTER-SENSOR DELAY

It is fairly straightforward to modify (4.6) or (4.12) so that they can be used with inter-sensor delay information (instead of multipath delay information). If the sensors are placed in a vertical array, no modification of either method is needed, only estimated target depth needs to be adjusted (see 3.18). With the sensors placed in a horizontal array, changes to the two methods must be made.

The inter-sensor delay in the case of a horizontal array is still written as,

$$D = P - Q \quad (4.18)$$

where, in this case,

$$P = [(X_T - Vt \cos \theta - X_S)^2 + (Y_T - Vt \sin \theta)^2 + (Z_T - Z_S)^2]^{1/2}$$

$$Q = [(X_T - Vt \cos \theta + X_S)^2 + (Y_T - Vt \sin \theta)^2 + (Z_T - Z_S)^2]^{1/2}$$

and

$$\begin{aligned} & (CD)^4 + (CDt)^2(-4V^2) + 8(CD)^2t \cdot (VX_T \cos \theta + VY_T \sin \theta) \\ & + (CD)^2 \cdot (-Y)(X_T^2 + X_S^2 + Y_T^2 + (Z_S - Z_T)^2) + t^2 \cdot (16X_S^2 V^2 \cos^2 \theta) \\ & + t \cdot (-16X_S^2 X_T V \cos \theta) + (16X_S^2 X_T^2) = 0 \end{aligned}$$

With the exception that there are six variables to be determined instead of four, solving for the coefficients of (4.18) is equivalent to solving for the coefficients of (4.2). The track parameters in (4.18) can be determined by the method described in (4.6). Additionally, any a priori knowledge of track parameters can be incorporated in a manner similar to (4.9).

The transformation,

$$T = (CD \pm \frac{Y}{CD})^2 \quad (4.19)$$

will again yield a polynomial for the correct choice of γ . The coefficients of the polynomial can then be fitted, determining the remaining track parameters. Unfortunately, the optimal choice of γ is,

$$\gamma^* = 2X_S(X_T - Vt\cos\theta) \quad (4.20)$$

and the search for γ is now over a two dimensional surface, which, without a good error criterion, will not yield accurate or computationally efficient results.

COMBINING ESTIMATES FROM TWO SENSORS

Even though there are many sets of track parameters resulting in essentially the same multipath delay curve at a sensor, these same sets of track parameters will not necessarily generate similar delay curves at another sensor location. Therefore, if information from two sensors is available, ambiguities in track parameter estimates can be resolved by looking for track parameter estimates which are consistent at the two sensor locations.

If data is available from two sensors placed in a vertical array, sets of estimates, parameterized by V (or Z_T), can be constructed using either (4.9) or (4.12). A line search can then be performed over V (or Z_T) for the set of track parameters minimizing the error,

$$\text{error} = [\hat{Y}_T(i,1) - \hat{Y}_T(i,2)]^2 \quad (4.21)$$

where $\hat{Y}_T(l,m)$ is the Y_T estimate from sensor m based on $\hat{V} = V_l$ or, equivalently,

$$\text{error} = [\hat{r}_{CPAO}(i,1) - \hat{r}_{CPAO}(i,2)]^2 \quad (4.22)$$

where $\hat{r}_{CPAO}(l,m)$ is the m^{th} sensor CPA range estimate to the point (0,0,0) based on $\hat{V} = V_l$.

If the data is from two sensors placed in a horizontal array, sets of estimates, parameterized by V (or Z_T), based on individual sensor data can be generated by (4.9) or (4.12). Estimates of the bearing angle, parameterized by v (or Z_T) can be made based on inter-sensor data using (4.18). Track parameter estimates can then be chosen by finding the set of estimates producing the most consistent $(\hat{r}_{CPA1}, \hat{r}_{CPA2}, \hat{\theta})$, i.e., the set $(\hat{r}_{CPA1}, \hat{r}_{CPA2}, \hat{\theta})$ minimizing the error,

$$\text{error} = \left[\sin \theta - \frac{\sqrt{r_{CPA1}^2 - Z_s^2} - \sqrt{r_{CPA2}^2 - Z_s^2}}{2X_s} \right]^2 \quad (4.23)$$

4.4 COMPUTER SIMULATION RESULTS

In this section, results of the parametric fit methods of track parameter estimation applied to simulated data are discussed. The equation error method and the transform method are applied to delays simulated for one and two sensor arrays.

DATA

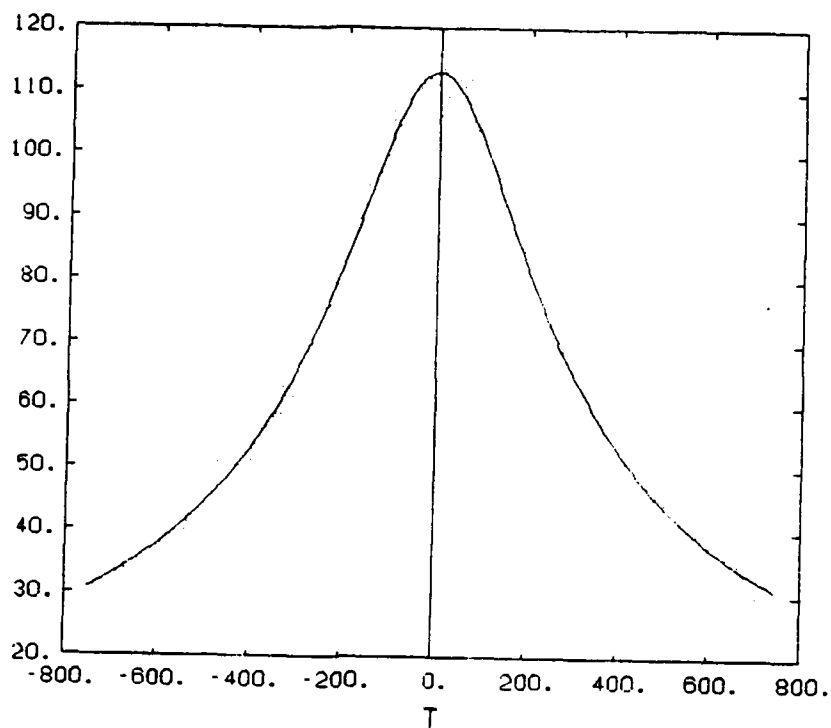
The data, \hat{D} was generated by calculating the true $D(t)$, using (2.1), and adding white gaussian noise. Since $D(t)$ estimates tend to be less certain near CPA (see appendix 1), the additive noise is scaled in proportion to the delay value in the case of single sensor multipath delay curves, and in the case of 2-sensor horizontal arrays, the noise is of constant variance.

Figure 4.1 shows examples of the simulated data. In Figure 4.1, the solid line is the true value of the delay; the dots are the data points used. The signal to noise ratio in these cases is about 20.

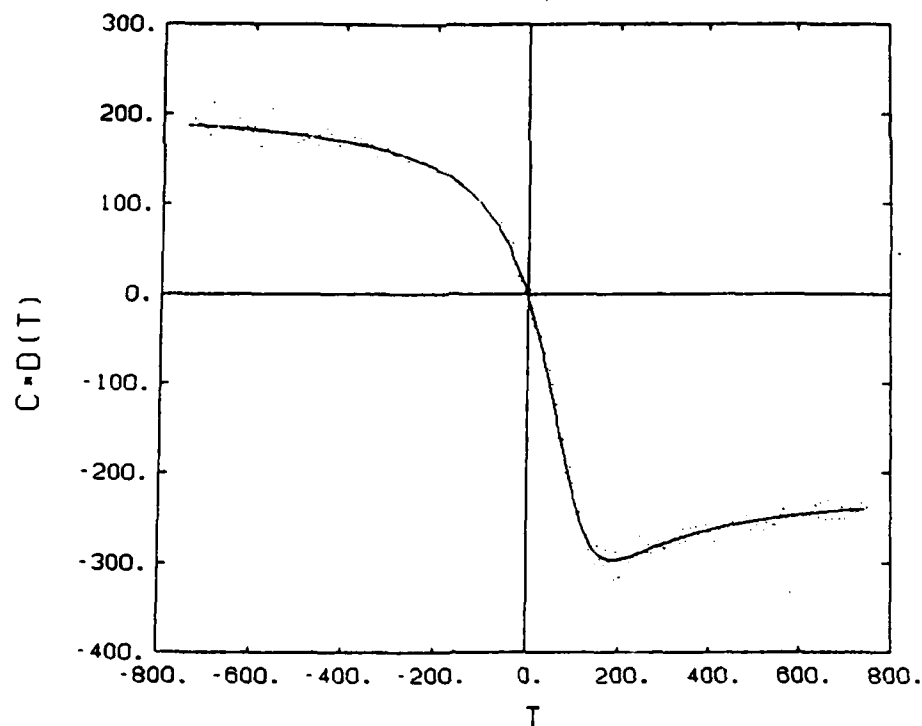
EQUATION ERROR METHOD

The equation error method was applied to data generated using,

Target: (5t, 1000, 200)



(a)



(b)

Figure 4.1 (4.1a) The simulated (dotted) and real (solid) differential delay curves for a 2-sensor horizontal array.

(4.1b) The same curves plotted for a single sensor with a multipath reflection.

Sensor: (0, 0, 300)

When no additive noise is present, the track parameters are estimated to one part in 10^4 . With a SNR of about 20, however, the estimates are off by factors of 100, due to the sensitivity problem discussed earlier.

If the value of V is assumed known, the equation error method can be applied to the noisy data with much improved results. Figure 4.2 shows track parameter estimates as functions of V for the equation error method applied to a data set with a SNR of 20. Note that at the correct value of V , the track parameter estimates are close to the true values.

Sensitivity

To illustrate the sensitivity problems, two delay curves, generated using different sets of track parameters have been plotted. Figure 4.3a and 4.3b show delay curves plotted using the estimated track parameters generated with $V=5$ and $V=10$. Also plotted are data sets with SNR's of 20. Both curves fit the data well. In fact, the differences between the two curves themselves are negligible. Therefore, in this case additional knowledge (knowledge of V , for instance) is required to make a unique choice of track parameter estimates.

TRANSFORM METHOD

The transform method was used to generate the track parameter estimates plotted as functions of \hat{Z}_T in Figure 4.4. Figure 4.4a shows estimates made from noiseless data. Estimates made from data with SNR=20 are essentially the same. The error, which is the norm of the difference between the transformed delay curve and the closest quadratic, is plotted as a function of \hat{Z}_T for the two cases in Figure 4.4b.

As functions of \hat{Z}_T , the track parameter estimates for the two cases are very similar, and assume values close to the true track parameter values for the correct choice of \hat{Z}_T . The error curves, however, indicate that practically any noise in estimating $D(t)$ will lead to ambiguities in determining track parameter estimates. As V is usually available through

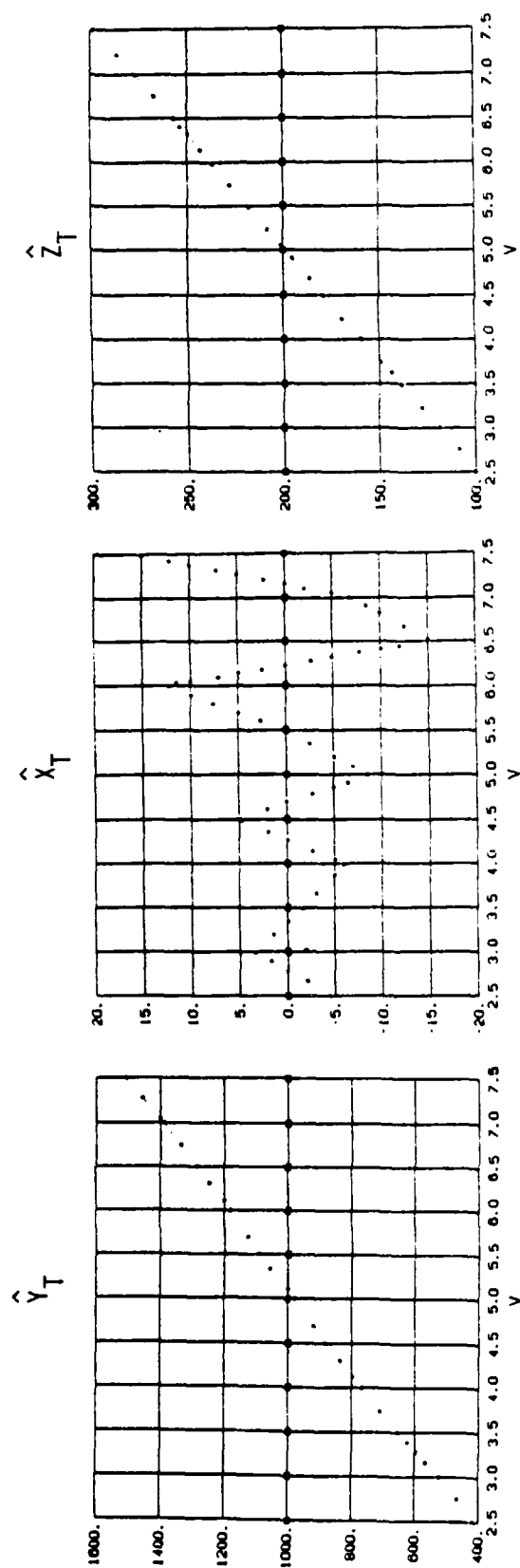


Figure 4.2 Track-parameter estimates as functions of an a priori estimate of velocity. The true parameter values are marked by squares, and the true velocity is 5 m/s.

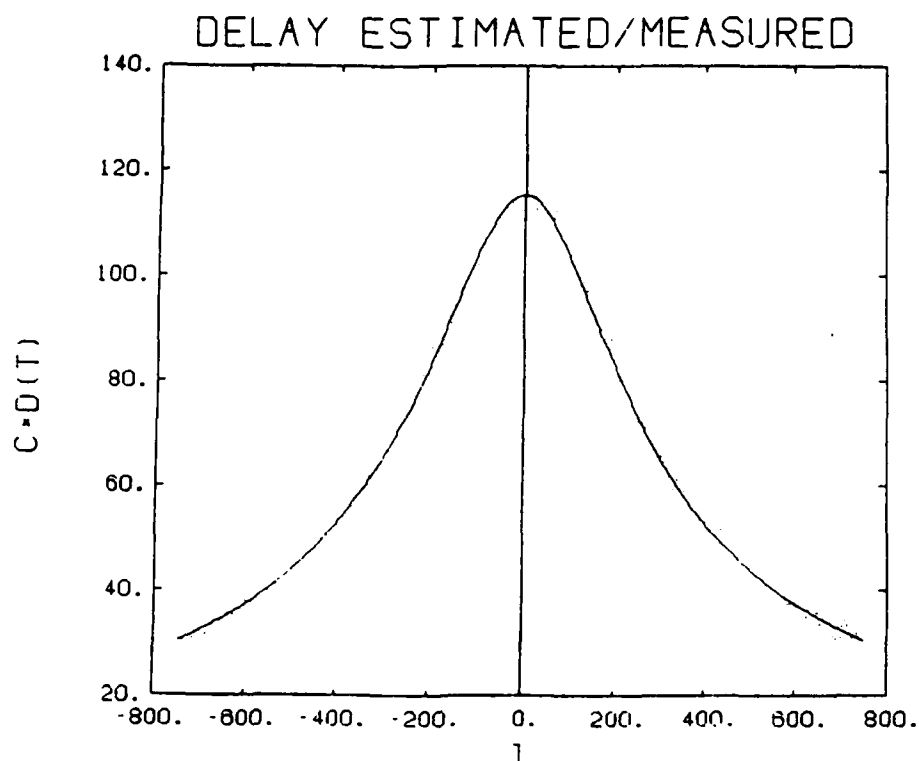


Figure 4.3a Estimated delay curve (solid) using $V=5$ m/s and the resulting track parameters estimated obtained with the equation error method. The dots are the original data set.

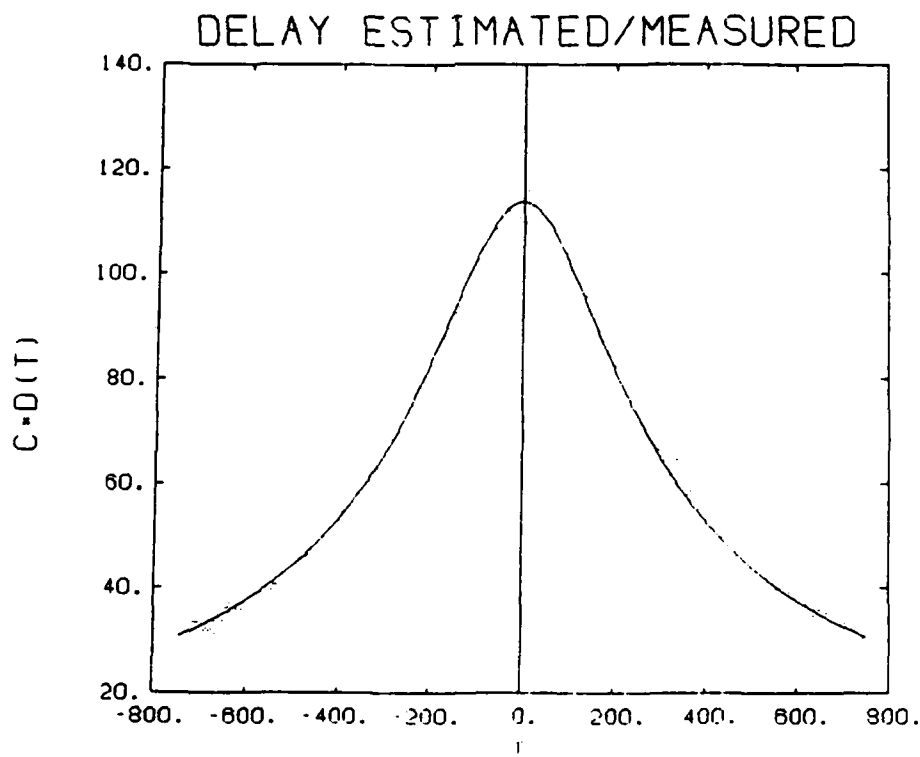


Figure 4.3b The same as 4.3a using $V=10$ m/s in the equation error method. The actual velocity for this example was $V=5$ m/s. Note the similarity between the two estimates.

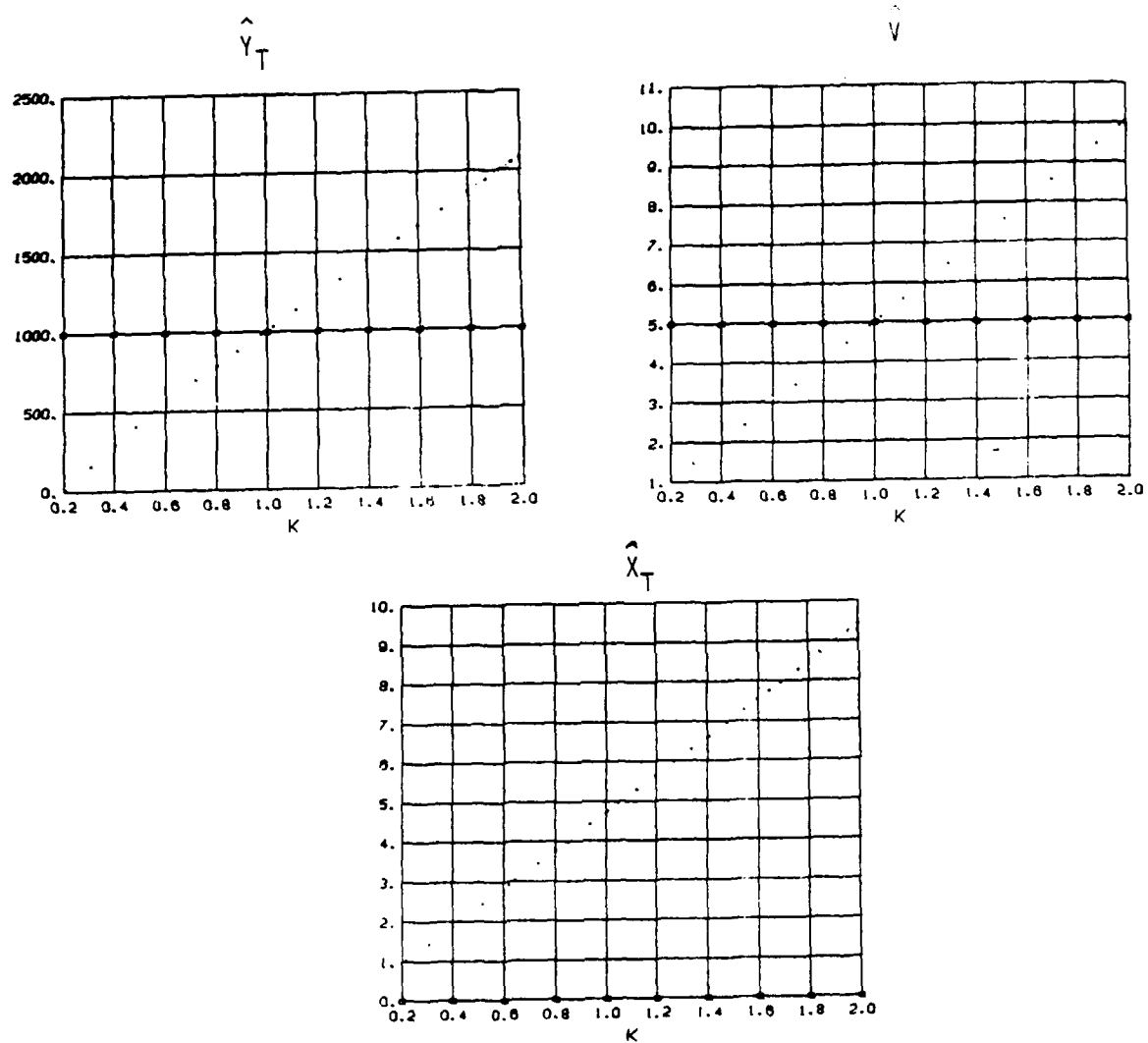
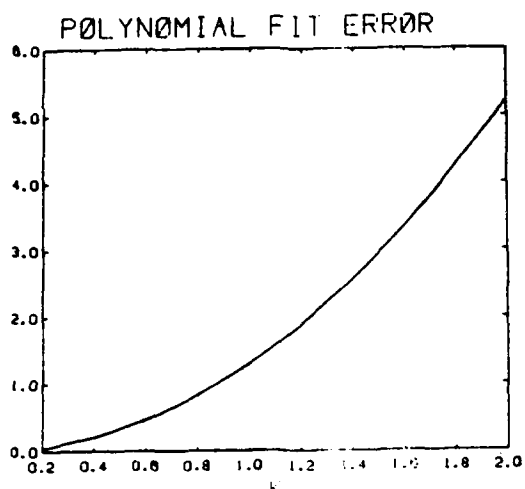
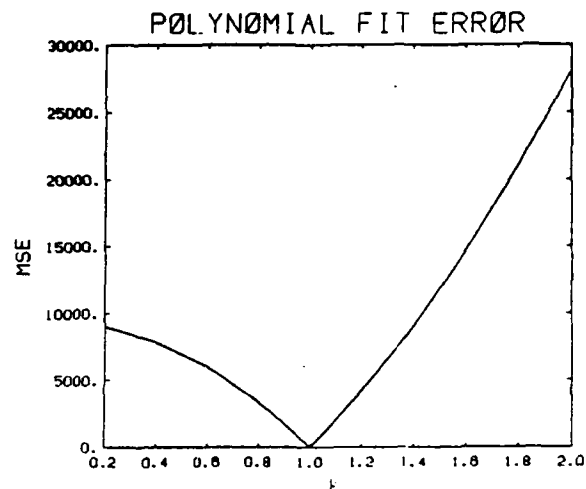


Figure 4.4a Track parameter estimators as functions of $K = \frac{\hat{Z}_T}{Z_T}$ using the transform method. The true track parameter values are marked by squares.



SNR = 20



SNR = ∞

Figure 4.4b The polynomial fit error for SNR's of ∞ , and 20 are plotted here.

other means, the track parameters can be determined by choosing \hat{Z}_T as the one which gives the correct value of V and using \hat{Z}_T to determine the remaining track parameters.

TWO SENSOR EXTENSIONS

When data from two sensors are available, ambiguities in choosing track parameter estimates can sometimes be resolved by looking for consistencies between the two sets of estimates. In a vertical array, delay information alone can determine track parameter estimates when,

$$Y_T \leq 0(10 \cdot |Z_{S1} - Z_{S2}|) \text{ and } \frac{\text{VarD}}{\text{ED}} \leq .1$$

and in a horizontal array when,

$$Y_T \leq 0(10 \cdot |X_{S1} - X_{S2}|) \text{ and } \frac{\text{VarD}}{\text{ED}} \leq .1$$

Both methods were applied to two sensor data satisfying the above constraints. Computer simulation results are given below.

Vertical array

Both methods were used to estimate track parameters from a two sensor vertical array. For the simulations, the sensors were placed at,

Sensor 1: (0,0,300)

Sensor 2: (0,0,100)

with a target at,

Target: (5t, 1000, 200)

and SNR=20.

The equation error method was used to generate track parameter estimates

as functions of V at each sensor. The error in \hat{Y}_T (4.21) is plotted in Figure 4.5 for two different simulations. For this SNR and \hat{Y}_T , the minimum of the error function will occur reasonably near the correct value of V .

Figure 4.6 shows track parameter estimates as functions of Z_T at each sensor. These estimates were generated using the transform method. Figure 4.7 shows CPA to (0,0,0) error, (4.22) as a function of Z_T . Again, for these values of SNR and $Y_T \leq 0(10 \cdot |Z_{S1} - Z_{S2}|)$, the minimum of the error curve will occur near the true value of Z_T .

Note that in the above simulations the inter-sensor delay measurements were not used. Using this information further, estimates of \hat{Y}_T or CPA to (0,0,0) as functions of V or Z_T could be used to lower the variance in determining V or Z_T .

Horizontal Array

Track parameters were estimated based on data from a horizontal array with sensors at

Sensor Locations: $(\pm 150, 0, 300)$

In this case, the track parameters were given by

Target: $V = 5$, $\theta = \pi/4$, $X_T = 0$, $Y_T = 650$, $Z_T = 200$

The equation error method was used to estimate track parameters at each sensor as functions of V . The bearing angle was estimated as a function of V from inter-sensor data also using the equation error method. The error criterion, (4.23) was used to determine the best estimate of V (see Figure 4.8). This error will reliably give good estimates of V , and therefore the remaining track parameters, since the inter-sensor angle estimate is an increasing function of V , whereas the individual sensor estimate of angle is a fairly constant function of V .

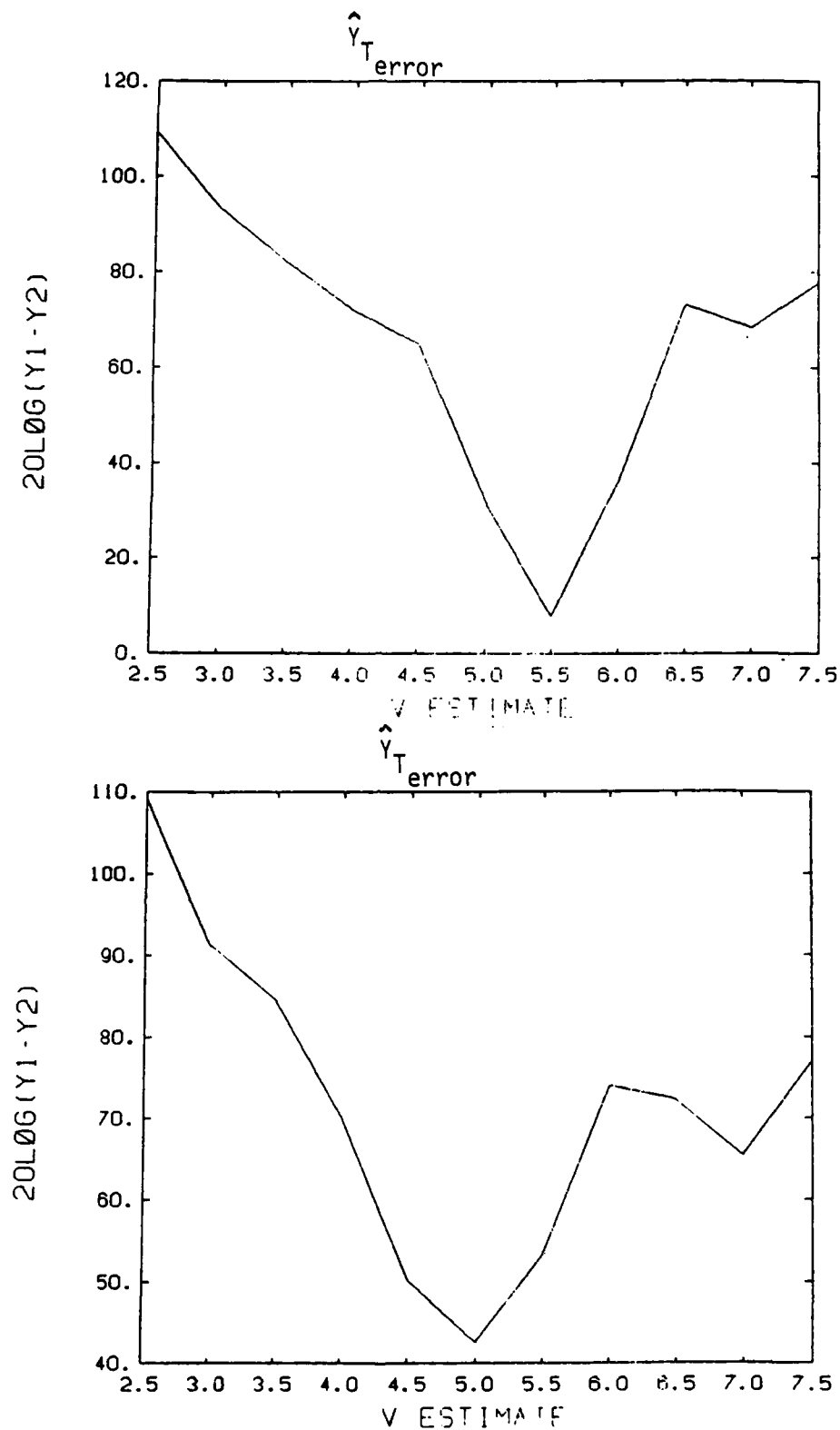
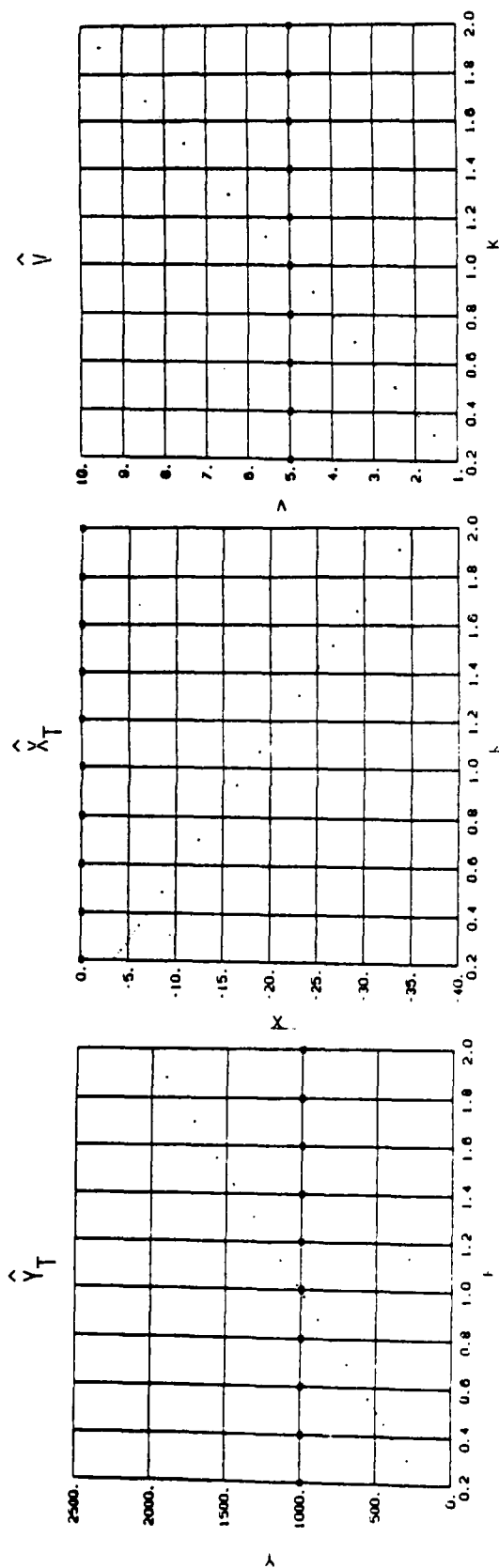
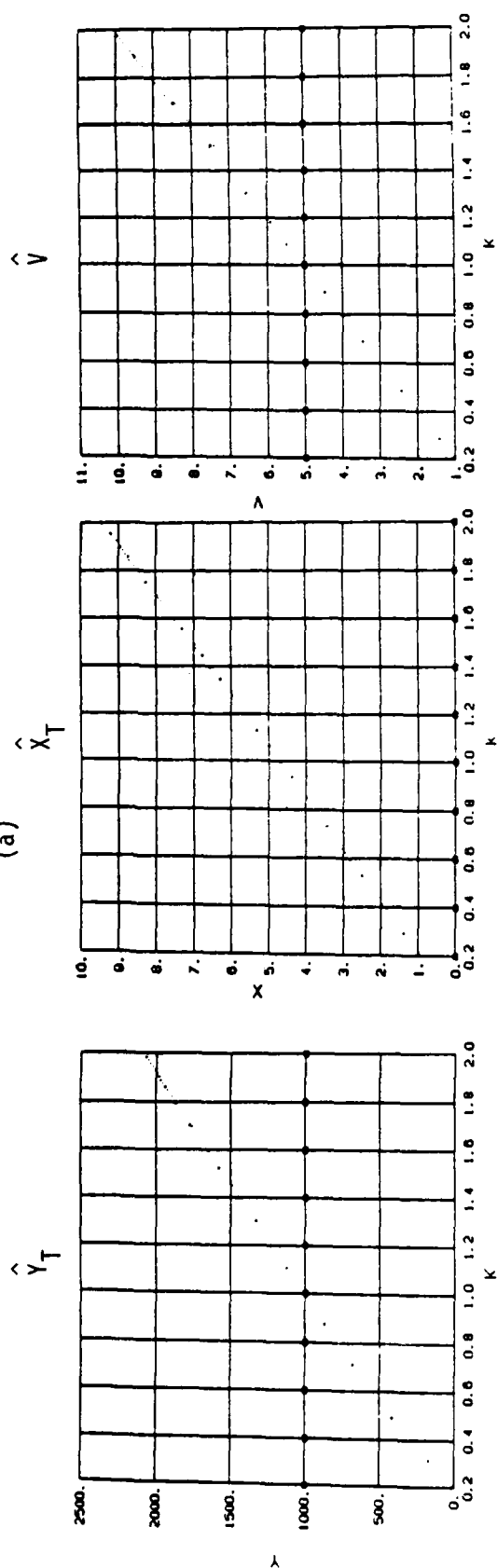


Figure 4.5 Error in \hat{Y}_T , (4.21), as a function of a velocity estimate for two cases. The true value of V is $V=5$ m/s.



(a)



(b)

Figure 4.6a Track parameter estimates as functions of $k = \frac{\hat{Z}_T}{Z_T}$ for sensor 1,
 $Z_{S_1} = 300$ m

Figure 4.6b The same estimates made from sensor 2, $Z_{S_2} = 100$ m .

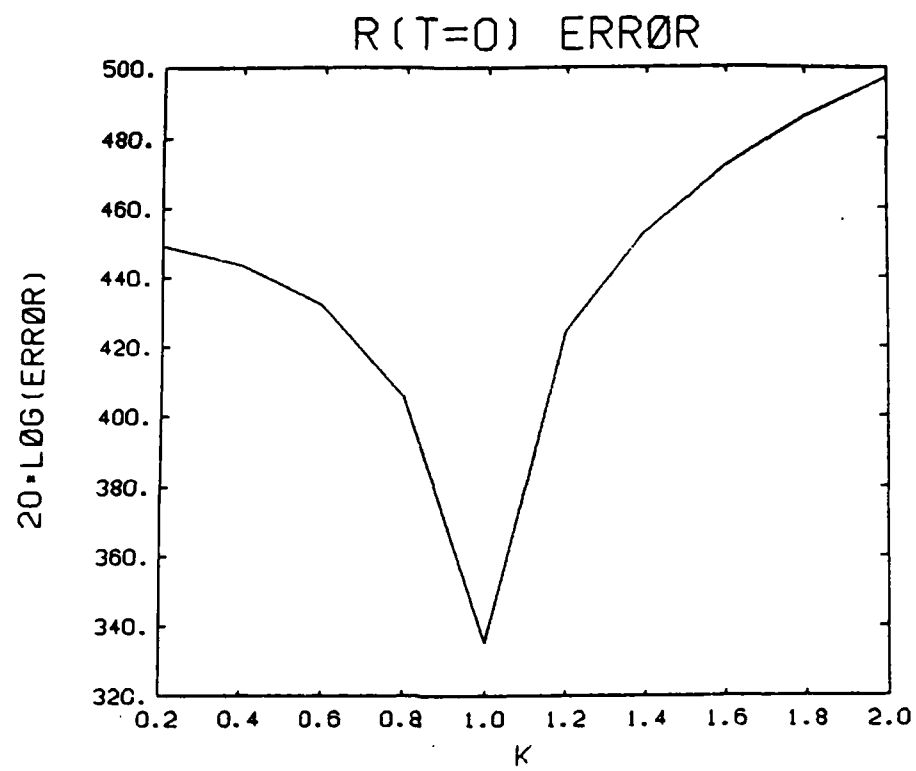


Figure 4.7 CPA error for the estimates shown in Figure 7

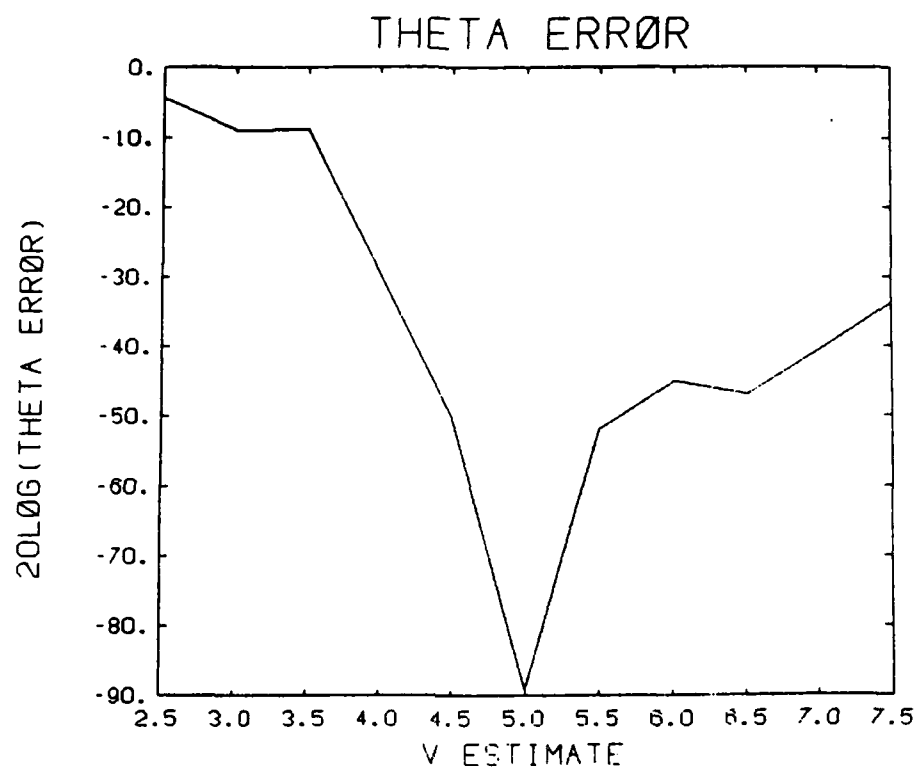


Figure 4.8 The error in θ estimates as a function of velocity estimates based on intersensor and individual sensor estimates. The true velocity is 5 m/s.

REMARKS

In the case of a single sensor in the presence of a multipath reflection, both the equation error method and the transform method yeild accurate results if the velocity or depth are known independently. In the case of a two sensor array, depth or velocity need not be known a priori, but can be chosen using consistency criteria.

5. CONCLUSION

In this report, techniques were developed for extracting track parameter information using sono-bouy data. In the case of a single sensor and a target moving in the presence of a multipath reflection, it was shown that differential delay and doppler information could be obtained and used to find reasonably accurate estimates of the depth, range, and velocity of the target. In the case of two sensors, additional range and velocity estimates can be obtained from intersensor differential delay information. These estimates can be combined to form lower variance estimates of these parameters. Additionally, depending on the sensor locations, further estimates of depth and/or estimates of bearing angle may be found.

As a final note, it is worth mentioning that a significant effort was spent developing software to process sonobouy data. The software developed included correlogram-based TDOA estimators -- SCOT, PHAT, and ML [4], and the ADEC linetracking algorithm. Listings are included in appendix 4. A real data example is presented in appendix 2.

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APPENDIX 1

DIFFERENTIAL DOPPLER EFFECTS ON CORRELATION

Appendix 1: DIFFERENTIAL DOPPLER EFFECTS ON CORRELATION

If two versions of the same signal have relative doppler shifts, the peak of the resulting cross correlation will be reduced compared to that of the cross correlation of the signals without a relative doppler shift. This decorrelation causes fading of correlogram lines near CPA, where differential doppler is greatest.

To examine this effect, assume $X(t)$ is a zero mean, gaussian bandpass process, with bandwidth B , and center frequency F_0 . The autocorrelation of X is given by

$$R_X(\tau) = R_0 \frac{\sin \pi B \tau}{\pi B \tau} \cos 2\pi \tau \quad (A1.1)$$

The mean correlation output, μ , of the signal $X(t)$ with itself is given by

$$\begin{aligned} \mu &= E\left\{\frac{2}{T} \int_0^{\frac{T}{2}} X(t)X(t)dt\right\} \\ \mu &= R_0 \end{aligned} \quad (A1.2)$$

The mean correlator output, μ of the signal $X(t)$ with its doppler shifted version is given by

$$\mu = E\left\{\frac{2}{T} \int_0^{\frac{T}{2}} X(t)X(\alpha t)dt\right\} \quad (A1.3)$$

which is not in general as large as R_0 .

Interchanging expectation and integration, and substituting (A1.1) for $E(X(t)X(t+\tau))$,

$$\mu = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} R_0 \frac{\sin \pi B |1-\alpha|t}{\pi B |1-\alpha|t} \cos 2\pi f_0 |1-\alpha|t dt \quad (A1.4)$$

$$\frac{\mu}{R_0} = \frac{1}{\pi B T |1-\alpha|} \int_0^{\frac{\pi B T |1-\alpha|}{2}} \frac{\sin X}{X} \cos \frac{2f_0}{B} X \, dX$$

$$\frac{\mu}{R_0} = \frac{1}{\pi B T |1-\alpha|} \left[\text{sinc}\left(\frac{\pi B T |1-\alpha|}{2} \left(\frac{2f_0}{B} + 1\right)\right) - \text{sinc}\left(\frac{\pi B T |1-\alpha|}{2} \left(\frac{2f_0}{B} - 1\right)\right) \right] \quad (A1.5)$$

Plots of mean correlator output as a function of doppler shift appear in Fig. (A1.1). Figure (A1.2) is a plot of a typical doppler history for a target moving in a straight line by an array. Several features are easily seen in Figure (A1.1). First, as the relative doppler shift increases, the correlator output decreases. Second, as integration time increases, the correlator output decreases. Finally, as the bandwidth of the signal increases relative to the center frequency, the correlator output increases.

The performance of the correlation method of time delay estimation is greatly effected by nonzero differential doppler. Fortunately, due to the relatively slow speeds of submarines, differential doppler is only likely to cause problems except near the time of CPA. See, for instance, Figure A2.1.

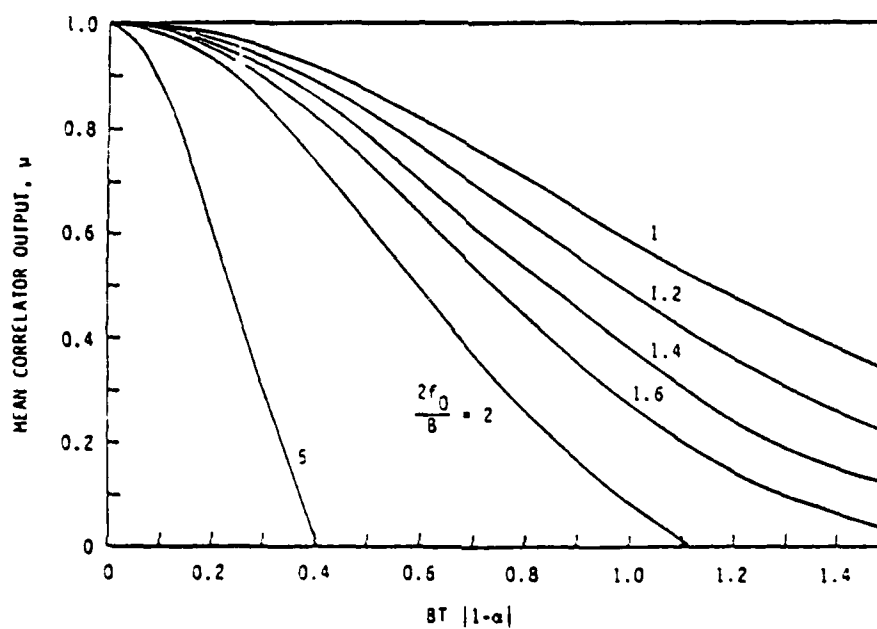


Figure A1.1 Mean correlator output as a function of doppler shift, α . f_0 is the center frequency, and β is the bandwidth of the input process. T is the integration time.

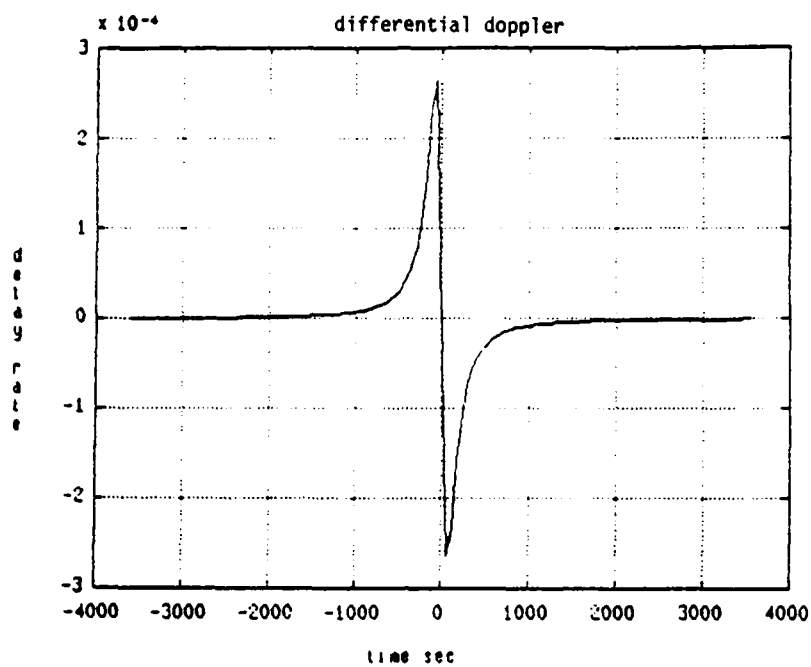


Figure A1.2 Example of the doppler history of a target passing by a sensor. CPA occurs at $t=0$.

APPENDIX 2

REAL DATA EXAMPLE

Appendix 2: REAL DATA EXAMPLE

This appendix presents an example of track parameter estimation from a real data set taken from a horizontal array. The track parameter estimation techniques described in Chapter 3 will be used. In this case, θ , V , Z_t and R_{CPA} will be estimated from the data and knowledge of the sensor locations.

The data was taken from an array with sensors located at ($\pm 136m$, 0, 308m). Figure A2.1 shows R_{11} , R_{12} , and R_{22} , the correlograms formed using the correlation method of time delay estimation. R_{11} and R_{22} have been energy normalized so that $r_i(0) = 1 \forall_i$; R_{12} has been SCOT normalized [4]. As the data set was of exceptional quality, the differential delay information needed for track parameter estimation can be measured without further processing. The immediately measurable parameters are listed below:

$$D_{12}(|t| \rightarrow \infty) \sim .187 \text{ sec} \quad (A2.1)$$

$$\left. \frac{\partial D_{12}(t)}{\partial t} \right|_{t: D_{12}(t)=0} \sim \left(\frac{.5 \text{ sec}}{200 \text{ sec}} \right) = .0025$$

$$t_{R_{CPA_1}} - t_{R_{CPA_2}} \sim 35 \text{ sec}$$

$$D_1(0) \sim .076 \text{ sec}$$

$$D_2(0) \sim .074 \text{ sec}$$

$$\hat{\rho}_1 \sim 4.9$$

$$\hat{\rho}_2 \sim 5.1$$

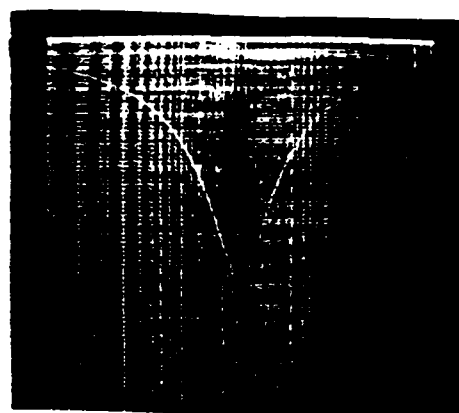
The relevant equations from the text are as follows:

$$\cos \theta = \frac{CD(|t| \gg 1)}{2X_s} \quad (A2.2)$$

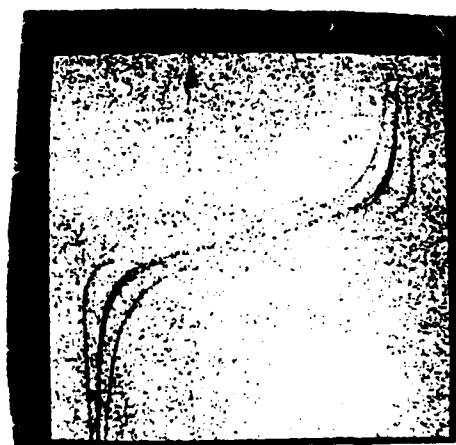
$$\frac{Z_T}{V} = \hat{\rho} \frac{C}{2Z_s} \quad (A2.3)$$



SENSOR 1



SENSOR 2



SCOT NORMALIZED
CROSS-CORRELOGRAM

Figure A2.1 Correlograms for sensor 1, sensor 2, and the SCOT normalized correlogram between sensor 1 and sensor 2.

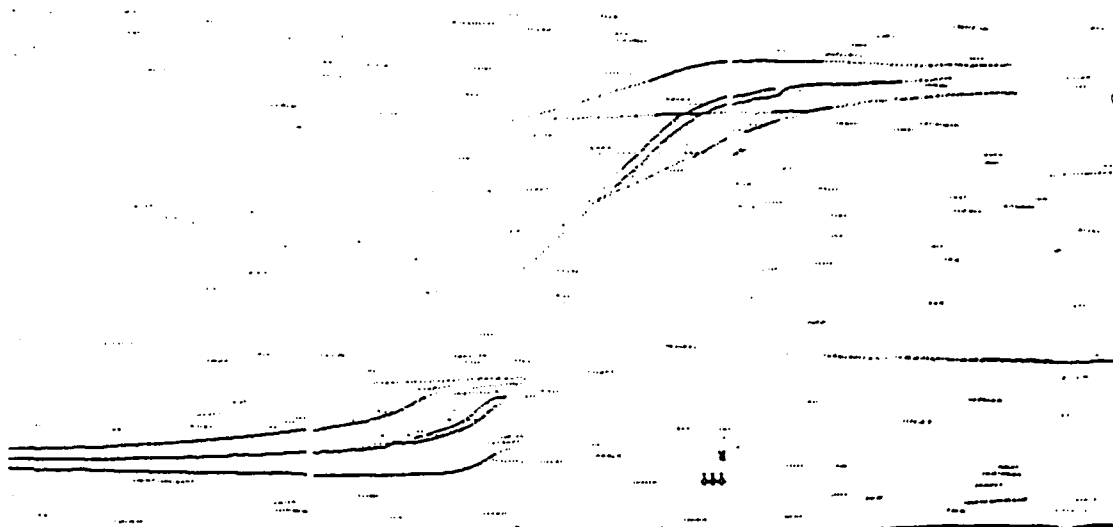


Figure A2.2 Example of the ADEC line tracking algorithm
run on the SCOT normalized cross-correlogram

$$R_{CPA} = \frac{2Z_S Z_T}{CD(0)} - \frac{CD(0)}{2} \quad (A2.4)$$

$$V = \frac{2X_S}{\cos \theta} \cdot \frac{1}{t_{R_{CPA_1}} - t_{R_{CPA_2}}} \quad (A2.5)$$

$$Y_C = \left[X_S^2 \left[\left(\frac{2V \cos \theta}{CD_{12}} \right)^2 - 1 \right] - (Z_T - Z_S)^2 \right]^{-1/2} \quad (A2.6)$$

$\frac{\partial}{\partial t} \Big|_{t: D_{12}(t)=0}$

Using (A2.2), one finds,

$$\cos \theta \sim 1, \theta \sim 0 \quad (A2.7)$$

Noting that the values of $D_1(0)$ and $D_2(0)$ are very close, and are related to R_{CPA} by (A2.4), the CPA ranges at sensors 1 and 2 will be similar, confirming the 0° bearing angle estimate.

If a 0° bearing angle is assumed, (A2.2) gives

$$C \sim 1450 \text{ m/s} \quad (A2.8)$$

with knowledge of C and θ , V can be estimated from (A2.5),

$$V \sim 7.7 \text{ m/s} = 14 \text{ KTS} \quad (A2.9)$$

Assuming Z_T is constant, the two estimates of $\hat{\rho}$ can be combined giving, from (A2.3),

$$Z_T \sim 92 \text{ m} \quad (A2.10)$$

Using the above value of Z_T , R_{CPA} for each of the sensors can be calculated with (A2.4)

$$R_{CPA_1} \sim 455 \text{ m} \quad (A2.11)$$

$$R_{CPA_2} \sim 470 \text{ m}$$

The Y-axis crossing can be estimated using (A2.6),

$$Y_C = 510 \text{ m} \quad (\text{A2.12})$$

Note that since $\theta \sim 0$, $Y_C \sim R_{CPA_{12}}$, and therefore the value of Y_C is consistent with the values of R_{CPA_1} and R_{CPA_2} .

From this real data set, a group of self-consistent track parameter values have been obtained using various easily measured quantities. Note that in this case, the value of $\theta \sim 0$ made it difficult to determine X_C (through (55)). Consequently, additional estimates of θ , V and R_{CPA} were not obtainable.

APPENDIX 3
ACCURACY OF DEPTH ESTIMATION IN A MULTIPATH ENVIRONMENT

ACCURACY OF DEPTH ESTIMATION IN A MULTIPATH ENVIRONMENT

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ABSTRACT

The problem of estimating the depth of an underwater source from acoustic measurements is considered. The Cramer-Rao bound on the variance of the depth estimate is evaluated for the cases of one and two sensors. The effect of multipath on estimation accuracy is investigated.

This work was supported by the Office of Naval Research under Contract No. N00014-84-C-0408.

1. INTRODUCTION

The problem of estimating the depth of an underwater source is of considerable interest in various surveillance applications. Given measurements from a vertical acoustic array it is possible to estimate the angle of arrival of the signal. From this estimate and knowledge of the distance to the source it is possible to estimate its depth. If the source range is not known it can be estimated from the curvature of the wavefront at the array.

Multipath propagation is a common effect in the transmission of acoustic waves in water. The presence of multipath propagation is usually considered to be an undesirable effect which complicates the processing of the acoustic signals in localization and detection problems. However, in some circumstances the presence of multipath can be quite useful.

As an example consider the case of depth estimation when only a single sensor is available. In the absence of multipath the measurements provided by the sensor contain no information about the location of the source. However, if multipath is present, the delay between the signals propagating in the direct and the secondary paths contain information about the depth of the source. In the presence of multipath it is, therefore, possible to estimate source depth, while in its absence this is not possible.

In this paper we study the accuracy of source depth estimation both in the presence and in the absence of multipath, for the case of one and two sensors. These results can be extended in a straightforward manner to an arbitrary number of sensors.

The Cramer-Rao bound (CRB) is used to evaluate estimation accuracy. The CRB specifies the best possible accuracy achievable by any unbiased estimator [1]. In the case of stationary Gaussian processes, the CRB can be evaluated by a simple frequency domain formula as the number of observations becomes large [2]. This simplified formula has been applied to the estimation of inter-sensor time delay, and single-sensor multipath delay [3]. The purpose of this study is to extend previous work to include multipath effects in the

two-sensor case. The main question is how much better can depth be estimated when both multipath and inter-sensor time delay information are used by the estimator.

Four cases are defined to show a progression from the single-sensor case to the two-sensor case:

- (1) Single-sensor case with multipath. The multipath delay is used to estimate depth.
- (2) Two-sensor case, no multipath. The inter-sensor time delay is used to estimate depth.
- (3) Two-sensor case with multipath. In this case both inter-sensor delay and multipath information are used to estimate depth.
- (4) Two-sensor case with multipath and unknown range. When range is not known, the combination of inter-sensor delay and multipath delays suffice to determine both range and depth. The CRB for this case is also presented.

Examples are provided in each case to illustrate the performance bounds as function of system parameters.

2. ESTIMATING DEPTH FROM SINGLE-SENSOR MULTIPATH INFORMATION

The single-sensor multipath case is depicted in Figure 1. The received signal $s(t)$ can be expressed as

$$s(t) = x(t) + gx(t-D_1) + e(t) \quad (1)$$

where $x(t)$ is the signal received by direct propagation from the source to the sensor, $e(t)$ is uncorrelated measurement noise, and $gx(t-D_1)$ is the attenuated and delayed version of the source signal arising from a surface bounce. The corresponding power spectral density (PSD) function at the sensor is given by

$$\begin{aligned} S_s(\omega) &= S_x(\omega) \left| 1 + ge^{-j\omega D_1} \right|^2 + S_e(\omega) \\ &= S_x(\omega) [(1+g^2) + 2g\cos(\omega D_1)] + S_e(\omega), \end{aligned} \quad (2)$$

for ω in the range $[-W, W]$, where $W = 2\pi B$, and B is the bandwidth in Hz.

In terms of the geometry (see figure 1), the multipath delay is given by

$$D_1 = \frac{1}{c} \{ [y^2 + (z+z_1)^2]^{1/2} - [y^2 + (z-z_1)^2]^{1/2} \}, \quad (3)$$

where c is the speed of sound. Thus, assuming the range y and sensor-depth z_1 are known, the source-depth z is determined by the multipath delay D_1 .

Using Whittle's formula [2], the CRB for the variance of the depth estimate is given by

$$\begin{aligned} & \left[\frac{N}{2} \cdot \frac{1}{2W} \int_{-W}^W \frac{\left[\frac{\partial S(\omega)}{\partial D_1} \right]^2}{S^2(\omega)} d\omega \left(\frac{\partial D_1}{\partial z} \right)^2 \right]^{-1} \\ &= \left[\frac{N}{2} \cdot \frac{1}{2W} \int_{-W}^W \frac{[-2g\omega \sin \omega D_1]^2}{S^2(\omega)} d\omega \right]^{-1} \left(\frac{\partial z}{\partial D_1} \right)^2 \end{aligned}$$

$$= \text{CRB}(D_1) \left(\frac{\partial z}{\partial D_1} \right)^2, \quad (4)$$

where N is the number of independent observation intervals. (In continuous time, the observation time is defined as $T=N/2B$. In discrete time, when B equals half the sampling rate, N is the number of sampled observations.) Equation (4) can be interpreted as a generalized form of the CRB, see [4].

2.1 SPECIAL CASES

When the PSD of $x(t)$ and $e(t)$ are constant for $|\omega| \leq W$, and zero for $|\omega| > W$, with the signal-to-noise-ratio (SNR) defined as S_x/S_e , we have the following approximations (see [3],[5]):

(i) $WD_1 \gg 1$, $\text{SNR} \ll 1$

$$\text{CRB}(D_1) = \frac{3\pi}{TW^3g^2} \frac{1}{\text{SNR}^2} = \frac{3}{NW^2g^2} \frac{1}{\text{SNR}^2}. \quad (5)$$

(ii) $WD_1 \gg 1$, $\text{SNR} \gg 1$

$$\text{CRB}(D_1) = \frac{3\pi(1-g^2)}{TW^3g^2}, \quad (6)$$

which is independent of SNR.

(iii) $WD_1 \ll 1$

$$\text{CRB}(D_1) = \frac{3\pi}{TW^3} \frac{[(1+g)^2\text{SNR}+1]}{g^2\text{SNR}^2} \cdot \frac{1}{1.2W^2D_1^4}. \quad (7)$$

Note that the CRB depends on the multipath delay D_1 for small delay-bandwidth product WD_1 , but not for $WD_1 \gg 1$.

When the range to the source is large compared to the depths of the source and sensor, the derivative $\frac{\partial z}{\partial D_1}$ has a simple form:

$$\frac{\partial z}{\partial D_1} = \frac{cy}{\partial z}, \quad z, z_1 \ll y. \quad (8)$$

Note that the variance of the depth estimate is inversely proportional to

$(2z/y)^2$, where $(2z/y)$ is approximately the angle between the source and its "reflection", as viewed from the sensor.

2.2 EXAMPLES

Figure 2 shows a specific scenario for which the CRB was evaluated. Figures 3, 4, and 5 display the normalized Cramer-Rao bound, $\text{CRB}(z)/z^2$ as a function of SNR, for delay-bandwidth products $BD_1 = 0.1, 1, \text{ and } 10$, respectively. For the geometry in Figure 2, these time-bandwidth products correspond to bandwidths $B = 3.78, 37.78, \text{ and } 377.78$, respectively. Each figure shows three different values of g : $g = -0.1, -0.5, \text{ and } -0.90$. As expected, increased reflection magnitude $|g|$ improves the ability to estimate z , as does increased delay-bandwidth product.

3. ESTIMATING DEPTH FROM INTER-SENSOR DELAY

Figure 6 shows the general case of two sensors configured in a vertical array at depths z_1 and z_2 , respectively. In this section multipath is assumed absent. The inter-sensor delay, i.e., the time-difference of arrival (TDOA) between sensors 1 and 2, is defined as

$$D_{12} = \frac{1}{c} [y^2 + (z-z_1)^2]^{1/2} - [y^2 + (z-z_2)^2]^{1/2} . \quad (9)$$

The respective received signals are given by (analogous to (1)),

$$\begin{aligned} s_1(t) &= x(t) + e_1(t) , \\ s_2(t) &= x(t-D_{12}) + e_2(t) . \end{aligned} \quad (11)$$

where $e_1(t)$ and $e_2(t)$ are assumed to be uncorrelated. The power spectral density of the 2-vector process $s(t) = [s_1(t), s_2(t)]^T$ is equal to

$$S(\omega) = \begin{bmatrix} S_x(\omega) + S_{e_1}(\omega) & S_x(\omega) e^{j\omega D_{12}} \\ S_x(\omega) e^{-j\omega D_{12}} & S_x(\omega) + S_{e_2}(\omega) \end{bmatrix} . \quad (12)$$

For the vector case, the asymptotic form of the CRB for the covariance of the parameter estimates θ becomes [2],

$$\begin{aligned} \text{Cov}(\theta) &> J^{-1} , \quad J = [J_{ij}] , \\ J_{ij} &= \frac{T}{4\pi} \int_{-W}^W \text{tr} \{ S^{-1}(\omega) \frac{\partial S(\omega)}{\partial \theta_i} S^{-1}(\omega) \frac{\partial S(\omega)}{\partial \theta_j} \} d\omega , \end{aligned} \quad (13)$$

where $\text{tr}(A)$ denotes the trace of the matrix A . The CRB for D_{12} is then given by

$$\begin{aligned} \text{CRB}(D_{12}) &= \left[\frac{T}{4\pi} \int_{-W}^W \text{tr} \left[S^{-1}(\omega) \frac{\partial S(\omega)}{\partial D_{12}} \right]^2 d\omega \right]^{-1} \\ &= \left[\frac{T}{2\pi} \int_{-W}^W \frac{\omega^2 \text{SNR}^2}{1+2\text{SNR}} d\omega \right]^{-1}, \end{aligned} \quad (14)$$

and the CRB for depth z is given by

$$\text{CRB}(z) = \text{CRB}(D_{12}) \left(\frac{\partial z}{\partial D_{12}} \right)^2. \quad (15)$$

3.1 SPECIAL CASES

If the noise and signal PSD functions are assumed flat in $[-W, W]$ and zero elsewhere, then

$$\text{CRB}(D_{12}) = \frac{3\pi}{W^3 T} \frac{1+2\text{SNR}}{\text{SNR}^2}. \quad (16)$$

For $\text{SNR} \ll 1$ and $WD_{12} \gg 1$, we have (comparing with (5))

$$\frac{\text{CRB}(D_{12})}{\text{CRB}(D_1)} = g^2. \quad (17)$$

At long ranges, $y \gg z$, z_1, z_2 , we have (cf. (8))

$$\frac{\partial z}{\partial D_{12}} = \frac{cy}{z_2 - z_1} \quad (18)$$

Thus,

$$\frac{\text{CRB}(z) [\text{two-sensors, no multipath}]}{\text{CRB}(z) [\text{one-sensor, multipath-only}]} = (2z)^2 \cdot \frac{g^2}{(z_2 - z_1)^2} \quad (19)$$

When $g=0$ or $z=0$, no depth information is obtained in the single-sensor multipath case, while for $z_1 = z_2$, no depth information is available in the TDOA case. These facts are, of course, to be expected.

3.2 EXAMPLES

Figure 7 shows the normalized CRB, $\text{CRB}(z)/z^2$, as a function of SNR for three different signal bandwidths $B = 3.78$, 37.78 , and 377.78 . The geometry is the same as in the single-sensor case (figure 2) with the second sensor being located at $z_2 = 400$. The three curves may be compared with the results in figures 3, 4, and 5, respectively. Figure 8 shows the effect of varying the geometry, using $B = 377.8$ Hz and $z_2 = 220, 400$, and 600 .

4. ESTIMATING DEPTH FROM BOTH MULTIPATH AND INTER-SENSOR DELAYS

Figure 9 shows the geometry for the two-sensor case in which both multipath and inter-sensor delays are to be estimated. The two multipath delays are given by

$$\begin{aligned} D_1 &= \frac{1}{c} \left([y^2 + (z+z_1)^2]^{1/2} - [y^2 + (z-z_1)^2]^{1/2} \right), \\ D_2 &= \frac{1}{c} \left([y^2 + (z+z_2)^2]^{1/2} - [y^2 + (z-z_2)^2]^{1/2} \right), \end{aligned} \quad (20)$$

and the TDOA is again equal to (cf. (10))

$$D_{12} = \frac{1}{c} \left([y^2 + (z-z_1)^2]^{1/2} - [y^2 + (z-z_2)^2]^{1/2} \right). \quad (21)$$

The received signals at sensors 1 and 2 are given by

$$\begin{aligned} y_1(t) &= x(t-\tau_{11}) + gx(t-\tau_{21}) + e_1(t), \\ y_2(t) &= x(t-\tau_{12}) + gx(t-\tau_{22}) + e_2(t), \end{aligned} \quad (22)$$

where

$$\begin{aligned} D_1 &= \tau_{21} - \tau_{11}, \\ D_2 &= \tau_{12} - \tau_{22}, \\ D_{12} &= \tau_{11} - \tau_{12}. \end{aligned} \quad (23)$$

The PSD matrix is (cf. (2) and (12))

$$S(\omega) = \begin{bmatrix} S_x(1+g^2+2g\cos\omega D_1) & S_x e^{-j\omega D_{12}}(1+ge^{-j\omega D_1})(1+ge^{-j\omega D_2}) \\ S_x e^{j\omega D_{12}}(1+ge^{j\omega D_1})(1+ge^{j\omega D_2}) & S_x(1+g^2+2g\cos\omega D_2) \end{bmatrix}. \quad (24)$$

The CRB for depth estimation is then

$$\text{CRB}(z) = \left[\frac{T}{4\pi} \int_{-W}^W J(\omega) d\omega \right]^{-1}, \quad (25)$$

where

$$J(\omega) = \left[S^{-1}(\omega) \frac{\partial S(\omega)}{\partial z} \right]^2,$$

$$S(\omega) = \begin{bmatrix} S_1(\omega) & S_{12}(\omega) \\ S_{12}^*(\omega) & S_2(\omega) \end{bmatrix},$$

$$\frac{\partial S(\omega)}{\partial z} \triangleq \dot{S}(\omega) = \begin{bmatrix} \dot{S}_1(\omega) & \dot{S}_{12}(\omega) \\ \dot{S}_{12}^*(\omega) & \dot{S}_2(\omega) \end{bmatrix}, \quad (26)$$

and

$$\begin{aligned} S_1(\omega) &= S_x(\omega) [1 + g_1^2 + 2g_1 \cos \omega D_1] + S_{e_1}(\omega), \\ S_2(\omega) &= S_x(\omega) [1 + g_2^2 + 2g_2 \cos \omega D_2] + S_{e_2}(\omega), \\ S_{12}(\omega) &= S_x(\omega) e^{-j\omega D_{12}} (1 + g_1 e^{-j\omega D_1}) (1 + g_2 e^{-j\omega D_2}), \end{aligned} \quad (27)$$

$$\dot{S}_1(\omega) = \frac{\partial S_1(\omega)}{\partial z} = 2g_1 S_x \omega \sin(\omega D_1) \left[\frac{z+z_1}{\tau_{21}} - \frac{z-z_1}{\tau_{11}} \right] \frac{1}{c^2},$$

$$\dot{S}_2(\omega) = \frac{\partial S_2(\omega)}{\partial z} = 2g_2 S_x \omega \sin(\omega D_2) \left[\frac{z+z_2}{\tau_{22}} - \frac{z-z_2}{\tau_{12}} \right] \frac{1}{c^2},$$

$$\dot{S}_{12}(\omega) = \frac{\partial S_{12}(\omega)}{\partial z} = j\omega S_x e^{-j\omega D_{12}}$$

$$\cdot \left[(1 + g_1 e^{-j\omega D_1}) \left(\frac{z-z_2}{\tau_{12}} \right) + g_2 e^{-j\omega D_2} (1 + g_1 e^{-j\omega D_1}) \left(\frac{z+z_2}{\tau_{22}} \right) \right]$$

$$-\left(1+g_2 e^{-j\omega D_2}\right)\left(\frac{z-z_1}{\tau_{11}}\right) - g_1 e^{-j\omega D_1}\left(1+g_2 e^{-j\omega D_2}\right)\left(\frac{z+z_1}{\tau_{21}}\right) \frac{1}{c^2} \right]. \quad (28)$$

4.1 EXAMPLES

(i) Different Bandwidths, $B=3.78, 37.78, 377.78$

Figures 10, 11, and 12 show the normalized CRB, $\text{CRB}(z)/z^2$, for the three delay-bandwidth cases seen in the previous examples. The case of $g=0$ in each figure is precisely the CRB curve obtained in the previous section for TDOA based depth estimation (no multipath). Note that use of multipath delay estimates can improve the relative variance in the depth estimate by 10 to 15 dB when the multipath is strong.

(ii) Changing Geometry

Figures 13, 14, 12, 15 show a sequence of CRB curves in which the second sensor is taken deeper and deeper, i.e., $z_2 = 200, 220, 400, 600$. All are at the large bandwidth $B = 377.78$. In figure 13, the $g=0$ curve is at infinity because for $z_1 = z_2$ and $g = 0$ there is no TDOA or multipath information on which to base a depth estimate. We find that increasing the depth of sensor 2 improves the bound. There is more improvement near $g=0$ than near $g=-0.9$ indicating that it is the TDOA component that is benefiting from increased z_2 . This is reasonable in view of equations (8) and (18) which show that at long range, the derivative of z with respect to TDOA depends strongly on $z_2 - z_1$ while the sensitivity to multipath delay does not.

5. ESTIMATING DEPTH AND RANGE FROM MULTIPATH AND INTER-SENSOR DELAYS

In the single-sensor case, it has been shown [6] that, assuming the range error is uncorrelated with the multipath delay error, the variance of the depth estimate becomes a sum of two terms involving the respective variances of range and delay:

$$\text{Var}(z) = \left(\frac{\partial z}{\partial D_1}\right)^2 \text{Var}(D_1) + \left(\frac{\partial z}{\partial y}\right)^2 \text{Var}(y) , \quad (29)$$

where the sensitivity of y to z is defined for fixed D_1 :

$$\frac{\partial z}{\partial y} = \frac{cD_1}{2z_1} \quad (30)$$

At long range ($z, z_1 \ll y$), we may use (8) to obtain

$$\frac{\text{Var}(z)}{z^2} = \frac{\text{Var}(D_1)}{D_1^2} + \frac{\text{Var}(y)}{y^2} \quad (31)$$

For two sensors with no multipath (TDOA only), a similar situation is obtained.

In the case of two sensors with multipath it is possible to estimate both range and depth. An interesting question is the following: how much is depth estimation accuracy effected by the lack of knowledge of the range? To answer this question we evaluate the CRB on the covariance matrix of the estimate of the parameter vector $[z, y]^T$. Using Whitte's formula we note that

$$\text{CRB}\{[z, y]^T\} = \begin{bmatrix} J_{zz} & J_{zy} \\ J_{yz} & J_{yy} \end{bmatrix}^{-1} , \quad (32)$$

where (cf. (25)),

$$J_{zz} = \frac{T}{4\pi} \int_{-\infty}^{\infty} \left[S(\omega)^{-1} \frac{\partial S(\omega)}{\partial z} \right] \left[S(\omega)^{-1} \frac{\partial S(\omega)}{\partial z} \right]^* d\omega , \quad (33a)$$

and

$$J_{zy} = J_{yz}^* = \frac{T}{4\pi} \int_{-\infty}^{\infty} [S(\omega)^{-1} \frac{\partial S(\omega)}{\partial z}] [S(\omega)^{-1} \frac{\partial S(\omega)}{\partial y}] d\omega, \quad (33b)$$

$$J_{yy} = \frac{T}{4\pi} \int_{-\infty}^{\infty} [S(\omega)^{-1} \frac{\partial S(\omega)}{\partial y}] [S(\omega)^{-1} \frac{\partial S(\omega)}{\partial y}] d\omega. \quad (33c)$$

The matrices $S(\omega)$ and $\frac{\partial S(\omega)}{\partial z}$ are defined in equations (25)-(26), while

$$\frac{\partial S(\omega)}{\partial y} = \begin{bmatrix} \frac{\partial S_1(\omega)}{\partial y} & \frac{\partial S_{12}(\omega)}{\partial y} \\ \frac{\partial S_{21}(\omega)}{\partial y} & \frac{\partial S_2(\omega)}{\partial y} \end{bmatrix} \quad (34)$$

where

$$\frac{\partial S_1(\omega)}{\partial y} = 2g_2 S_{x\omega} \sin(\omega D_1) \left[\frac{1}{\tau_{21}} - \frac{1}{\tau_{11}} \right] \frac{1}{c^2} \quad (35)$$

$$\frac{\partial S_2(\omega)}{\partial y} = 2g_2 S_{x\omega} \sin(\omega D_2) \left[\frac{1}{\tau_{22}} - \frac{1}{\tau_{12}} \right] \frac{y}{c^2}$$

$$\begin{aligned} \frac{\partial S_{12}(\omega)}{\partial y} &= \frac{\partial S_{21}^*(\omega)}{\partial y} = j\omega S_x e^{-j\omega D_{12}} \cdot \left[(1+g_1 e^{-j\omega D_1}) \frac{1}{\tau_{12}} \right. \\ &\quad + g_2 e^{-j\omega D_2} (1+g_1 e^{-j\omega D_1}) \frac{1}{\tau_{22}} - (1+g_2 e^{-j\omega D_2}) \frac{1}{\tau_{11}} \\ &\quad \left. - g_1 e^{-j\omega D_1} (1+g_2 e^{-j\omega D_2}) \frac{1}{\tau_{21}} \right] \frac{y}{c^2} \end{aligned}$$

Examples

Figures 16, 17, and 18 show the normalized CRB, $CRB(z)/z^2$, for the three bandwidths considered in the previous examples ($BD_1 = 0.1, 1, 10$). In this particular geometry, the TDOA component of the depth estimate is independent of the range due to the hyperbola of constant TDOA degenerating to a straight line. Consequently, for $g=0$, the CRB curves reduce to the TDOA-only case of figure 7. Note that at small BD_1 , the presence of multipath only makes the estimates worse, while at intermediate and high BD_1 , the depth estimate is improved by multipath.

Figure 19 shows the results at high BD_1 for a different geometry ($z_2=600$ instead of 400). In this case the TDOA component of the depth estimate depends on range. This figure compares with figure 18. In the non-degenerate geometry, the unknown range adds significantly to the uncertainty in depth.

6. DISCUSSION

The performance analysis presented in this paper shows the potential usefulness of multipath information in enhancing the accuracy of depth estimation. The results presented here are asymptotic, and need to be verified by finite data simulations. Two related issues of practical interest are:

(i) The Case of Unknown g

The earlier analysis assumed perfect knowledge of the reflection coefficient g . When g is unknown, it can be estimated from the data. In [6] we have shown for the examples considered here that the asymptotic accuracy of depth estimation is not affected by the need to estimate g , provided that $WD \gg 1$, where

$$D = \max\{D_1, D_2, D_{12}\}.$$

(ii) The Case of Unknown SNR

Similarly to the case of unknown g , it can be shown [6] that the need to estimate SNR does not affect the asymptotic depth estimation accuracy, provided that $WD \gg 1$.

Finally, we note that these results can be extended in a straightforward manner to the case of M sensors. In this case $S(\omega)$ and $\hat{S}(\omega)$ will be $M \times M$ matrices. The entries of these matrices can be easily evaluated by obvious extrapolation from the case of $M=2$.

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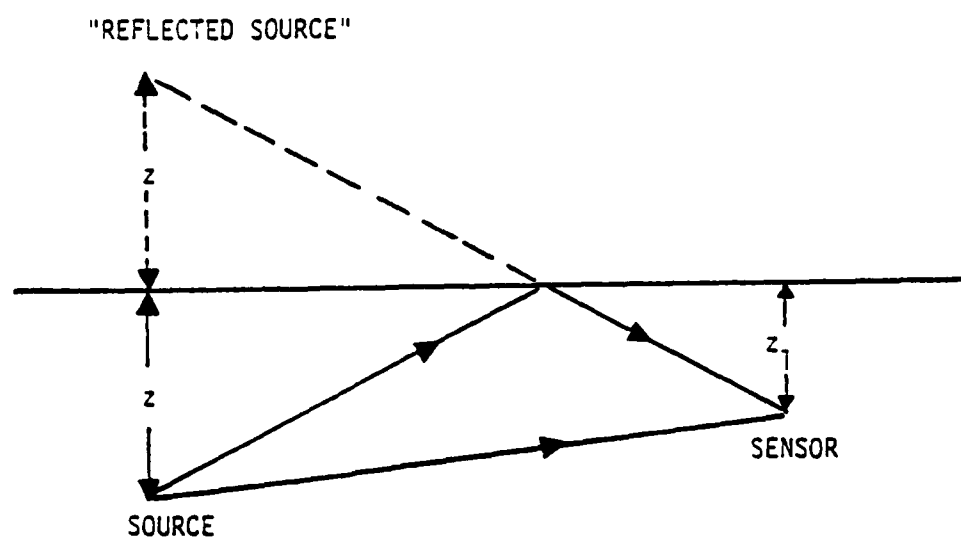


Figure 1: Single sensor geometry

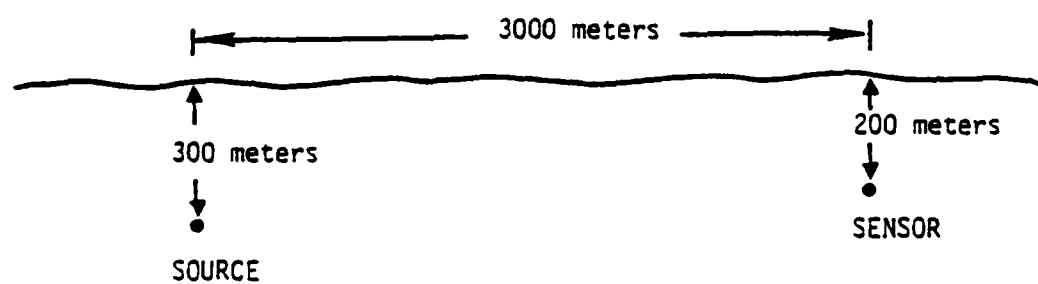


Figure 2: Single Sensor Example

1CH VAR(Z) Z1=200 Z=300 Y=3000 B=3.78

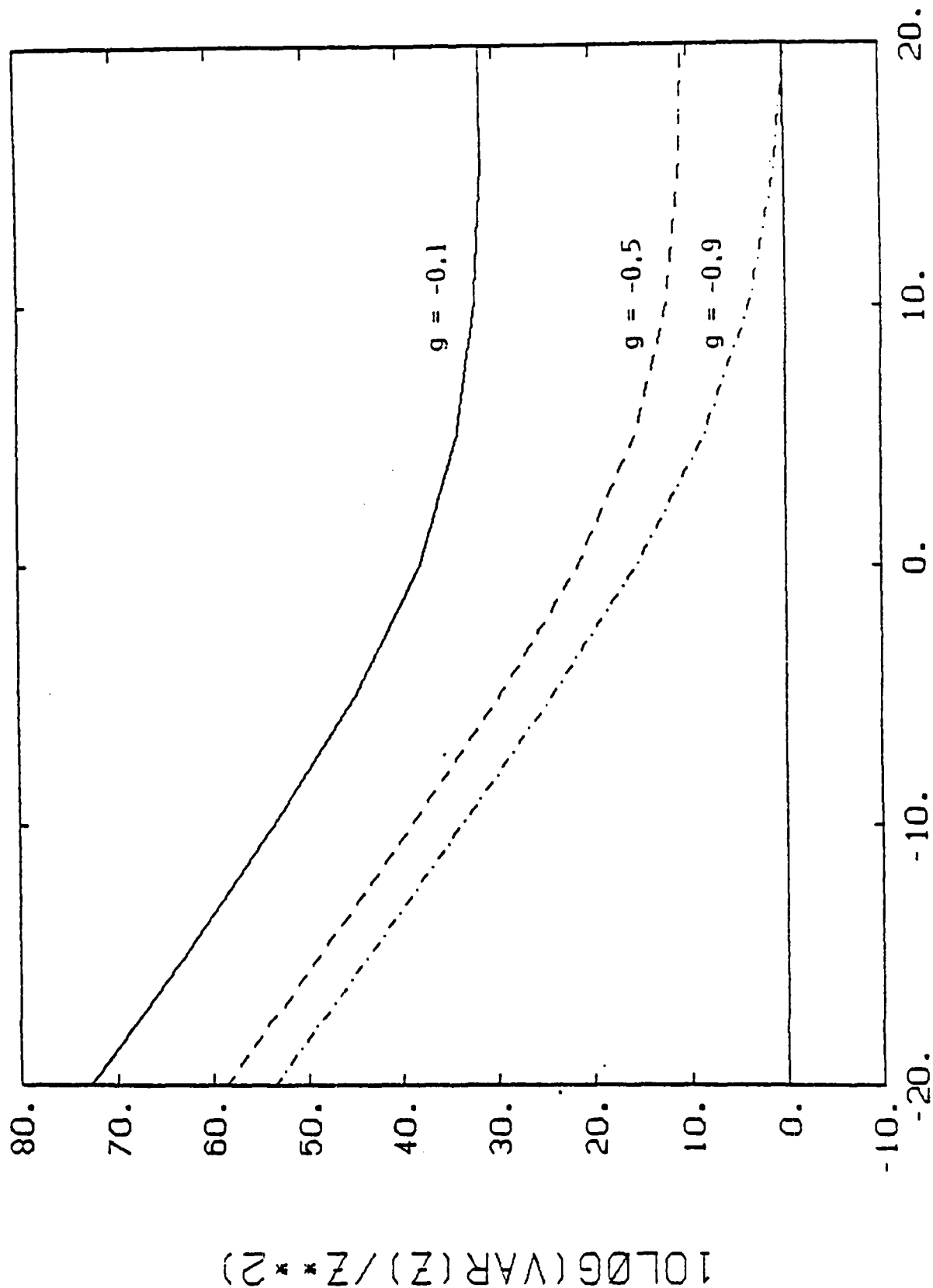
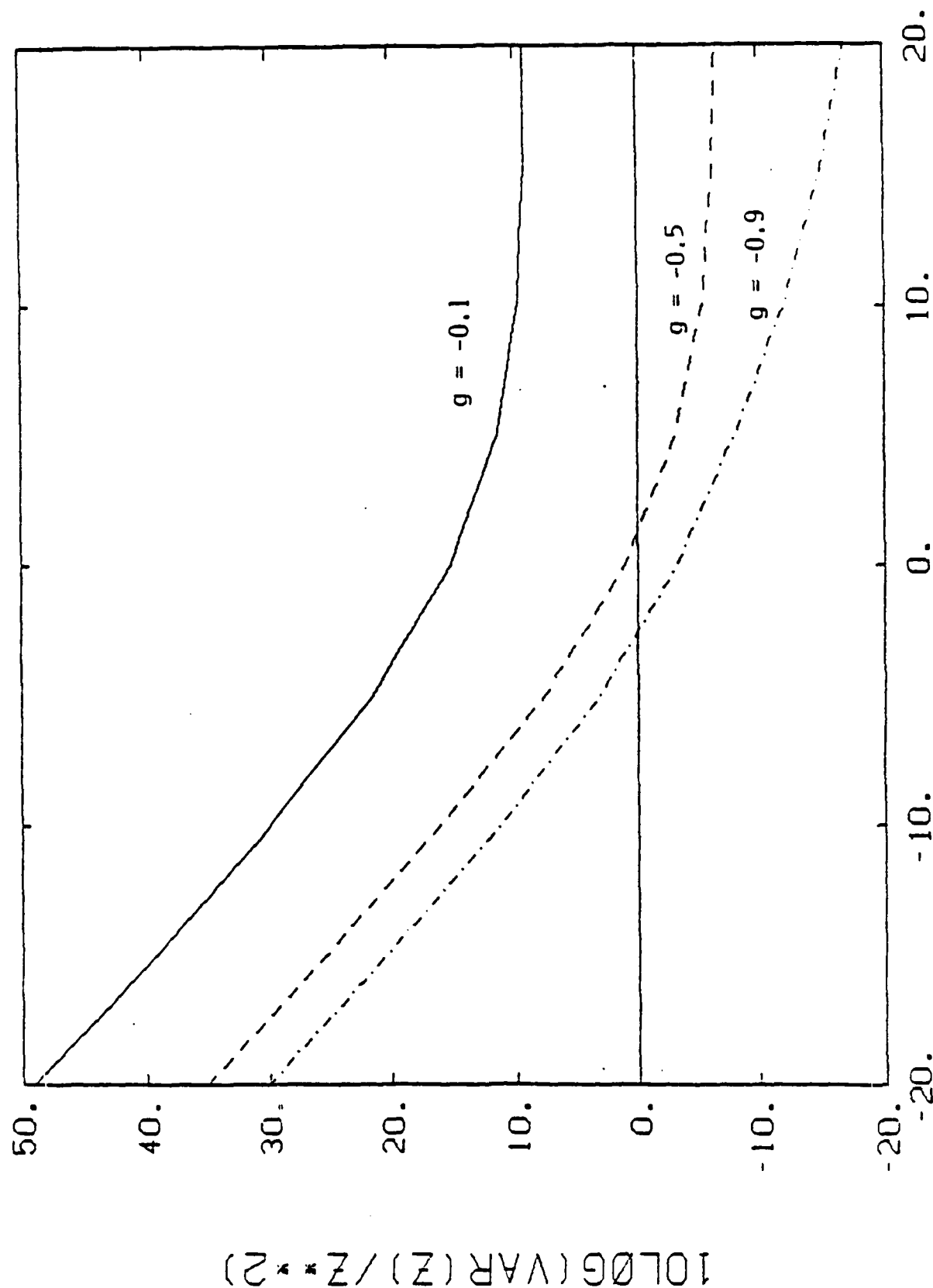


Figure 3: Single sensor with multipath, B = 3.78

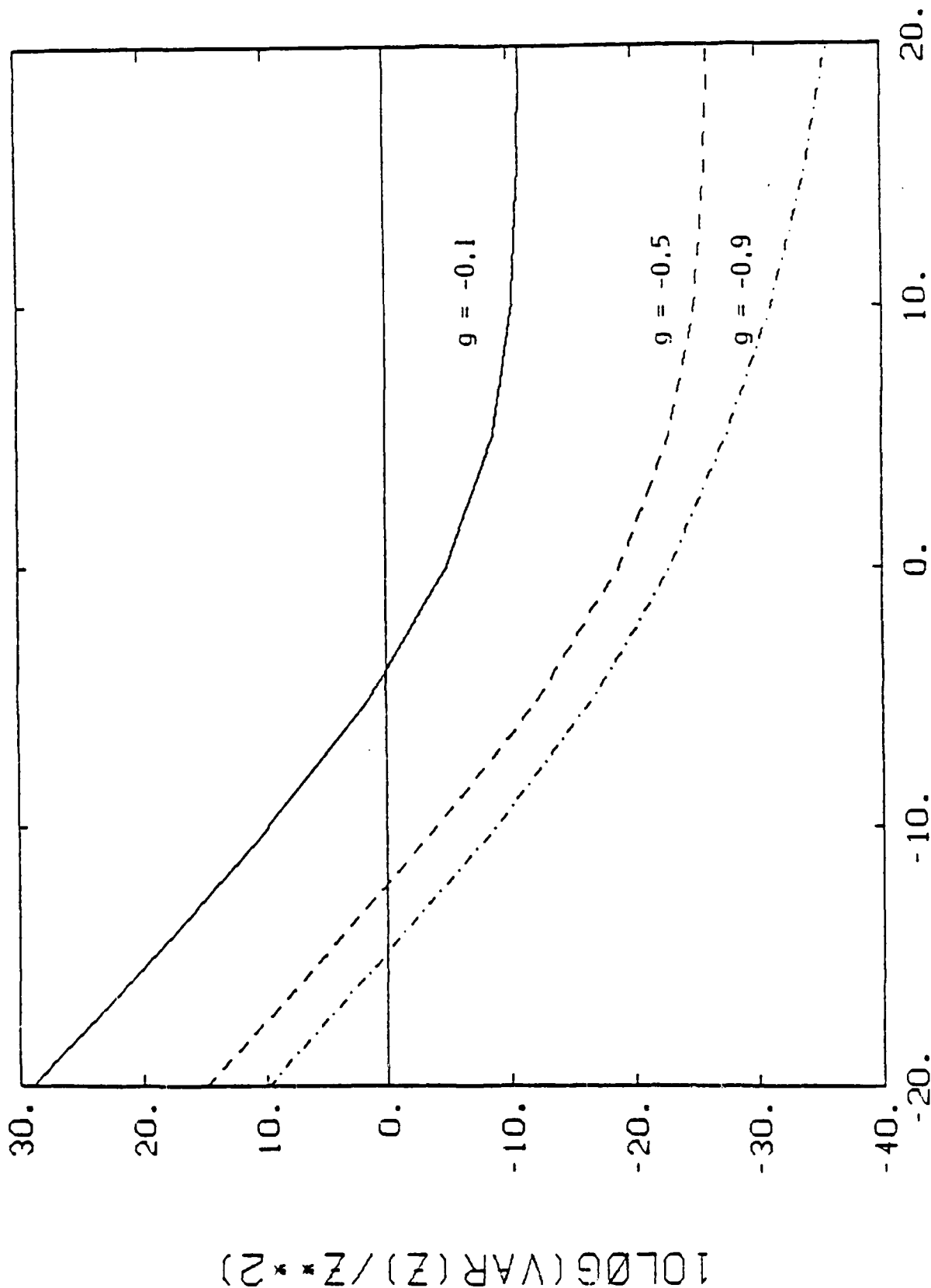
1CH VAR(Z) Z1=200 Z=300 Y=3000 B=37.77



SNR (DB); $g = -0.1, -0.5, -0.9$; NFRQ=100; BT1=1.0 BT2=1.90 BT12=0

Figure 4: Single sensor with multipath, $B = 37.77$

1CH VAR(Z) Z1=200 Z=300 Y=3000 B=377.70



SNR (DB); G= -0.1, -0.5, -0.9; NFR0=755; BT1=10.0 BT2=10.87 BT12=0

Figure 5: Single sensor with multipath, B = 377.70

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TRACK PARAMETER EXTRACTION USING MULTIPATH DELAY AND
DOPPLER INFORMATION(U) SYSTEMS CONTROL TECHNOLOGY INC
PALO ALTO CA K LASHKARI ET AL. FEB 86 5517

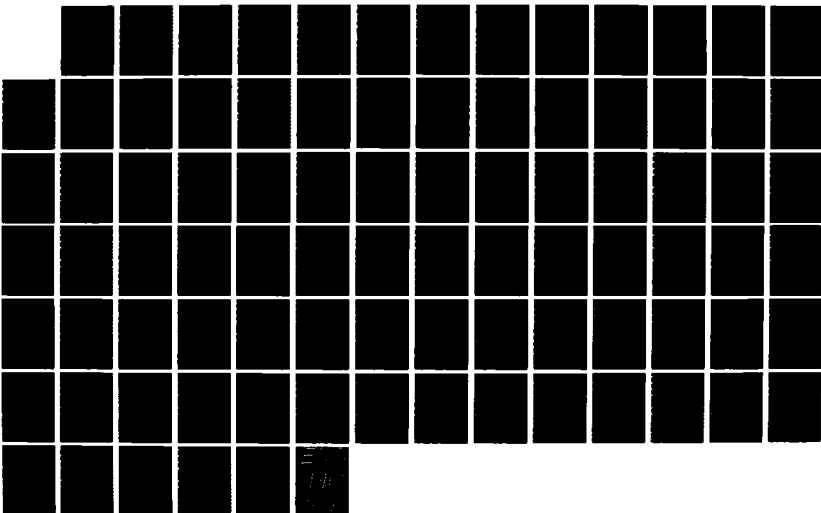
2/2

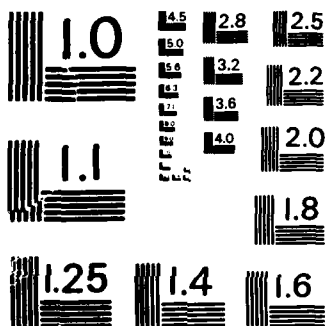
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MICROCOPY RESOLUTION TEST CHART
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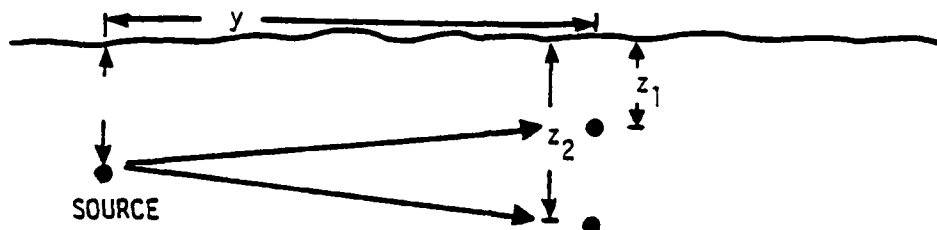


Figure 6: Geometry for two sensors no multipath

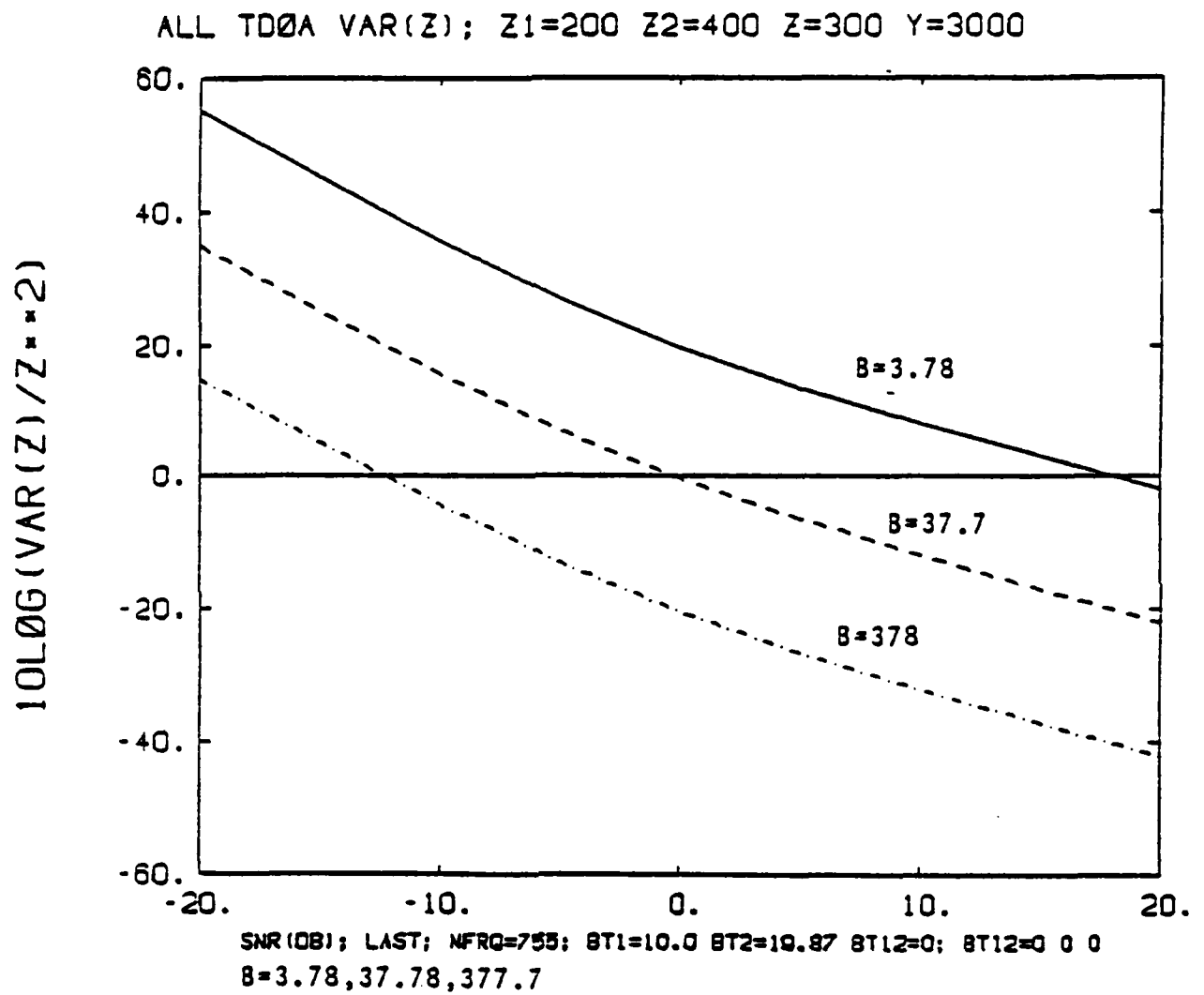


Figure 7: Two sensors no multipath example -- varying bandwidth

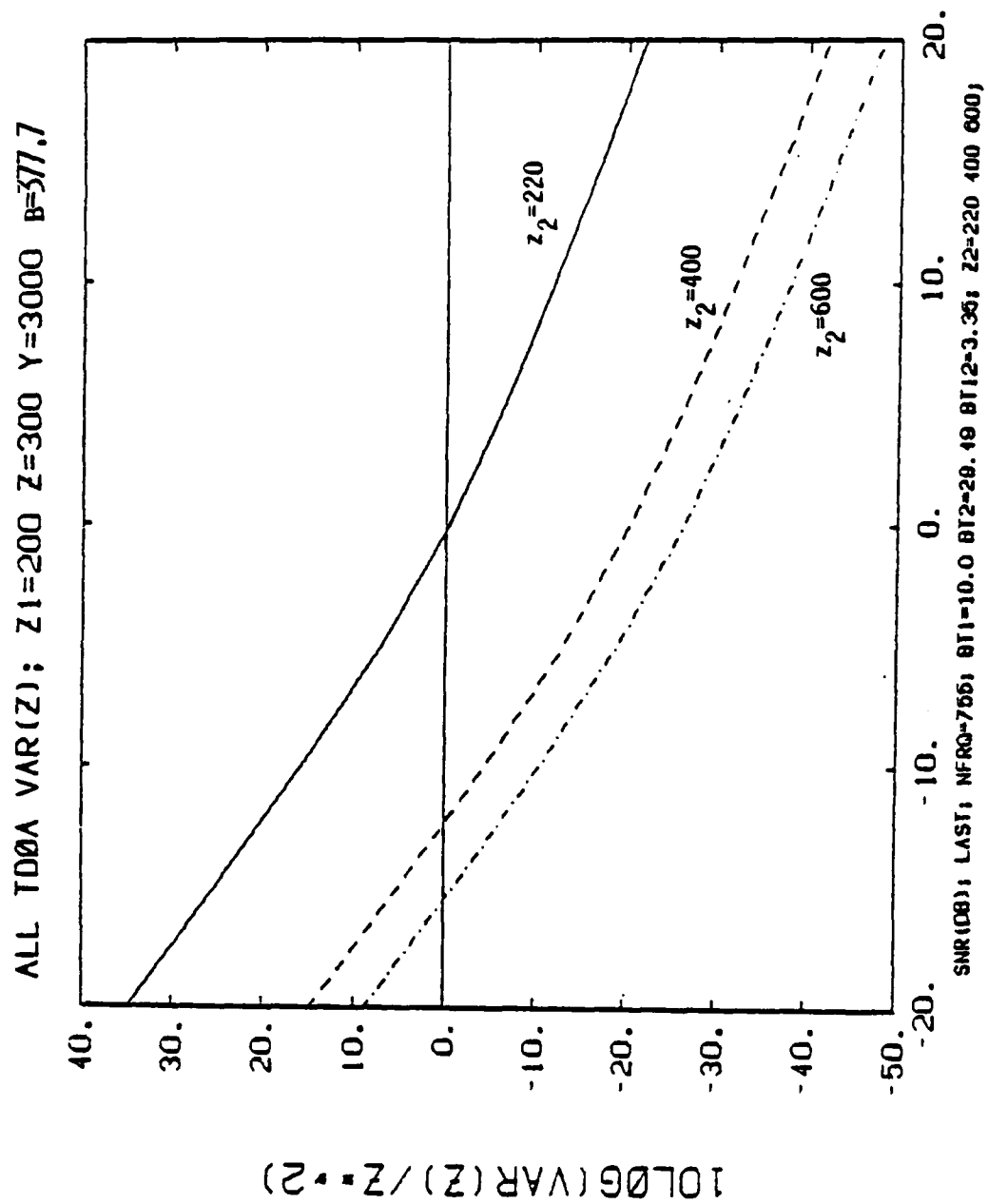


Figure 8: Two sensors no multipath example -- varying sensor separation

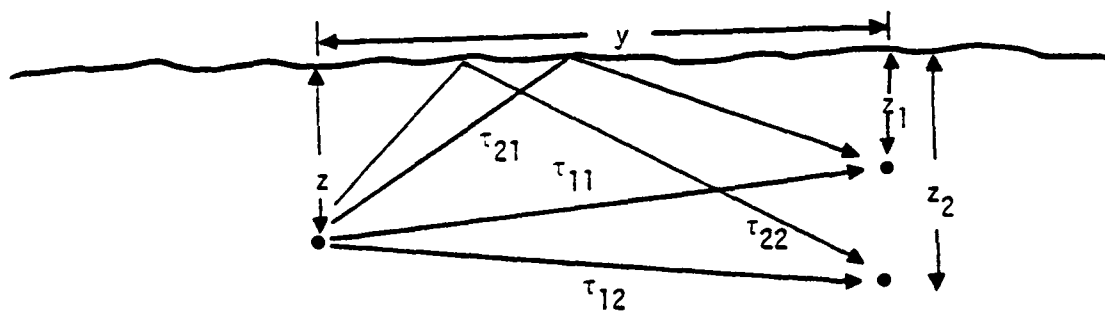


Figure 9: Geometry for two sensors with multipath

2CH VAR(Z) Z1=200 Z2=400 Y=3000 B=3.78

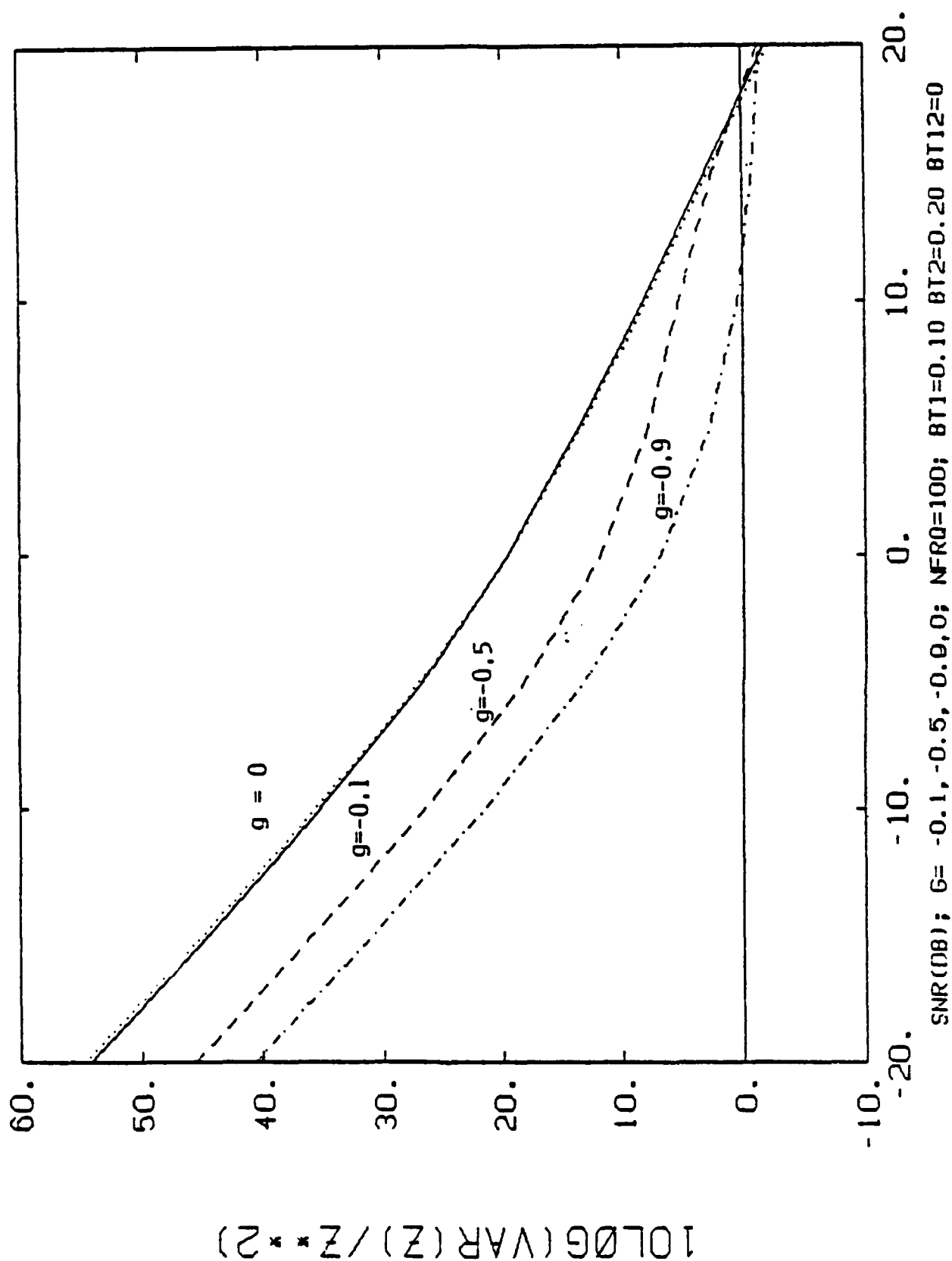
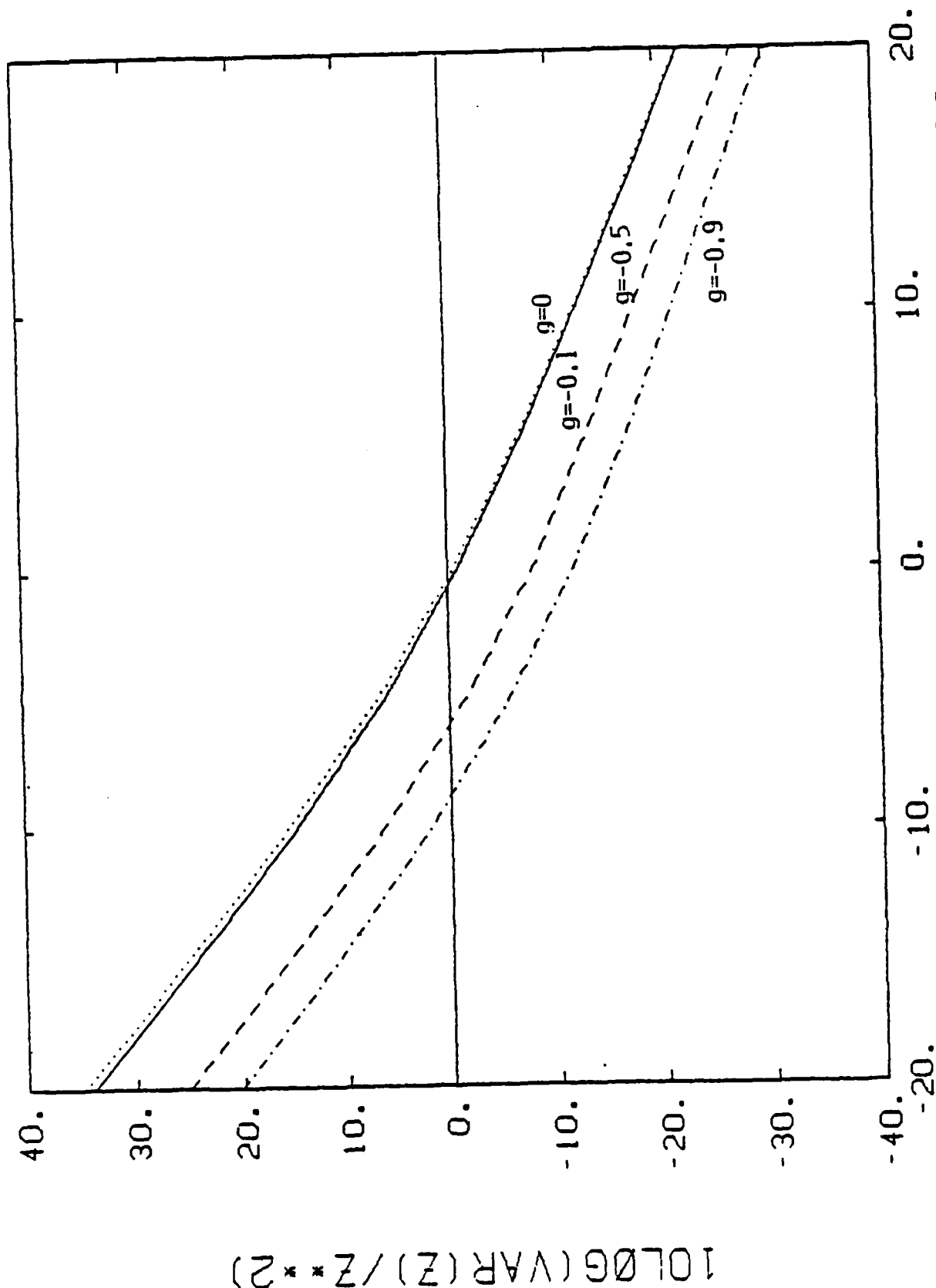


Figure 10: Two sensors with multipath -- $z_2 = 400$, $B = 3.78$

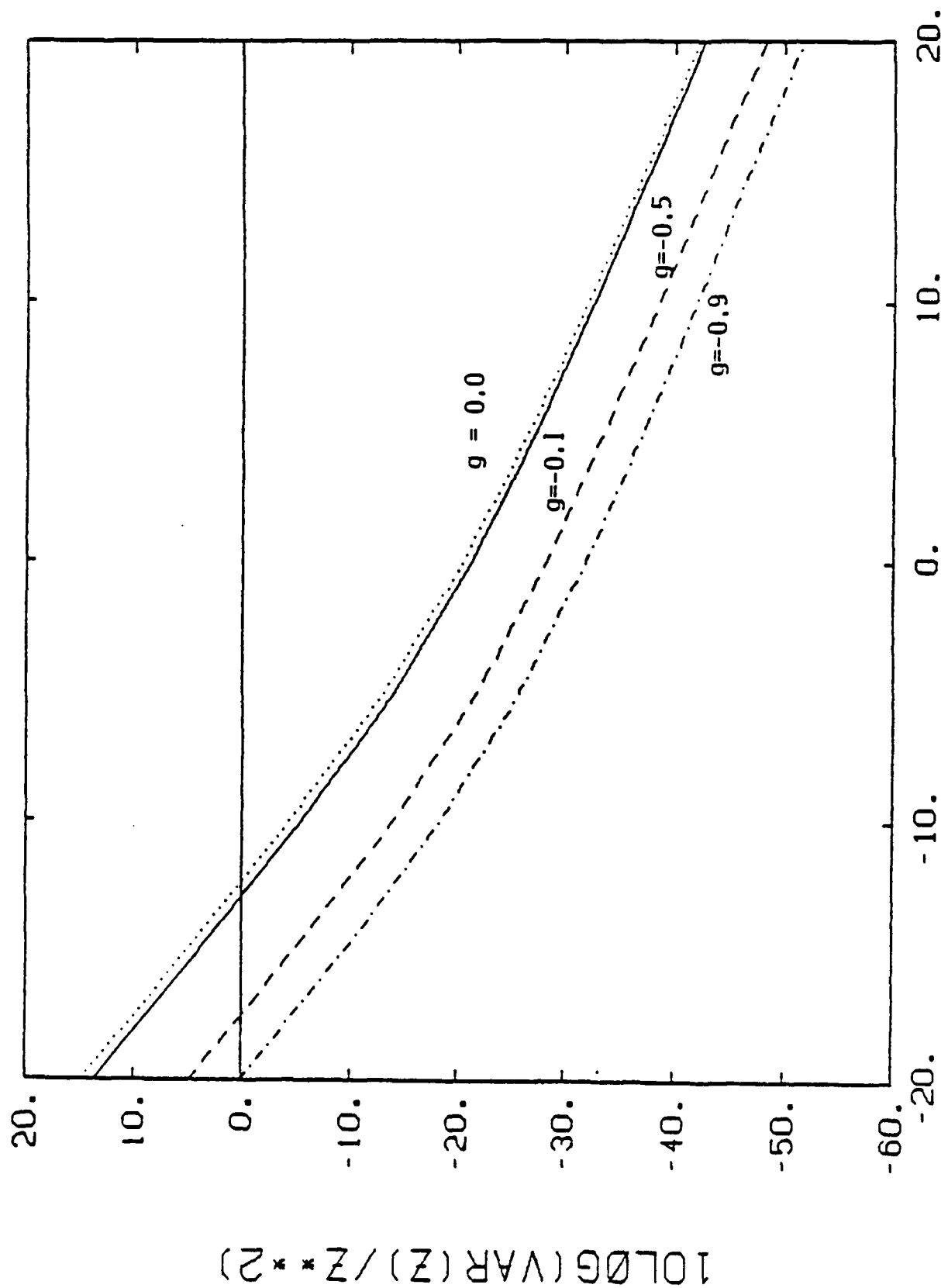
2CH, VAR(Z) Z1=200 Z2=400 Z=300 Y=3000 B=37.77



SNR (DB); $G = -0.1, -0.5, -0.9, 0$; NFRQ=100; BT1=1.0 BT2=1.09 BT12=0

Figure 11: Two sensors with multipath -- $z_2 = 400$, $B = 37.77$

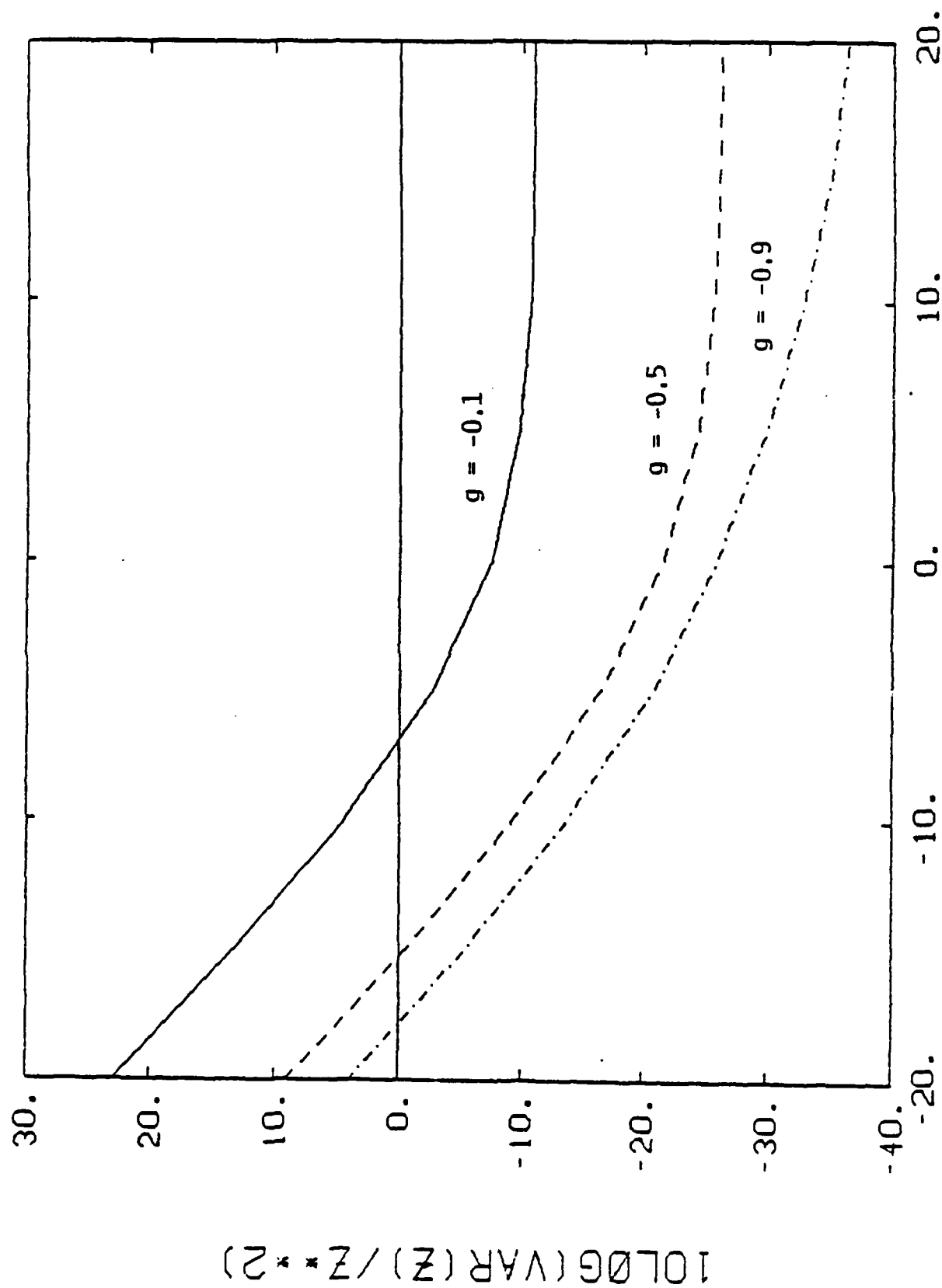
2CH VAR(Z) Z1=200 Z2=400 Y=3000 B=377.70



SNR(0B); 6= -0.1, -0.5, -0.9, 0; NFRQ=755; BT1=10.0 BT2=19.87 BT12=0

Figure 12: Two sensors with multipath -- $z_2 = 400$, $B = 377.70$

2CH VAR(Z) Z1=200 Z2=200 Z=300 Y=3000 B=377.70



SNR(DB); G= -0.1, -0.5, -0.9, 0; NFR0=755; BT1=10.0 BT2=10.0 BT12=0

Figure 13: Two sensors with multipath --- $z_2 = 200$, $B = 377.70$

2CH, VAR(Z) Z1=200 Z2=600 Z=300 Y=3000 B=377.70
 SNR(0B); G= -0.1, -0.5, -0.9, 0; NFR0=755; BT1=10.0 BT2=29.49 BT12=3.35

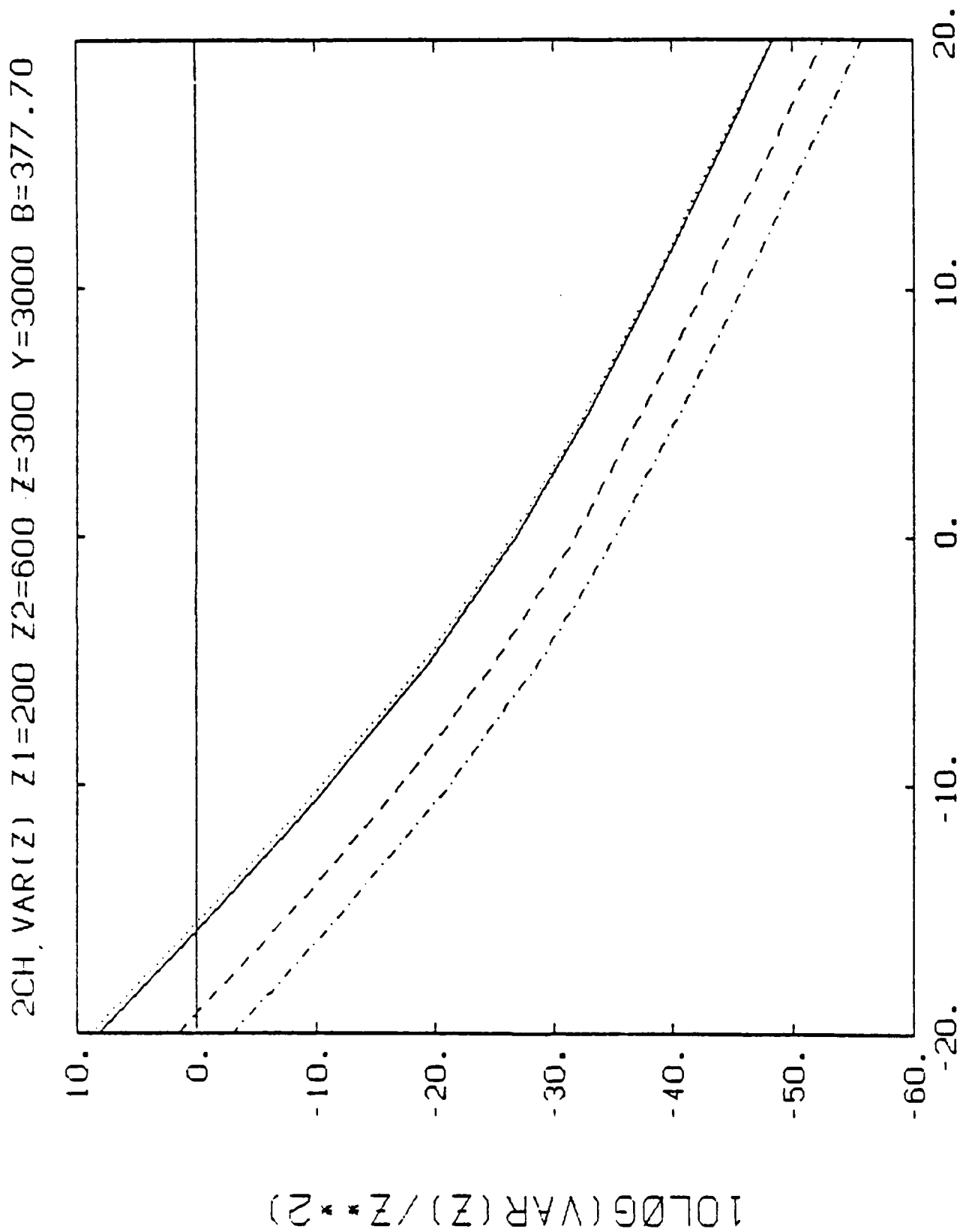


Figure 15: Two sensors with multipath -- $z_2 = 600$, $B = 377.70$

2CH VAR(Z) Z1=200 Z2=400 Z=300 Y=3000 B=37.77

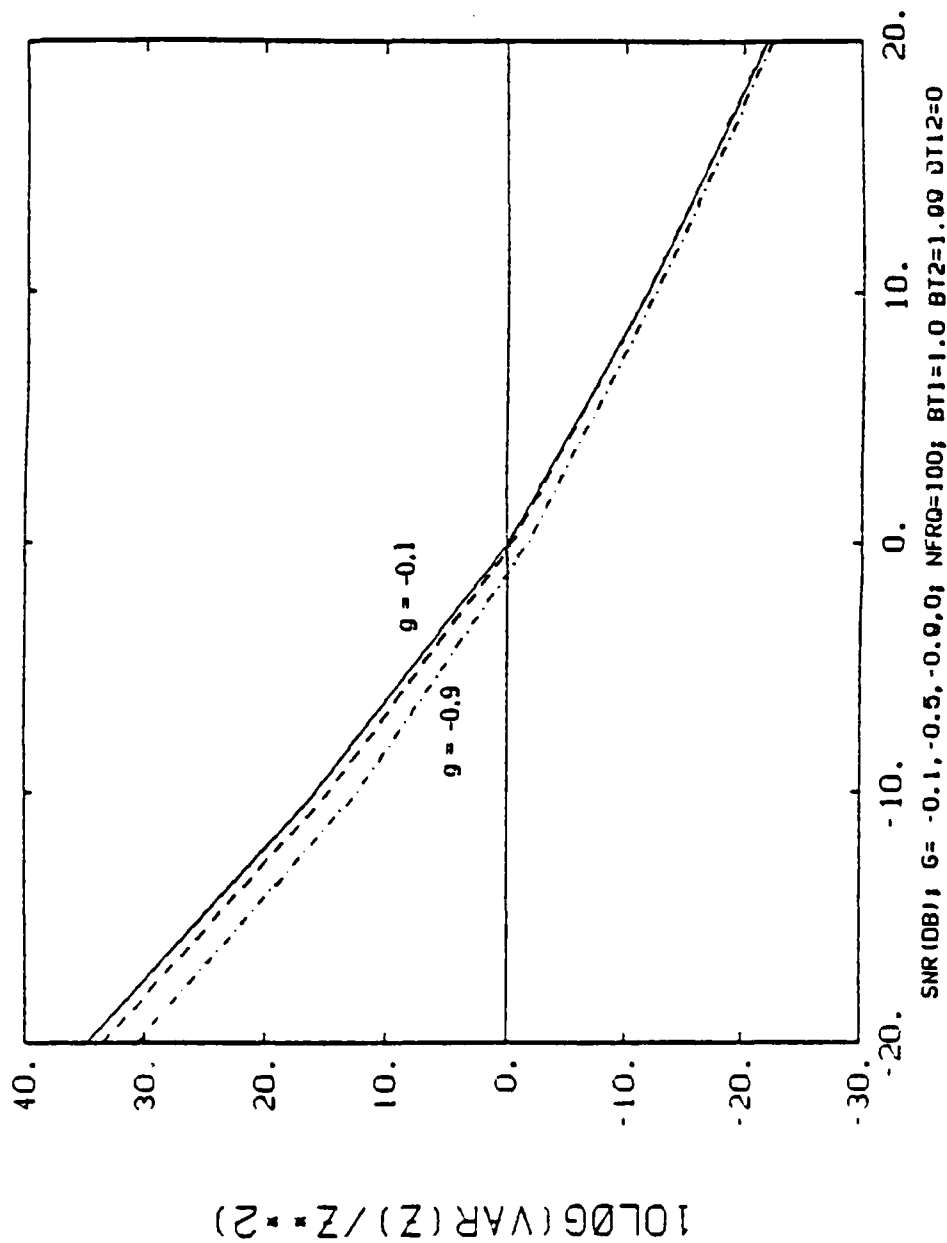


Figure 17: Unknown range -- $z_2 = 400$, $B = 37.77$

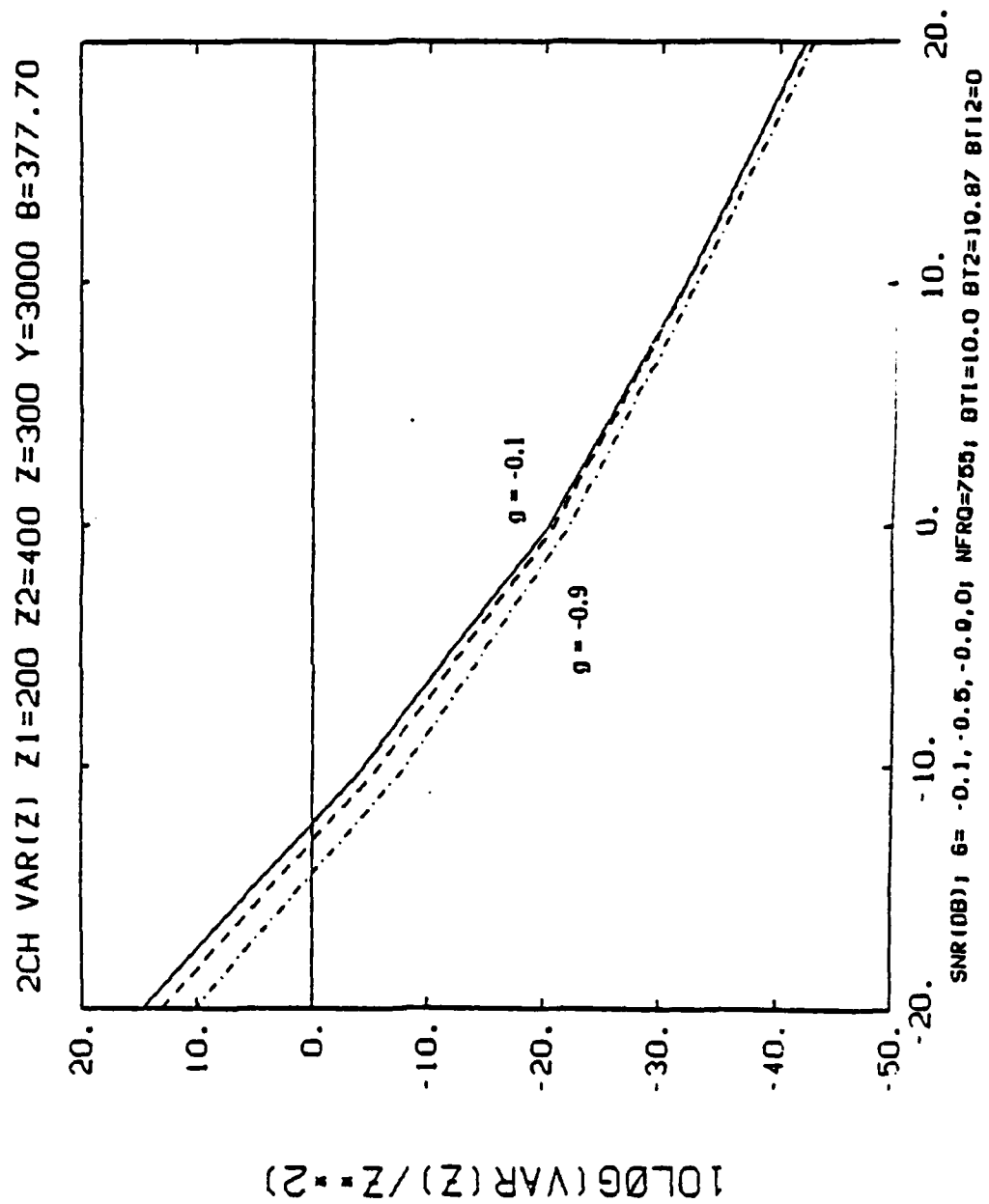


Figure 18: Unknown range -- $Z_2 = 400$, $B = 377.70$

2CH VAR(Z) Z1=200 Z2=600 Z=300 Y=3000 B=377.70

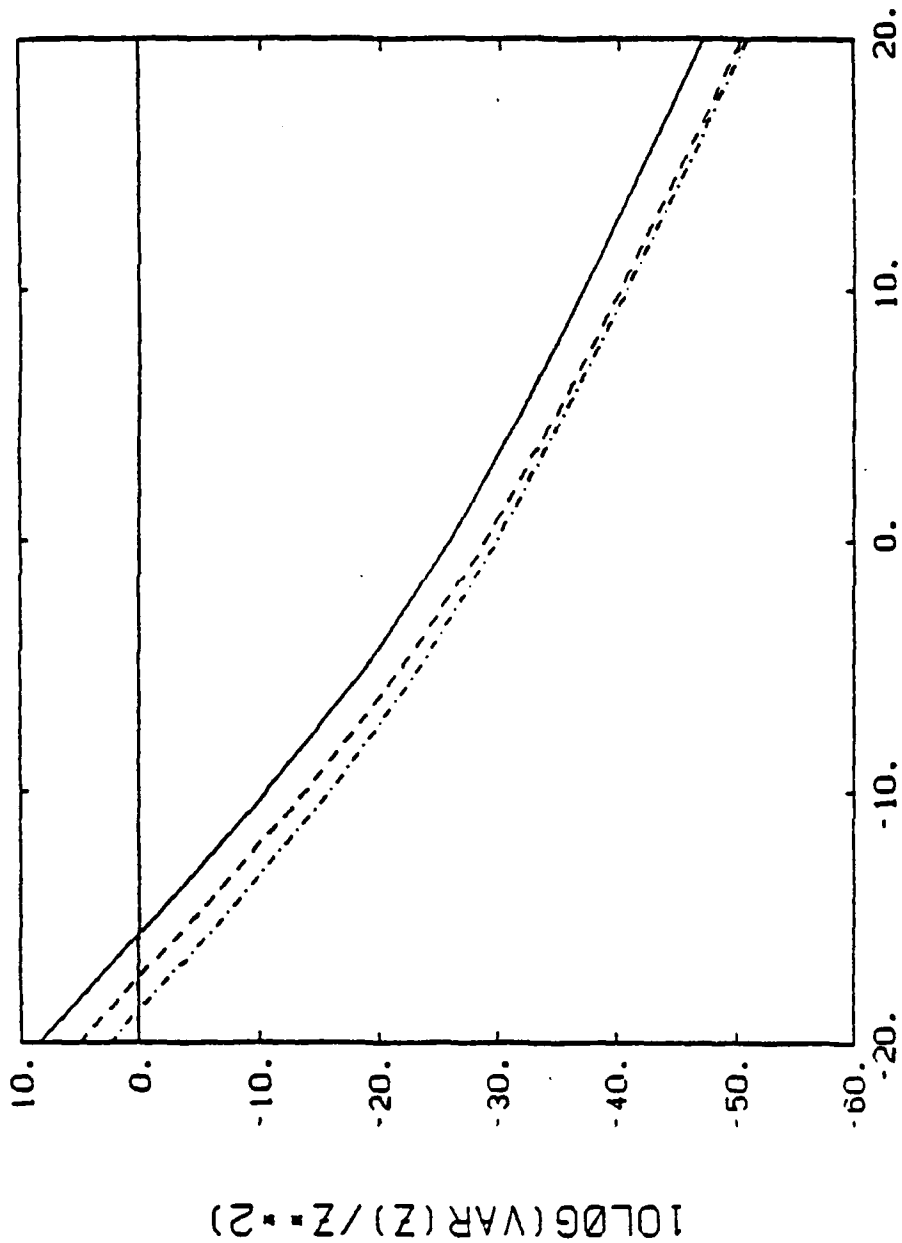


Figure 19: Unknown range -- $z_2 \approx 600$, $B = 377.70$

APPENDIX - SOFTWARE LISTINGS

The software developed to compute and display the CRB for the various test cases was written in the CtrlC language. CtrlC is a software product of Systems Control Technology. The CtrlC code below is contained on the SCT VAX directory NETVAX::dra2:[mts.bound.cr.depth]*.*. While connected to that directory, the monitor command @CMCM will run an example test case. The command @CMCM invokes the VAX/VMS DCL command file CMCM.COM which is also listed below. A summary of the various files is given first.

- cmcm.com - Run CtrlC and feed it cmcm.ctr
- cmcm.ctr - Outer loop of CtrlC commands for different SNR, BT, etc.
- tdoa.ctr - Compute CRB for case of two-channel TDOA
- scmp.ctr - Compute CRB for case of single-channel multipath data
- mcmp.ctr - Compute CRB for case of multichannel multipath data
- mctd.ctr - Compute multipath delays and tdoa from geometry
- mpsn.ctr - Adjust SNR to eliminate signal boost due to multipath
- simp.ctr - Simpson's rule for numerical integration

The file cmcm.com loads the CtrlC function library dra2:[MTS.ML.SPLIB]SP.LIB which contains many simple utility functions not implemented directly in CtrlC. The contents of SP.LIB are described in [Smith84b].

CMCM.COM - Initiation Of Test Cases

```
$! cmcm.com - Go into CtrlC, load SPLIB, and DO cmcm.CTR to obtain the
$! crb's for the 1-channel and 2-channel multipath situation
$!
$ run dra1:[sctlb.ctrlc]ctrlc.exe/nodebug
diary >cmcm.log;
lib DRA2:[MTS.ML.SPLIB]sp;
j = sqrt(-1);
// echo=1;
// term='vt12';
term='ptx';
hard = 'ptx';
redh >cmcm.ptx
do cmcm;
exit;
$ pra2 cmcm.ptx
```

```
# pra2 ctrlc.ptx
# pra2 cmcm.log
```

CMCM.CTR - Outer Loop Of CtrlC Commands For Different SNR, BT,
Etc.

```
// []=cmcm()
deff mcmp
deff scmp
deff tdoa
deff mpsn
deff mctd
deff simp
dotdoa=0;
doscmp=0;
dompsnr=0;
z1=200;
snr=[-20,-10,0,10,20]; nsnr=5;
g=[-0.001,-0.01,-0.05]; ng=3;
vzpn=ones(nsnr,ng+1);
ntd=9; // max number of tdoa-only plots
vztd=ones(nsnr,ntd);
itd=1;
FOR z2=[600],...
  FOR z=[300],...
    FOR y=[3000],...
      FOR B=[10]/.026476,...
        [mpd1,mpd2,td12]=mctd(z1,z2,z,y);...
        bt1=mpd1*B;bt2=mpd2*B;bt3=abs(td12)*B;...
        str5=['; BT1=',cvfs(bt1,2), ' BT2=',cvfs(bt2,2), ' BT12=',cvfs(bt3,2)]
        Nfrq=max([2*round(b),100])+1;...
        str0=['; Nfrq=',cvs(round(Nfrq))];...
        disp([str5,str0]);...
        tmp1=[' z1=',cvs(z1)];...
        tmp2=[' z=',cvs(z), ' y=',cvs(y), ' b=',cvfs(b,2)];...
        IF dompsnr=1,tmp2=[tmp2,'C'];ELSE end;...
        str1=[tmp1, ' z2=',cvs(z2),tmp2];...
        str4=[tmp1,tmp2];...
        gstr=' ';...
        IF DoTdoa=1,...
          FOR i=1:nsnr,...
            vzpn(i,ng+1)=tdoa(snr(i),z1,z2,z,y,B);...
            IF itd<=ntd,vztd(i,itd)=vzpn(i,ng+1); ELSE end;...
            disp(['TDOA Var(z)=',cvs(.5*db(vzpn(i,ng+1))), ' dB']);...
          end,...i
        ELSE end;...
        itd=itd+1;...
        FOR ig=1:ng,...
          tmp=cvfs(g(ig),1);...
```

```

str2=[' g=',tmp];...
gstr=[gstr,tmp];...
IF ig<ng,gstr=[gstr,','];ELSE end;...
sstr='';...
FOR i=1:nsnr,...
    tsnr=mpsn(snr(i),z1,z2,z,y,B,g(ig));...
    IF dompsnr=1,csnr=tsnr;ELSE csnr=snr(i);end;...
    tmp=[cvs(snr(i)),(' ',cvfs(tsnr,2),')');...
    str3=[' snr=',tmp];...
   sstr=[sstr,tmp];...
    IF i<nsnr,sstr=[sstr,','];ELSE end;...
    disp([str1,str2,str3]);...
    IF doscmp=1,...
        vzsc(i,ig)=scmp(csnr,z1,z,y,B,g(ig),Nfrq);...
        disp(['1ch Var(z)=',cvs(0.5*db(vzsc(i,ig))),' dB']);...
    ELSE end;...
    [tmp,vypn,vzpn]=mcmp(csnr,z1,z2,z,y,B,g(ig),Nfrq);...
    vzpn(i,ig)=tmp;...
    disp(['2ch Var(z)=',cvs(0.5*db(vzpn(i,ig))),' dB']);...
    disp(['2ch Var(y)=',cvs(0.5*db(vypn)), ' dB']);...
    disp(['2ch Xv(zy)=',cvs(0.5*db(abs(vzpn))), ' dB']);...
end,...i
end,...ig
IF doscmp=1,...
    erase;...
    plot(snr,db(vzsc)/2);...
    title(['1ch Var(z)',str4]);...
    xlab(['SNR(dB); G=',gstr,str0,str5]);...
    ylab('10log(Var(z)/z**2)');...
    IF norm(term(1:3)-'ptx')<>0,replot;ELSE end;...
ELSE end;...
    erase;...
    plot(snr,db(vzpn)/2);...
    title(['2ch Var(z)',str1]);...
    xlab(['SNR(dB); G=',gstr,',0',str0,str5]);...
    gstr='';...
    ylab('10log(Var(z)/z**2)');...
    IF norm(term(1:3)-'ptx')<>0,replot;ELSE end;...
end,...B
end,...y
end,...z
end, // z2
IF DoTdoa=1, ...
    erase;...
    plot(snr,db(vztd)/2);...
    title(['All TDOA Var(z); LAST ',str4]);...
    xlab(['SNR(dB); LAST',str0,str5]);...
    ylab('10log(Var(z)/z**2)');...
    IF norm(term(1:3)-'ptx')<>0,replot;ELSE end;...
ELSE end;

```

TDOA.CTR - Compute CRB For Case Of Two-channel TDOA

```
// [vzpn] = tdoa(snr, z1, z2, z, y, B)
//
// Compute CRB for source depth given 2-channel TDOA measurements
//
// z1 = Sensor 1 depth
// z2 = Sensor 2 depth
// z = Target depth
// y = Target range projected to surface (meters)
// B = Target bandwidth (Hz)
// Snr = Signal to noise ratio in dB at each sensor

c = 1500; // Speed of sound (m/sec)
snr1 = 10**((snr/10); snr2 = 10**((snr/10);
t11 = sqrt(y*y+(z-z1)**2)/c;
t12 = sqrt(y*y+(z-z2)**2)/c;
d = t12 - t11;
dztmp = z1*t12-z2*t11-z*d;
if abs(dztmp)<eps, ...
    disp(' tdoa: numerical failure. tdoa not a function of depth'); ...
    vzpn=1.0; ... create line at 0dB ...
    return;
dzdd = c*c*t11*t12/dztmp;
vard = (3/(2*pi*B)**2)*(1+snr1+snr2)/(snr1*snr2);
vzpn = (vard*dzdd**2)/(z*z);
```

SCMP.CTR - Compute CRB For Case Of Single-channel Multipath Data

```
// [vzpn] = scmp(snr, z1, z, y, B, g, Nfrq)
//
// Compute per-sample CRB for 1-channel multipath situation
// Sampling rate is assumed to be 2B rad/sec
//
// z1 = Sensor 1 depth
// z = Target depth
// y = Target range projected to surface (meters)
// B = Target bandwidth (Hz)
// g = Multipath attenuation
// Snr = Signal to noise ratio in dB
// Nfrq = Number of frequency samples uniform on [0, B]
//
// Derived constants

c = 1500; cs = c*c; // Speed of sound (m/sec)
f = b*[0:Nfrq-1]/Nfrq; // Hertz frequency axis
w = 2*pi*f; // Radian frequency axis
Sx=1; Se = 10**(-snr/10); // PSD in band [-B, B]
```

```

t11 = sqrt(y*y+(z-z1)**2)/c;
t21 = sqrt(y*y+(z+z1)**2)/c;
D = t21-t11;
dDdz = (z+z1)/(c*t21) - (z-z1)/(c*t11);
Sy = ((1+g**2)*ONES(1,Nfrq)+2*g*cos(w*D))*Sx + Se*ones(1,Nfrq);
SydD = -2*Sx*g*w.*sin(w*D);
si = SydD./(Sy+EPS*ONES(1,Nfrq)); // Specific information for delay estimation
JD = SUM(si.*si)/(2*Nfrq); // per-sample CRB Var(D) .ge. 1/JD
vzpn = (1/(JD*(dDdz**2)+EPS))/(z*z);

```

MCMP.V2 - CRB For Multichannel Multipath Data, Known Range

```

// [vzpn] = mcmp(snr, z1, z2, z, y, B, g, Nfrq)
//
// Compute CRB for 2-channel multipath situation
//
// z1 = Sensor 1 depth
// z2 = Sensor 2 depth
// z = Target depth
// y = Target range projected to surface (meters)
// B = Target bandwidth (Hz). Must be from 0 to .5
// g = Common multipath attenuation
// Snr = Signal to noise ratio in dB
// Nfrq = Number of frequency samples uniform on [0,B]
//
// Derived constants
j = sqrt(-1);
g1 = g; // Relative attenuation of 2ndary path to channel 1
g2 = g; // Relative attenuation of 2ndary path to channel 2
c = 1500; // Speed of sound (m/sec)
f = b*[0:Nfrq-1]/Nfrq; // Hertz frequency axis
w = 2*pi*f; // Radian frequency axis
Sx1=1; Sx2=1; // PSD of signal in band [-B,B]
snr1 = snr; snr2 = snr; // SNR in channels 1 and 2, resp.
Se1 = 10**(-snr1/10); // PSD of noise in band [-pi,pi]
Se2 = 10**(-snr2/10); // PSD of noise in band [-pi,pi]
// disp('disabling channel 1'); Sx1=0;

// Multipath time delays

t11 = sqrt(y*y+(z-z1)**2)/c;
t21 = sqrt(y*y+(z+z1)**2)/c;
t12 = sqrt(y*y+(z-z2)**2)/c;
t22 = sqrt(y*y+(z+z2)**2)/c;
BT = max([(t22-t12)*B, (t21-t11)*B]);
ppc = Nfrq/BT; // Number of integration points per multipath spectral cycle
if ppc<20, disp(['Warning, BT=',cvfs(BT,2), ' while Nfrq=',cvs(Nfrq)]); ...
disp([' which means only ',cvfs(ppc,2), ' integration points per cycle']);

```

```

// derivatives of delay wrt z

cs = c*c;
t11z = (z-z1)/(cs*t11);
t21z = (z+z1)/(cs*t21);
t12z = (z-z2)/(cs*t12);
t22z = (z+z2)/(cs*t22);

// Derivatives of source-to-sensor spectra wrt delays

// s1/z = s1/t11 t11/z + s1/t21 t21/z
s111 = -(2*Sx1*g1)*(w.*sin((t11-t21)*w)); // s1/t11 = - s1/t21
s1z = s111*(t11z-t21z); // s111*t11z + s121*t21z

// s2/z = s2/t12 t12/z + s2/t22 t22/z
s212 = -(2*Sx2*g2)*(w.*sin(w*(t12-t22))); // = -s222
s2z = s212*(t12z - t22z);

// s12z = conj(s21z) = sum(i,j=1,2) s12/tij tij/z
ejw = exp(j*w);
ej11 = exp(j*w*t11);
ej12 = exp(j*w*t12);
ej21 = exp(j*w*t21);
ej22 = exp(j*w*t22);
k1=ej12+g2*ej22;
k2=conj(ej11+g1*ej21);
t=j*w*sqrt(Sx1*Sx2);
x11 = -t.*conj(ej11).*k1; // x expands to "S12/t"
x21 = -g1*t.*conj(ej21).*k1;
x12 = t.*ej12.*k2;
x22 = g2*t.*ej22.*k2;
s12z = x11*t11z + x12*t12z + x21*t21z + x22*t22z;

s1 = Sx1*abs(ones(1,Nfrq)+g1*ej11.*conj(ej21)).**2 + Se1*ones(1,Nfrq);
s2 = Sx2*abs(ones(1,Nfrq)+g2*ej12.*conj(ej22)).**2 + Se2*ones(1,Nfrq);
s12 = sqrt(Sx1*Sx2)*k2.*k1;

// Do sisz = S**(-1) S/z

// d1 means d ln ... dlij means S^-1 dS/dz [i,j]
detS = s1.*s2 - s12.*conj(s12);
d111 = (s2.*s1z-s12.*conj(s12z))./detS;
d112 = (s2.*s12z-s12.*s2z)./detS;
d121 = (s1.*conj(s12z)-conj(s12).*s1z)./detS;
d122 = (s1.*s2z-conj(s12).*s12z)./detS;

// Trace d1**2

td1s = d111.*d111 + d122.*d122 + 2*d112.*d121;
std1 = max([eps,abs(sum(td1s))]);
if std1==eps, disp('numerical failure. vanishing info matrix');
s1 = sum(td1s(1:2:Nfrq));

```



```

s2 = sum(td1s(2:2:Nfrq));
errv = [(s1-s2)/std1, abs(s1+s2)-std1];
if sum(abs(errv))>0.01, ...
    disp('relative half-sum difference, 0] (numerical integration check): ')
    errv, ...
else end;
tinf = std1/(2*Nfrq);
vzpn = (1/tinf)/(z*z);

```

MCMP.CTR - CRB For Multichannel Multipath Data, Unknown Range

```

// [vzpn, vypn, vyzp] = mcmp(snr, z1, z2, z, y, B, g, Nfrq)
//
// Compute CRB for range and depth estimation given 2-channel
// multipath and tdoa measurements.
//
// z1 = Sensor 1 depth
// z2 = Sensor 2 depth
// z = Target depth
// y = Target range projected to surface (meters)
// B = Target bandwidth (Hz). Must be from 0 to .5
// g = Common multipath attenuation
// Snr = Signal to noise ratio in dB
// Nfrq = Number of frequency samples uniform on [0,B]
//
// vzpn = Cramer-Rao lower bound for the estimation of z
// vypn = Cramer-Rao lower bound for the estimation of y
// vyzp = Cramer-Rao lower bound for cross-variance of y and z
//
// Derived constants

j = sqrt(-1);
g1 = g; // Relative attenuation of 2ndary path to channel 1
g2 = g; // Relative attenuation of 2ndary path to channel 2
c = 1500; // Speed of sound (m/sec)
f = b*[0:Nfrq-1]/Nfrq; // Hertz frequency axis
w = 2*pi*f; // Radian frequency axis
Sx1=1; Sx2=1; // PSD of signal in band [-B,B]
snr1 = snr; snr2 = snr; // SNR in channels 1 and 2, resp.
Se1 = 10**(-snr1/10); // PSD of noise in band [-pi,pi]
Se2 = 10**(-snr2/10); // PSD of noise in band [-pi,pi]
// disp('disabling channel 1'); Sx1=0;

// Multipath time delays

t11 = sqrt(y*y+(z-z1)**2)/c;
t21 = sqrt(y*y+(z+z1)**2)/c;
t12 = sqrt(y*y+(z-z2)**2)/c;
t22 = sqrt(y*y+(z+z2)**2)/c;

```

```

BT = max([(t22-t12)*B, (t21-t11)*B]);
ppc = Nfrq/BT; // Number of integration points per multipath spectral cycle
if ppc<20, disp([' Warning, BT=', cvfs(BT,2), ' while Nfrq=', cvs(Nfrq)1]);
    disp([' which means only ', cvfs(ppc,2), ' integration points per cycle']);

// derivatives of delay wrt z
cs = c*c;
t11z = (z-z1)/(cs*t11);
t21z = (z+z1)/(cs*t21);
t12z = (z-z2)/(cs*t12);
t22z = (z+z2)/(cs*t22);

// derivatives of delay wrt y
cs = c*c;
t11y = y/(cs*t11);
t21y = y/(cs*t21);
t12y = y/(cs*t12);
t22y = y/(cs*t22);

// Derivatives of source-to-sensor spectra wrt delay, depth, and range

// s1/z = s1/t11 t11/z + s1/t21 t21/z
s111 = -(2*Sx1*g1)*(w.*sin((t11-t21)*w)); // s1/t11 = -s1/t21
s1z = s111*(t11z-t21z); // s111*t11z + s121*t21z
s1y = s111*(t11y-t21y); // s111*t11y + s121*t21y

// s2/z = s2/t12 t12/z + s2/t22 t22/z
s212 = -(2*Sx2*g2)*(w.*sin(w*(t12-t22))); // = -s222
s2z = s212*(t12z - t22z);
s2y = s212*(t12y - t22y);

// s12z = conj(s21z) = sum(i,j=1,2) s12/tij tij/z
ejw = exp(j*w);
ej11 = exp(j*w*t11);
ej12 = exp(j*w*t12);
ej21 = exp(j*w*t21);
ej22 = exp(j*w*t22);
k1=ej12+g2*ej22;
k2=conj(ej11+g1*ej21);
t=j*w*sqrt(Sx1*Sx2);
x11 = -t.*conj(ej11).*k1; // x expands to "S12/t"
x21 = -g1*t.*conj(ej21).*k1;
x12 = t.*ej12.*k2;
x22 = g2*t.*ej22.*k2;
s12z = x11*t11z + x12*t12z + x21*t21z + x22*t22z;
s12y = x11*t11y + x12*t12y + x21*t21y + x22*t22y;

s1 = Sx1*abs(ones(1,Nfrq)+g1*ej11.*conj(ej21))*2 + Se1*ones(1,Nfrq);
s2 = Sx2*abs(ones(1,Nfrq)+g2*ej12.*conj(ej22))*2 + Se2*ones(1,Nfrq);
s12 = sqrt(Sx1*Sx2)*k2.*k1;

```

```

detS = s1.*s2 - s12.*conj(s12);

// Do sisz = S**(-1) S/z. Below, dzi means S^-1 dS/dz [i,j]
dzi1 = (s2.*s1z-s12.*conj(s12z))./detS;
dzi2 = (s2.*s12z-s12.*s2z)./detS;
dz21 = (s1.*conj(s12z)-conj(s12).*s1z)./detS;
dz22 = (s1.*s2z-conj(s12).*s12z)./detS;

// Trace dz**2
tdzs = dzi1.*dzi1 + dz22.*dz22 + 2*dzi2.*dz21;
stdz = simp(tdzs);
ctdz = simp(tdzs(1:2:Nfrq));
disp(' J11: [simp(n)-simp((n-1)/2)]/simp(n) = ');
(stdz-ctdz)/max([stdz,eps])
disp(' J11: [simp(n)-simp((n-1)/2)] = ');
stdz-ctdz
if abs(imag(stdz))>eps, disp('reality failure, depth part'); stdz
stdz = real(stdz);
Jmtx = ONES(2); // Allocate Fisher information matrix
Jmtx(1,1) = stdz/2;

// Do sisz = S**(-1) S/y. Below, dyi means S^-1 dS/dy [i,j]
dyi1 = (s2.*s1y-s12.*conj(s12y))./detS;
dyi2 = (s2.*s12y-s12.*s2y)./detS;
dy21 = (s1.*conj(s12y)-conj(s12).*s1y)./detS;
dy22 = (s1.*s2y-conj(s12).*s12y)./detS;

// Trace dy**2
tdys = dyi1.*dyi1 + dy22.*dy22 + 2*dyi2.*dy21;
stdy = simp(tdys);
ctdy = simp(tdys(1:2:Nfrq));
disp(' J22: [simp(n)-simp((n-1)/2)]/simp(n) = ');
(stdy-ctdy)/max([stdy,eps])
disp(' J22: [simp(n)-simp((n-1)/2)] = ');
stdy-ctdy
if abs(imag(stdy))>eps, disp('reality failure, range part'); stdy
stdy = real(stdy);
Jmtx(2,2) = stdy/2;

// Trace dz*dy
tzys = dzi1.*dyi1 + dzi2.*dy21 + dz21.*dyi2 + dz22.*dy22;
stzy = simp(tzys);
ctzy = simp(tzys(1:2:Nfrq));
disp(' J12: [simp(n)-simp((n-1)/2)]/simp(n) = ');
(stzy-ctzy)/max([abs(stzy),eps])
disp(' J12: [simp(n)-simp((n-1)/2)] = ');
stzy-ctzy
if abs(imag(stzy))>eps, disp('reality failure, range part');
stzy = real(stzy);
if abs(stzy)<eps, disp('mcmp: zero off-diagonal in info matrix');
Jmtx(1,2) = stzy/2;
Jmtx(2,1) = Jmtx(1,2);

```

```

long; Jmtx
short;
disp('condition number of J matrix:'); COND(Jmtx)

Jinv = INV(Jmtx);
vzpn = Jinv(1,1)/(z*z);
vyzn = Jinv(2,2)/(y*y);
vyzp = Jinv(1,2)/(y*z);

```

MCTD. CTR - Compute Multipath Delays And Tdoa From Geometry

```

// [mpd1,mpd2,td12] = mctd(z1,z2,z,y)
//
// Given geometry, compute multipath delays in each channel,
// and tdoa between channels.
//
// z1 = Sensor 1 depth
// z = Target depth
// y = Target range projected to surface (meters)
//
c = 1500; cs = c*c; // Speed of sound (m/sec)
t11 = sqrt(y*y+(z-z1)**2)/c; // source to sensor 1 direct
t21 = sqrt(y*y+(z+z1)**2)/c; // source to sensor 1 reflected
mpD1 = t21-t11; // multipath delay, sensor 1
t12 = sqrt(y*y+(z-z2)**2)/c; // source to sensor 2 direct
t22 = sqrt(y*y+(z+z2)**2)/c; // source to sensor 2 reflected
mpD2 = t22-t12; // multipath delay, sensor 2
td12 = t12-t11; // tdoa, channel 1 minus 2

```

MPSN. CTR - Adjust SNR To Eliminate Signal Boost Due To Multipath

```

// [csnr] = mpsn(snr,z1,z2,z,y,B,g)
//
// Compute SNR correction due to signal power gain
// in the presence of multipath.
//
// z1 = Sensor 1 depth
// z = Target depth
// y = Target range projected to surface (meters)
// B = Target bandwidth (Hz)
// g = Multipath attenuation
// Snr = Signal to noise ratio in dB given no multipath
//
// Derived constants

```

```

c = 1500; cs = c*c; // Speed of sound (m/sec)
W = 2*pi*B; // Radian band limit

t11 = sqrt(y*y+(z-z1)**2)/c; // source to sensor 1 direct
t21 = sqrt(y*y+(z+z1)**2)/c; // source to sensor 1 reflected
D1 = t21-t11; // multipath delay, sensor 1
WD1 = W*D1;
fac1 = 1+g**2+2*g*SIN(WD1)/WD1;

t12 = sqrt(y*y+(z-z2)**2)/c; // source to sensor 2 direct
t22 = sqrt(y*y+(z+z2)**2)/c; // source to sensor 2 reflected
D2 = t22-t12; // multipath delay, sensor 2
WD2 = W*D2;
fac2 = 1+g**2+2*g*SIN(WD2)/WD2;

if snr=-10, if abs(g)=0.1, disp('BT for MP1,MP2, and TDCA:'), ...
[B*D1,B*D2,B*abs(t12-t11)]

fac = sqrt(fac1*fac2); // I don't know if this is b
if fac<eps, fac=eps; disp('mpsn: numerical failure: zero delay');

csnr = snr/fac; // corrected SNR

```

SIMP.CTR - Simpson's Rule For Numerical Integration

```

// [int] = simp(f)
// integrate f using Simpson's rule. Integral is NORMALIZED.
n = max(size(f));
if round(n/2)*2=n, disp('simp: Need odd number of points');
if n<5, disp('simp: Need at least 5 data points');
int = (f(1)+f(n)+4*sum(f(2:2:n-1))+2*sum(f(3:2:n-2)))/3;
int = int/(n-1);

```

APPENDIX 4

CORRELOGRAM GENERATION PROGRAM

The following are listings of the correlogram and line tracking software.

options/check=all

program xrsda

XRSDA takes .i2 data from xfile and yfile and produces auto- and cross- correlograms and spectrograms stored as .r4 in rxyfile, sxyfile, rxxfile, etc.

The ith line of the cross-correlogram is +/-1024 lags of the biased/unbiased ML/PHAT/SCOT/unnormalized cross-correlation estimate based on nspl*nrps*256 points, beginning at the (d*i)th point of x and y. The lines of the auto-correlograms are 1024 lags of the auto-correlation estimate.

Correlograms are computed as ifft(spectrograms). The spectrograms are computed as peroidograms based on nspl non-overlapping averages of nrps*256 point 8k fft's of x and y.

XRSDA 'decimates' the correlograms and spectrograms for display on the DeAnza. r42mas, daform and flx should be used to create plot files on floppy disks.

declarations

```
implicit none                                !! input/computation variables
character*20 xfile,yfile,rxyfile,sxyfile
character*20 rxxfile,sxxfile,ryyfile,syyfile
character*16 nrmlzn
integer i,ii,iii,j,k,l,itype
integer nspl,nrps,sdf,m,d,nl,nrpl,frf
integer lpco,hpco,nrm
integer*2 x(256,2048),y(256,2048)
real*4 r(2048,3),s(512,3),rtemp(3),scl(3)
logical gtyes,xey,bce
```

```
real*4 temp(1024*64)                        !! ****
integer a,b,c                               !! ****
```

```
integer status,ierr                        !! ap variables
integer xadr,xxadr,yadr,yyadr,wadr,sadr
integer xyadr,tempadr,fts,nc,ne
real*4 apbufr(8192,3),apbufs(4097,3),apbufw(8192)
```

```
integer xch,ych,sxych,rxych                !! i/o variables
```

integer sxxch, rxxch, syych, ryych

initialization

xfile='bvdata:mpc1.i2' !! set default input values
yfile='bvdata:mpc2.i2'
rxyfile='cg:rxy.r4'
sxyfile='cg:sxy.r4'
rxxfile='cg:rxx.r4'
sxxfile='cg:sxx.r4'
ryyfile='cg:ryy.r4'
syyfile='cg:syy.r4'
xey=.false.
nrmlzn='nonePHATSCOTML'

nl=512
nrps=16
m=512
sdf=8
d=1
nsp1=4
lpco=4096
hpco=1
frr=1
nrm=0

xadr=1000 !! ap defaults
xxadr=9200
yadr=17400
yyadr=25600
xyadr=33800
tempadr=42000
sadr=50200
wadr=55000

nc=4097
fts=8192

a=0 !! ****
b=1024*64-1 !! ****
c=2 !! ****

xch=1 !! i/o defaults
ych=2
rxych=3
sxych=4
rxxch=13
sxxch=14
ryych=23
syych=24

input

call clrscrn


```

call otstr('Program XRSDA -- computes the atuo- and cross-',1)
call otstr('          correlogram and spectrogram',1)
call otstr('          of x,y. Output for DeAnza',5)

call gtstr('Enter the name of the input file for x ',xfile,20)
call gtstr('Enter the name of the input file for y ',yfile,20)
call gtstr('Enter the output file-name for Rxy',rxyfile,20)
call gtstr('Enter the output file-name for Sxy',sxyfile,20)
call gtstr('Enter the output file name for Rxx',rxxfile,20)
call gtstr('Enter the output file name for Sxx',sxxfile,20)
call gtstr('Enter the output file name for Ryy',ryyfile,20)
call gtstr('Enter the output file name for Syy',syyfile,20)
call otstr(' ',2)
call gtint('Number of records per processing segment',nrps,16,2)
itemp=int(2048./float(nrps))
call gtint('Number of segments per correlogram line',nspl,itemp,1)
call gtint('Number of records skipped between lines',d,99999,1)
call gtint('Number of the first record read',frr,99999,1)
call gtint('Number of lines computed',nl,512,1)
call otstr(' ',2)
call gtint('0-no normalization, 1-PHAT, 2-SCOT, 3-ML',nrm,3,0)
bce=gtyes('Biased correlation estimates (y/n):')
call otstr(' ',2)
call gtint('Enter low pass cut off -- 4096 bins ',lpco,4097,1)
call gtint('Enter high pass cut off -- 4096 bins',hpco,lpco,0)

```

```

call clrscrn                                !! print input values

```

```

call otstr('Data entered:',2)
write(6,120) xfile
format(' data source 1:',a20)
write(6,130) yfile
format(' data source 2:',a20)
write(6,140) rxyfile
format(' Rxy:',a20)
write(6,150) sxyfile
format(' Sxy:',a20)
write(6,141) rxxfile
format(' Rxx:',a20)
write(6,142) sxxfile
format(' Sxx:',a20)
write(6,143) ryyfile
format(' Ryy:',a20)
write(6,144) syyfile
format(' Syy:',a20)
call otstr('S',1)
write(6,160) (nspl*nrps)
format(' # of 256 pt records per correlogram line :',i6)
write(6,170) d
format(' # of 256 pt records skipped between lines:',i6)
write(6,196) (frr-1)
format(' # of records skipped before the 1st line :',i6)
write(6,180) nl
format(' # of correlogram lines          :',i4)
write(6,194) nrps
format(' # of records processed per 8k fft:',i4)
call otstr('#',1)
write(6,192) (nrmlzn(nrm*4+1:nrm*4+4))

```

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```
main loop -- get data, compute correlogram lines
```

```
do 230 j=1,n1
```

```
if (j .eq. 1) then                !! first data set -- read
                                   !! nrpl records
```

```
    call rrecxy(xch,x(1,1),ych,y(1,1),frr,frr+nrpl-1,xey)
```

```
else                                !! not first data set --
```

```
    if (d .ge. nrpl) then        !! d># -- fresh data
```

```
        ii=(j-1)*d+frr
```

```
        iii=ii+nrpl-1
```

```
        call rrecxy(xch,x(1,1),ych,y(1,1),ii,iii,xey)
```

```
    else                            !! make room for d
```

```
                                   !! records new data
```

```
        do 260 i=1,nrpl-d
```

```
        do 270 ii=1,256
```

```
        y(ii,i)=y(ii,i+d)
```

```
        x(ii,i)=x(ii,i+d)
```

```
        continue
```

```
                                   !! get d new records
```

```
                                   !! put at end of x,y
```

```
        iii=(j-1)*d+nrpl+frr
```

```
        ii=iii-d+1
```

```
        i=nrpl-d+1
```

```
        call rrecxy(xch,x(1,i),ych,y(1,i),ii,iii,xey)
```

```
    endif
```

```
endif
```

```
ap computations
```

```
if (j.eq.1) then
```

```
    call apinit(0,0,status)
```

```
                                   !! initialize ap
```

```
    call vclr(0,1,65535)
```

```
                                   !! clear ap
```

```
    call apwr
```

```
                                   !! load constants
```

```
    call apput(apbufw,wadr,8192,2)
```

```
    call apwd
```

```
else
```

```
    call vclr(1000,1,53500)
```

```
                                   !! clear all but window
```

```
endif
```

```
do l=1,nspl
```

```
                                   !! process x,y
```

```
call vclr(xadr,1,2*ne)
```

```
                                   !! clear data area
```

```
call vclr(yadr,1,2*ne)
```

```

c
c
call apwr                                !! x,y --> ap
call apput(x(1,(1-1)*nrps+1),xadr,ne,1)
call apput(y(1,(1-1)*nrps+1),yadr,ne,1)
call apwd

c
c
call vflt(xadr,1,xadr,1,ne)              !! convert to reals
call vflt(yadr,1,yadr,1,ne)

c
c
call rfft(xadr,fts,1)                    !! take 8k fft's
call rfft(yadr,fts,1)
call rfftsc(xadr,fts,3,1)                !! scale/undo wierd packing
call rfftsc(yadr,fts,3,1)

c
c
call vmov(xyadr,1,tempadr,1,fts+2)        !! conj(X)*Y+sum --> xyadr
call cvma(xadr,2,yadr,2,tempadr,2,xyadr,2,nc,-1)

c
c
call vmov(xxadr,1,tempadr,1,nc)           !! conj(X)*X+sum --> xxadr
call scjma(xadr,2,tempadr,1,xxadr,1,nc)

c
c
call vmov(yyadr,1,tempadr,1,nc)           !! conj(Y)*Y+sum --> yyadr
call scjma(yadr,2,tempadr,1,yyadr,1,nc)

c
c
c
c
enddo                                    !! get new x,y

c
c
c
if (nrm.eq.2) then                        !! SCOT
c
    call vmul(yyadr,1,xxadr,1,tempadr,1,nc)
    call vsqrt(tempadr,1,sadr,1,nc)        !! (xx*yy)**0.5
    call crvdiv(xyadr,2,sadr,1,tempadr,2,nc) !! SCOT
    call vmov(tempadr,1,xyadr,1,2*nc)
c
endif

c
c
c
if (nrm.eq.1) then                        !! PHAT
c
    call vmov(xyadr,1,tempadr,1,nc*2)
    call cvmags(tempadr,2,xyadr,1,nc)      !! magnitude**2
    call vsqrt(xyadr,1,sadr,1,nc)          !! sqrt(mag**2)
    call crvdiv(tempadr,2,sadr,1,xyadr,2,nc) !! PHAT
c
endif

c
c
c
if (nrm.eq.3) then                        !! ML

```

```

call cvmags(xyadr,2,sadr,1,nc)          !! mag**2(xy)
call vsqrt(sadr,1,tempadr,1,nc)         !! mag(xy)
call vclr(xadr,1,2*nc)
call crvdiv(xyadr,2,tempadr,1,xadr,2,nc) !! phase(xy)
call vclr(yadr,1,2*nc)
call vmul(xxadr,1,yyadr,1,yadr,1,nc)    !! xx*yy
call vsub(sadr,1,yadr,1,xyadr,1,nc)     !! xx*yy-xy**2
call vdiv(xyadr,1,sadr,1,tempadr,1,nc)  !! xy**2/(...)
call crvmul(xadr,2,tempadr,1,xyadr,2,nc) !! ML

endif

call vmov(xyadr,1,tempadr,1,fts+2)      !! mag of Sxy
call cvmags(tempadr,2,sadr,1,nc)
call vmov(sadr,1,tempadr,1,nc)
call vsqrt(tempadr,1,sadr,1,nc)

call apwr
call apget(apbufs(1,1),sadr,nc,2)       !! xy-->apbuf
call apget(apbufs(1,2),xxadr,nc,2)     !! xx-->apbuf
call apget(apbufs(1,3),yyadr,nc,2)     !! yy-->apbuf
call apwd

if (hpco.ne.0) then                    !! lp filter
    call vclr(xyadr,1,2*hpco)          !! Sxy, Sxx, Syy
    call vclr(xxadr,1,hpco)
    call vclr(yyadr,1,hpco)
endif

if (lpco.ne.4097) then                !! hp filter
    call vclr(xyadr+2*lpco,1,2*nc-2*lpco) !! Sxy, Sxx, Syy
    call vclr(xxadr+lpco,1,nc-lpco)
    call vclr(yyadr+lpco,1,nc-lpco)
endif

call vmov(xxadr,1,tempadr,1,nc)        !! make Sxx cplx
call vclr(xxadr,1,2*nc)
call vmov(tempadr,1,xxadr,2,nc)

call vmov(yyadr,1,tempadr,1,nc)        !!make Syy cplx
call vclr(yyadr,1,2*nc)
call vmov(tempadr,1,yyadr,2,nc)

call rfftsc(xyadr,fts,-3,0)            !! pack for ifft
call rfftsc(xxadr,fts,-3,0)

```

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```
do 321 i=1,512                                !! fill Rxx,Ryy
```

```
do k=2,3
r(i,k)=apbufr(i,k)/scl(k)
rtemp(k)=0.
enddo
```

```
321 continue
```

```
l=0
do k=1,3
rtemp(k)=0.
enddo
```

```
do 322 i=1,1024                                !! fill Rxy
```

```
rtemp(1)=rtemp(1)+apbufr(i,1)**2
rtemp(2)=rtemp(2)+apbufr(7168+i,1)**2
```

```
if (mod(i,4).eq.0) then
    l=l+1
    r(256+l,1)=rtemp(1)/((scl(1)**2)*4.)
    r(1,1)=rtemp(2)/((scl(1)**2)*4.)
    rtemp(1)=0.
    rtemp(2)=0.
endif
```

```
322 continue
```

```
call wrec(rxych,r(1,1),4*j-3,4*j)                !! write r,s
call wrec(sxych,s(1,1),4*j-3,4*j)
call wrec(rxxch,r(1,2),4*j-3,4*j)
call wrec(sxxch,s(1,2),4*j-3,4*j)
call wrec(ryych,r(1,3),4*j-3,4*j)
call wrec(syych,s(1,3),4*j-3,4*j)
```

```
call otstr(':',0)
```

```
30 continue
```

```
call cls(xch)                                !! close data files
call cls(ych)
```

```
call cls(rxych)                                !! close output files
```

```
call cls(sxych)
call cls(rxxch)
call cls(sxxch)
call cls(ryych)
call cls(syych)
```

```
c
call otstr(' ',1)
call otstr('...files written',1)
c
c
c
c
stop
end
c
c
include 'dra2:[abel.jsalib]jsaio.for/list'    !! get i/o
```



```
file i/o subroutines -- records
written as 512 byte blocks
```

```
subroutine opn(ch,nam,oon)
```

```
opens file w/ name=nam on unit ch
```

```
implicit none
integer ch,ios
character*(*) nam
character*(3) oon
```

```
!! open file
```

```
open(unit=ch,name=nam,status=oon,err=100,iostat=ios,
x      recordtype='fixed',recordsize=512/4,access='direct',
x      organization='sequential',blocksize=512*64)
return
100 call prterr('opn error',ios)      !! print error
return
end
```

```
subroutine cls(ch)
```

```
closes file on unit ch
```

```
implicit none
integer ch,ios
```

```
close(unit=ch,status='keep',err=100)      !! close file
return
```

```
100 call prterr('cls error',ios)      !! print error
return
end
```

```
subroutine rrecxy(chx,xbuf,chy,ybuf,sr,fr,xey)
```

```
reads starting sr finnishng fr: chx-->xbuf, chy-->ybuf
if xey sets ybuf=xbuf -- no chy exists
```

```
implicit none
integer chx,chy,nrcds,sr,fr,i
byte xbuf(abs((fr-sr+1)*512)),ybuf(abs((fr-sr+1)*512))
logical xey
```

```

c
c
c      call rrec(chx,xbuf,sr,fr)                !! read x's records
c
c      if (xey) then                            !! xey-->set y=x
c          nrcds=fr-sr+1
c          do 200 i=1,nrcds*512
200      ybuf(i)=xbuf(i)
c      else
c          call rrec(chy,ybuf,sr,fr)            !! else read y's records
c      endif
c
c      return
c      end
c
c
c
c
c      subroutine rrec(ch,buf,sr,fr)
c
c      reads fr-sr 512 byte records from ch to buf,  starting at
c      record sr finishing at fr
c
c      implicit none
c      integer sr,fr,ch,ios,i,s,j
c      byte buf(abs((fr-sr+1)*512)),temp(512)
c
c
c      if (sr .gt. fr) then                      !! starting record after
c          ios=999                              !! ending record
c          goto 200
c      endif
c
c      do 100 i=sr,fr                          !! read records sr...fr
c
c      read(unit=ch,rec=i,err=200,iostat=ios)temp
c
c      s=(i-sr)*512                            !! put read buffer in
c      do j=1,512                              !! return variable, buf
c      buf(j+s)=temp(j)                        !! 512 bytes/record
c      enddo
c
c      100 continue
c
c      return
c
c      200 call prterr('rrec err',ios)          !! print errors
c      return
c      end
c
c
c
c
c      subroutine wrec(ch,buf,sr,fr)
c
c      writes buf to ch in 512 byte records --

```

starting at record sr, finishing at fr

implicit none

integer s,ch,sr,fr,ios,i,j

byte buf(abs((fr-sr+1)*512)),temp(512)

```
if (sr .gt. fr) then          !! starting record after
    ios=999                  !! last record
    go to 200
```

endif

```
do 100 i=sr,fr                !! write records sr...fr
```

s=(i-sr)*512

do j=1,512

```
temp(j)=buf(j+s)             !! fill write buffer --
```

```
enddo                         !! 512 bytes/record
```

```
write(unit=ch,rec=i,err=200,iostat=ios)temp
```

return

```
call prtterr('wrec error',ios) !! print errors
```

return

end

terminal i/o routines

subroutine otstr(str,nlf)

prints str, on the current line, followed by nlf cr/linefeeds

implicit none

integer nlf,l

character*(*) str

```
write(6,100)str               !! prints string to terminal
```

```
format(1h+,a,$)
```

```
if (nlf .lt. 1) return        !! prints lf's
```

```
do 200 l=1,nlf
```

```
write(6,300)
```

```
format(' ')
```

```
continue
```

```
return
```

end

```

c
c
c
subroutine gtstr(pt,var,n)
c
c gets a string from the terminal -- prompts w/ pt, var=string
c var has length n<101
c
c implicit none
c character*(*) pt,var
c integer n,i,nchrs
c character*100 invar
c
c i=min(len(var),index(var,' '))
c write(6,100) pt,var !! write prompt, default
100 format(' ',a,' (' ,a<i>,' ):',$)
c
c read(5,200)nchrs,(invar(i:i),i=1,nchrs) !! read string
200 format(q,100a1)
c
c if (nchrs .eq. 0) return !! return default
c do 300 i=1,n
c var(i:i)=' '
300 if (i .le. nchrs) var(i:i)=invar(i:i) !! fill return variable
c return
c end
c
c
c subroutine gtint(pt,igr,mx,mn)
c
c gets integer from terminal -- prompts user w/ pt, accepts
c igr in range (mn,mx)
c
c
c
c implicit none
c character*10 itstr
c integer igr,mx,mn,it,nchrs,i,lmn,lmx
c character*(*)pt
c
c i=2+max(1,int(log10(abs(float(igr))+.1)))
c write(6,100)pt,igr !! write prompt, default
100 format(' ',a,' (' ,i<i>,' ):',$)
c
c read(5,400)nchrs,(itstr(i:i),i=1,10) !! get string
200 format(q,10a1)
400
c
c if (nchrs .eq. 0) return !! take default if no
c !! entry
c call s2i(it,itstr) !! convert str-->int
c
c if ((it .le. mx) .and. (it .ge. mn)) then !! check range
c igr=it
c return
c endif
c lmn=2+max(1,int(log10(abs(floatj(mn))+.1)))
c lmx=2+max(1,int(log10(abs(floatj(mx))+.1)))
c write(6,300)mn,mx !! not in range

```

```

300    format(' The (min,max)are (' ,i<lmn>',' ,i<lmx>',' ) -- reenter:',$)
      go to 200
      end

```

```

      subroutine s2i(itr,str)

```

```

      converts string -- str -- to integer -- itr.

```

```

      implicit none
      integer a,l
      integer itr,i,j,temp,pt
      character*(*) str

```

```

      temp=0

```

```

      pt=1

```

```

      l=len(str)

```

```

      do 100 i=0,l-1

```

```

                                !! itr=sum(str(i)*10**i)

```

```

      a=ichar(str(l-i:l-i))

```

```

      if (a .eq. 48) go to 200

```

```

                                !! a='0'

```

```

      if (a .eq. 45) go to 300

```

```

                                !! a='-'

```

```

      if ((a .lt. 49) .or. (a .gt. 57)) go to 100 !! a not in 1--9

```

```

      temp=temp+pt*(a-48)

```

```

200    pt=pt*10

```

```

300    continue

```

```

      itr=temp

```

```

      return

```

```

00    itr=-temp

```

```

      return

```

```

      end

```

```

      subroutine gtrel(pt,rel,mx,mn)

```

```

      gets real*4 from terminal -- prompts user w/ pt, accepts
                                rel in range (mn,mx)

```

```

      implicit none

```

```

      character*10 rlstr

```

```

      real*4 rel,mx,mn,rl

```

```

      integer nchrs,i,lmx,lmn

```

```

      character*(*)pt

```

```

      write(6,100)pt,rel

```

```

                                !! write prompt, default

```

```

      format(' ',a,' (' ,f<5+max(1,int(log10(abs(rel)+.1)))>.3,' ):',$)

```

```

000    read(5,400)nchrs,(rlstr(i:i),i=1,10)

```

```

                                !! get string

```

```

000    format(q,10a1)

```

```

      if (nchrs .eq. 0) return

```

```

                                !! take default if no

```

```

c                                     !! entry
c      call s2r(rl,rlstr)             !! convert str-->int
c
c      if ((rl .le. mx) .and. (rl .ge. mn)) then      !! check range
c          rel=rl
c          return
c      endif
c      lmx=5+max(1,int(log10(abs(mx)+.1)))
c      lmn=5+max(1,int(log10(abs(mn)+.1)))
c      write(6,300)mn,mx                !! not in range
300  format(' The (min,max)are (' ,f<lmn>.3,' ,',f<lmx>.3,')
x      -- reenter:',$)
c      go to 200
c      end
c
c
c
c      subroutine s2r(r,str)
c
c      converts string -- str -- to real -- r.
c
c      implicit none
c      integer a,l,i,j
c      real*4 r,temp,pt
c      character*(*) str
c
c      temp=0.
c      pt=1.
c      l=len(str)
c
c      do 100 i=0,l-1                    !! itr=sum(str(i)*10**i)
c          a=ichar(str(l-i:l-i))
c          if (a .eq. 45) go to 300        !! a='-'
c          if (a .eq. 48) go to 200        !! a='0'
c          if (a .eq. 46) then            !! a='.'
c              temp=temp/pt
c              pt=1.
c              go to 100
c          endif
c          if ((a .lt. 49) .or. (a .gt. 57)) go to 100 !! a not in 1--9
c          temp=temp+pt*float(a-48)
200  pt=pt*10.
100  continue
c      r=temp
c
c      return
c
c      r=-temp
c
c
c      return
c      end
c
c
c
c      subroutine clrscrn
c

```

clears the screen

byte sbuf(4)

sbuf(1)=27 ! ESC

sbuf(2)=91 ! [

sbuf(3)=50 ! 2

sbuf(4)=74 ! J

write(6,100)(sbuf(i),i=1,4)

format(lh+,4al)

return

end

logical function gtyes(pt)

prompts user w/ pt, returns .true. if 'yes'

implicit none

character ystr

character*(*) pt

gtyes=.false.

write(6,100) pt

!! write prompt

format(' ',a,\$)

read(5,200) ystr

!! get response

format(al)

if ((ystr .eq. 'y') .or. (ystr .eq. 'Y')) gtyes=.true.

return

!! true if first

end

!! character is y or Y

subroutine prterr(msg,ios)

prints runtime error codes

character*(*) msg

integer ios

write(6,100) msg,ios

!! write message and code

format(' ',a,':',i4)

!! to terminal

return

end

APPENDIX 4
ADEC LINETRACKER SOFTWARE


```

integer*4      number_of_points
integer*4      output_file_number
integer*4      starting_point
character*20    temp_string
character*80    oname,iname,tfnam
integer*4      och(4),ich
logical        gtyes

```

initialization

```

do i=1,4
och(i)=14+i
enddo
ich=2
iname='data:rxystest.r4'
oname='data:rxylgm.r4'
tfnam='data:track.fil'
number_of_points=100
sl=1
nbins=512
sbin=1
scl=1.
thr=2.
pct=.7

```

input

```

100 call gtstr('Enter the output gram file name',oname,80)
call gtstr('Enter the output track file name',tfnam,80)
call gtstr('Enter the input file name',iname,80)
call gtint('Enter the number of epochs',number_of_points,700,1)
call gtint('Enter the starting epoch number',sl,9999,1)
call gtint('Enter the number of fft bins',nbins,99999,1)
call gtint('Enter the starting bin number',sbin,99999,1)
call gtrel('Enter the input scale factor',scl,99999,..00001)
call gtrel('Enter the pw threshold',thr,99.,1.)
call gtrel('Enter the pw percent',pct,1.,0.)
call otstr(' ',2)
if (.not.gtyes('Inputs ok (y/n): ')) go to 100
call otstr(' ',5)

call opn(och,oname,'new')
call opn(ich,iname,'old')
call adecini(number_of_points)

```

body

```

starting_point = 1

```

```

call lfcr

```

call percom (0, number_of_points, 5)

do i = 1, number_of_points

call percom (i, number_of_points, 5)

call adecrd (ich,i,fft_amplitudes,sl,scl,nbins,sbin)

!! read in an FFT line and normalize

starting_point = starting_point + 512

call doadec (fft_amplitudes) ! process FFT line

if (mod (i, 175) .eq. 1 .and. i .ne. 1) then

call abelfin (och,gram_number, gram)

do j = 1, 89600

gram (j) = 0

end do

gram_number = gram_number + 1

temp_string = 'adec' // char (gram_number + 48) // '.grm'

call opn(och(gram_number),temp_string,'new')

end if

call adecgram (mod (i - 1, 175) + 1, gram) ! output adec results

call writestuff(i,fft_amplitudes,thr,pct,number_of_points,tfnam)

end do

call abelfin (och, gram_number, gram)

call cls(ich)

end

include 'jsaio.for'

!! get jsa's i/o

subroutine abelfin(ch,gn,x)

writes gram -- x to channel ch(gn)

implicit none

integer*4 ch(4),gn,i,j

real temp(512),x(512,175)

do i=1,512

temp(i)=0

enddo

do 1000 i=1,175

do 2000 j=1,512

temp(j)=x(j,i)

continue

call wrec(ch(gn),temp,4*(i-1)+1,4*i)

continue

call cls(ch(gn))

end

subroutine assoc (association_threshold, association_gate_min,
1 association_gate_max, association_gate_slope, fft_amplitude,
1 fft_associated, max_fft_bin_number)

implicit none

real association_gate_max
real association_gate_min (1)
real association_gate_slope (1)
real association_threshold
real fft_amplitude (1)
logical*1 fft_associated (1)
integer max_fft_bin_number

real association_gate
integer bin
logical*1 lower_edt
real lower_limit
integer lower_limit_bin
integer other_track
integer track
logical*1 upper_edt
real upper_limit
integer upper_limit_bin

include 'tracks.inc'

```

do bin = 1, max_fft_bin_number
  fft_associated ( bin) = .false.
end do

```

```

do track = 1, number_of_tracks

```

```

  if ( t_adaptive_amplitude ( track) .gt. association_threshold) then

```

```

    association_gate =
1      association_gate_min ( t_type ( track)) +
1      association_gate_slope ( t_type ( track)) *
1      ( t_adaptive_amplitude ( track) - association_threshold)

```

```

    association_gate =
1      min ( association_gate, association_gate_max)

```

```

  else

```

```

    association_gate = association_gate_min ( t_type ( track))

```

```

  end if

```

```

  upper_limit = min ( t_frequency ( track) + association_gate,
1    float ( max_fft_bin_number))
  lower_limit = max ( t_frequency ( track) - association_gate, 1.)

```

```

c    Check for to see if any higher frequency edt track will affect the
c    upper limit of the association.

```

```

  do other_track = track + 1, number_of_tracks
    if ( t_type ( other_track) .eq. edt) then
      upper_edt = .true.
      goto 1000
    end if
  end do

```

```

  upper_edt = .false.

```

```

1000  continue

```

```

  if ( upper_edt) then
    upper_limit_bin = min( upper_limit,
1      ( t_frequency ( track) + t_frequency ( other_track)) * .5)
1      + 0.5
  else
    upper_limit_bin = upper_limit + .5
  end if

```

```

c    Check to see if any lower frequency edt track will affect
c    the lower limit of the association

```

```

  do other_track = track - 1, 1, -1
    if ( t_type ( other_track) .eq. edt) then
      lower_edt = .true.
      goto 2000
    end if
  end do

```

```
lower_edt = .false.
```

000

```
continue
```

```
if ( lower_edt) then
```

```
1       lower_limit_bin = max ( lower_limit,  
1       ( t_frequency ( track) + t_frequency ( other_track)) * .5)  
        + .5
```

```
else
```

```
    lower_limit_bin = lower_limit + .5  
end if
```

c Associate cell(s) with track.

```

t_associated_amplitude ( track) = fft_amplitude ( lower_limit_bin)
t_associated_cell ( track) = lower_limit_bin
do bin = lower_limit_bin, upper_limit_bin
  if ( fft_amplitude ( bin) .gt. t_associated_amplitude ( track))
1    then

      t_associated_amplitude ( track) = fft_amplitude ( bin)
      t_associated_cell ( track) = bin

    end if
    if ( t_type ( track) .eq. edt) fft_associated ( bin) = .true.
      ! all tracks in window of edt are associated
end do

fft_associated ( t_associated_cell ( track)) = .true.

if ( t_associated_amplitude ( track) .lt.
1   t_adaptive_amplitude ( track)) then

    t_dcell ( track) = ( t_associated_cell ( track) -
1      t_frequency ( track)) * ( t_associated_amplitude ( track) /
1      t_adaptive_amplitude ( track))

  else

    t_dcell ( track) = t_associated_cell ( track) -
1      t_frequency ( track)

  end if

end do

end
real function besseli0 ( x)

real          x

real          arg
real          b
integer       i
real          term

b = 1
arg = x * x * .25
term = 1

do i = 1, 25

  term = term * arg / float ( i) ** 2
  if ( abs ( term / b) .lt. 1e-4) goto 1000
  b = b + term

end do

```

```

1000  besseli0 = b

      end
      subroutine cmlne ( window_size, upper, lower, ns, rx, x)

      implicit complex*8 ( a - z)

      integer*4      window_size
      integer*4      upper
      integer*4      lower
      integer*4      ns
      real           rx ( *)
      real           x ( *)

      integer*4      i
      integer*4      j
      real           list ( 64)
      real           mean
      real           temp

      Build first list

      do i = 1, window_size
        list ( i) = rx ( i)
      end do

      Sort list ( crudely right now.)

      do i = 1, window_size
        do j = i + 1, window_size
          if ( list ( i) .gt. list ( j)) then
            temp = list ( j)
            list ( j) = list ( i)
            list ( i) = temp
          end if
        end do
      end do

      Calculate mean

      mean = 0.
      do i = lower, upper
        mean = mean + list ( i)
      end do
      mean = mean / float ( upper - lower + 1)

      Calculate noise estimate for left end of data

      do i = 1, window_size / 2
        x ( i) = mean
      end do

      Calculate noise estimate for middle of data

      do i = window_size / 2 + 1, ns - window_size / 2
        call sort0 ( list, window_size, rx ( i - window_size / 2))

```

```
      call sorti ( list, window_size, rx ( i + window_size / 2))  
      call aver ( list, upper, lower, mean)  
      x ( i) = mean  
end do
```

c Calculate noise estimate for right end of data

```
do i = ns - window_size / 2 + 1, ns  
  x ( i) = mean  
end do  
  
end
```



```
block data

include      'tracks.inc'

data free_entry / 1/
data number_of_tracks / 0/

end
subroutine adecfin ( output_file_number, gram)

implicit      none

real          gram ( 58100)
integer*4     output_file_number

real          buffer ( 512)
integer       buffer_pointer
integer       i
integer       j
integer*4     page

page = 0
buffer_pointer = 1

do i = 1, 332
  do j = 1, 175

    buffer ( buffer_pointer) = gram (( j - 1) * 332 + i)
    if ( buffer_pointer .eq. 512) then
      call ptpage ( page, output_file_number, buffer)
      page = page + 1
      buffer_pointer = 0
    end if

    buffer_pointer = buffer_pointer + 1

  end do
end do

Zero pad last page.

do i = buffer_pointer, 512
  buffer ( i) = 0.
end do

call ptpage ( page, output_file_number, buffer)
call nclose ( output_file_number)

end
subroutine adecgram ( i, gram)

implicit      none

real          gram ( 512, 175)
integer       i

integer       bin
integer       track
```

```
include      'tracks.inc'

do bin = 1, 512
  gram ( bin, i) = 0.
end do

do track = 1, number_of_tracks
  bin = t_frequency ( track) + .5
  if ( t_detection_flag ( track)) then
    gram ( bin, i) = 7.
  else
    gram ( bin, i) = 2.
  end if
end do

end

subroutine adecini(number_of_points)

implicit      none

integer*4      number_of_points
character*80    coefficient_file_name
logical*1      error
integer        i
real           new_track_pfa
real           old_track_pd
real           old_track_pfa
character*80    output_file_name
character*80    param_file_name
integer*4      param_unit
integer*4      range ( 2)
real           temp_real

include      'jhjlib.inc'
include      'param.inc'
```

```

call getjfn ( param_unit)
error = .false.
100 param_file_name = 'adec.prm'
if ( error) call outmes ( 'Couln't find file. Try again.')
error = .true.
call askstr ( 'Adec parameter file', param_file_name)
open ( unit = param_unit, err = 100, type = 'old', readonly,
1 form = 'formatted', file = param_file_name)

Read in adec paramters

type 1000

read ( param_unit, *) amplitude_smoothing_constant
type 1001, 'amplitude_smoothing_constant', amplitude_smoothing_constant
read ( param_unit, *) association_gate_min ( 1)
type 1001, 'association_gate_min', association_gate_min ( 1)
read ( param_unit, *) association_gate_max
type 1001, 'association_gate_max', association_gate_max
do i = 1, 3
    read ( param_unit, *) association_gate_slope ( i)

    type 1001, 'association_gate_slope ' // char (i + 48),
1 association_gate_slope ( i)
end do
read ( param_unit, *) association_threshold
type 1001, 'association_threshold', association_threshold
read ( param_unit, *) old_track_pd
type 1001, 'old_track_pd', old_track_pd
read ( param_unit, *) old_track_pfa
type 1001, 'old_track_pfa', old_track_pfa
detection_threshold = log ( old_track_pd / old_track_pfa)
drop_threshold = log (( 1. - old_track_pd) / ( 1. - old_track_pfa))
read ( param_unit, *) temp_real
display_threshold = detection_threshold + temp_real
type 1001, 'display_threshold', display_threshold
read ( param_unit, *) dynamic_tracking_threshold
type 1001, 'dynamic_tracking_threshold', dynamic_tracking_threshold
read ( param_unit, *) faca
type 1001, 'faca', faca
read ( param_unit, *) log_likelihood_max
type 1001, 'log_likelihood_max', log_likelihood_max
read ( param_unit, *) max_fft_bin_number
type 1002, 'max_fft_bin_number', max_fft_bin_number
read ( param_unit, *) merge_gate
type 1001, 'merge_gate', merge_gate
read ( param_unit, *) rate_gate
type 1001, 'rate_gate', rate_gate
read ( param_unit, *) new_track_pfa
type 1001, 'new_track_pfa', new_track_pfa

close ( unit = param_unit)

type 1003

do i = 1, 3
    new_track_threshold ( i) = sqrt ( -2. * log ( new_track_pfa))
end do

```

```

association_gate_min ( 2) = association_gate_min ( 1)
association_gate_min ( 3) = association_gate_min ( 1)

detection_threshold = log ( old_track_pd / old_track_pfa)
drop_threshold = log (( 1. - old_track_pd) / ( 1. - old_track_pfa))

```

```

1000 format ( '0Adec parameters:'//)
1001 format ( 1x, a, '-', g13.6)
1002 format ( 1x, a, '-', i13)
1003 format ( '0')

```

```

end
subroutine adecrd ( ch, starting_point,
1    fft_amplitudes, sl, scl,nbins,sbin)

```

```

real          fft_amplitudes ( *),scl
integer*4      ch,sl,i,j,k,nbins,sbin
integer*4      starting_point

```

```

complex        coefficient_array ( 512)
real           nse ( 512)
real           temp ( 512)
real           temp2 ( 9999)

```

```

include        'jhjlib.inc'

```

c
c
c

```

j=(sl+starting_point-2)*nbins+sbin
k=int(float(j)/128)+1
l=k+int(float(nbins)/128)+1
call rrec(ch,temp2,k,l)

```

```

ii=j-(k-1)*128+1

```

```

do i=1,512
temp(i)=scl*temp2(i+ii)
enddo

```

c
c
c

```

call cmlne ( 32, 16, 1, 512, temp, nse)

```

```

do i = 1, 512
    fft_amplitudes ( i) = scl*temp2 ( i+ii) / sqrt(nse(i))*0.558
end do

```

```

end
program adecw

```

```

implicit none

```

```

integer*4      coefficient_file_number
real           fft_amplitudes ( 512), scl, thr, pct
real           gram ( 89600)
integer        gram_number / 1/
integer        i,j
integer*4      sl,sbin,nbins

```

```
subroutine sort0 ( list, window_size, value)
```

```
real          list ( 1)  
integer*4     window_size  
real          value
```

```
integer*4     i  
integer*4     j
```

```
do i = 1, window_size  
  if ( value .eq. list ( i)) goto 100  
end do
```

```
100 continue
```

```
Compress list
```

```
do j = i, window_size - 1  
  list ( j) = list ( j + 1)  
end do
```

```
end
```

subroutine sorti (list, window_size, value)

real list (1)
integer*4 window_size
real value

integer*4 i
integer*4 j
real temp1
real temp2

do i = 1, window_size - 1
if (value .lt. list (i)) then
goto 100
end if
end do

i = window_size

100 continue

temp2 = value

c Compress list

do j = i, window_size
temp1 = list (j)
list (j) = temp2
temp2 = temp1
end do

end

```

subroutine aver ( list, upper, lower, mean)

real          list ( 1)
integer*4     upper
integer*4     lower
real          mean

mean = 0.

do i = lower, upper
    mean = mean + list ( i)
end do

mean = mean / float ( upper - lower + 1)

end
subroutine compress

implicit none

integer       target_track
integer       track
integer       track_counter

include       'tracks.inc'

track_counter = 0
target_track = 1

do track = 1, free_entry - 1

    if ( t_frequency ( track) .ge. 0) then

        track_counter = track_counter + 1
        if ( track .ne. target_track) then

            t_adaptive_amplitude ( target_track) =
1            t_adaptive_amplitude ( track)
            t_age ( target_track) = t_age ( track)
            t_associated_amplitude ( target_track) =
1            t_associated_amplitude ( track)
            t_associated_cell ( target_track) =
1            t_associated_cell ( track)
            t_dcell ( target_track) = t_dcell ( track)
            t_detection_flag ( target_track) =
1            t_detection_flag ( track)
            t_frequency ( target_track) = t_frequency ( track)
            t_frequency_rate ( target_track) =
1            t_frequency_rate ( track)
            t_id ( target_track) = t_id ( track)
            t_log_likelihood ( target_track) =
1            t_log_likelihood ( track)
            t_type ( target_track) = t_type ( track)

        end if

        target_track = target_track + 1
    end if
end do

```

```
        end if

    end do

    number_of_tracks = track_counter
    free_entry = number_of_tracks + 1

    end
    subroutine deltra ( track)

    implicit none

    integer          track

    include          'tracks.inc'

    t_frequency ( track) = -1.0

    end
    subroutine loader ( fft_amplitudes)

    implicit none

    real             fft_amplitudes ( *)

    real             alpha ( 32) / 10 * .18750, .20099, .21301, .22601,
1                   .23700, .24899, .26099, .28125, .30600, .32999,
1                   .36499, 12 * .37900/

    real             beta ( 32) / 9 * .87500, .01941, .02246, .02637,
1                   .02863, .03186, .03640, .03918, .04602, .05527,
1                   .06522, .07661, 12 * .08862/

    logical*1        fft_associated ( 512)

    include          'param.inc'
    include          'tracks.inc'
```


Associate existing tracks with FFT cells.

```
call assoc ( association_threshold, association_gate_min,  
1  association_gate_max, association_gate_slope, fft_amplitudes,  
1  fft_associated, max_fft_bin_number)
```

Update existing tracks.

```
call update ( amplitude_smoothing_constant, detection_threshold,  
1  display_threshold, drop_threshold, log_likelihood_max)
```

Create new tracks.

```
call newtra ( fft_amplitudes, fft_associated, max_fft_bin_number,  
1  new_track_threshold)
```

Put the track table back into order of increasing frequency.

```
call sort
```

Merge equivalent tracks.

```
call merge ( merge_gate, rate_gate)
```

Smooth and predict new frequency and rate.

```
call smooth ( dynamic_tracking_threshold, faca, alpha, beta,  
1  max_fft_bin_number)
```

end

```
subroutine domerg ( track1, track2)
```

implicit none

```
integer      track1  
integer      track2
```

```
integer      deleted_track  
integer      retained_track
```

```
include      'tracks.inc'
```

```
if (( t_type ( track1) .eq. edt) .and. ( t_type ( track2) .eq. edt))
1  then

    if ( t_detection_flag ( track1) .eq. t_detection_flag ( track2))
1  then

        if ( t_adaptive_amplitude ( track1) .ge.
1      t_adaptive_amplitude ( track2)) then

            retained_track = track1

        else

            retained_track = track2

        end if

    else

        if ( t_detection_flag ( track1)) then

            retained_track = track1

        else

            retained_track = track2

        end if

    end if

else if ( t_type ( track1) .eq. edt) then

    retained_track = track1

else if ( t_type ( track2) .eq. edt) then

    retained_track = track2

else

    if ( t_log_likelihood ( track1) .gt. t_log_likelihood ( track2))
1  then

        retained_track = track1

    else if ( t_log_likelihood ( track1) .lt.
1  t_log_likelihood ( track2)) then

        retained_track = track2

    else if ( t_adaptive_amplitude ( track1) .gt.
1  t_adaptive_amplitude ( track2)) then

        retained_track = track1

    else
```

```
        retained_track = track2

    end if

end if

if ( retained_track .eq. track1) then
    deleted_track = track2
else
    deleted_track = track1
end if

if ( t_age ( track1) .ge. t_age ( track2)) then
    t_id ( retained_track) = t_id ( track1)
else
    t_id ( retained_track) = t_id ( track2)
end if

t_age ( retained_track) = max ( t_age ( track1), t_age ( track2))

call deltra ( deleted_track)

end
file i/o subroutines -- records
written as 512 byte blocks
```

```
subroutine opn(ch,nam,oon)
```

```
opens file w/ name=nam on unit ch
```

```
implicit none
integer ch,ios
character*(*) nam
character*(3) oon
```

```
!! open file
```

```
open(unit=ch,name=nam,status=oon,err=100,iostat=ios,
x      recordtype='fixed',recordsize=512/4,access='direct',
x      organization='sequential',blocksize=512*64)
```

```
return
call prterr('opn error',ios)      !! print error
return
end
```

```
subroutine cls(ch)
```

```
closes file on unit ch
```

```
implicit none
```

```

integer ch,ios
c
close(unit=ch,status='keep',err=100)          !! close file
return
c
100 call prterr('cls error',ios)                !! print error
return
end

c
c
c
c
c
subroutine rrecxy(chx,xbuf,chy,ybuf,sr,fr,key)
c
c
c reads starting sr finishing fr: chx-->xbuf, chy-->ybuf
c if key sets ybuf=xbuf -- no chy exists
c
c
c implicit none
c integer chx,chy,nrcds,sr,fr,i
c byte xbuf(abs((fr-sr+1)*512)),ybuf(abs((fr-sr+1)*512))
c logical key
c
c call rrec(chx,xbuf,sr,fr)                    !! read x's records
c
c if (key) then                                !! key-->set y=x
c   nrcds=fr-sr+1
c   do 200 i=1,nrcds*512
c     ybuf(i)=xbuf(i)
200 else
c   call rrec(chy,ybuf,sr,fr)                !! else read y's records
c endif
c
c return
c end
c
c
c
c
c
subroutine rrec(ch,buf,sr,fr)
c
c reads fr-sr 512 byte records from ch to buf, starting at
c record sr finishing at fr
c
c implicit none
c integer sr,fr,ch,ios,i,s,j
c byte buf(abs((fr-sr+1)*512)),temp(512)
c
c
c if (sr .gt. fr) then                        !! starting record after
c   ios=999                                  !! ending record
c   goto 200
c endif
c

```

```
do 100 i=sr,fr                !! read records sr...fr
```

```
read(unit=ch,rec=i,err=200,iostat=ios)temp
```

```
s=(i-sr)*512                !! put read buffer in
do j=1,512                  !! return variable, buf
buf(j+s)=temp(j)            !! 512 bytes/record
enddo
```

```
continue
```

```
return
```

```
call prterr('rrec err',ios)  !! print errors
return
end
```

```
subroutine wrec(ch,buf,sr,fr)
```

```
writes buf to ch in 512 byte records --
starting at record sr, finishing at fr
```

```
implicit none
integer s,ch,sr,fr,ios,i,j
byte buf(abs((fr-sr+1)*512)),temp(512)
```

```
if (sr .gt. fr) then          !! starting record after
ios=999                        !! last record
go to 200
endif
```

```
do 100 i=sr,fr                !! write records sr...fr
```

```
s=(i-sr)*512
do j=1,512
temp(j)=buf(j+s)              !! fill write buffer --
enddo                          !! 512 bytes/record
```

```
write(unit=ch,rec=i,err=200,iostat=ios)temp
return
```

```
call prterr('wrec error',ios) !! print errors
return
end
```

```
terminal i/o routines
```

```

c
c
c
  subroutine otstr(str,nlf)
c
c  prints str, on the current line, followed by nlf cr/linefeeds
c
c
c  implicit none
c  integer nlf,1
c  character*(*) str
c
c  write(6,100)str          !! prints string to terminal
100  format(lh+,a,$)
c
c  if (nlf .lt. 1) return    !! prints lf's
c  do 200 l=1,nlf
c  write(6,300)
300  format(' ')
200  continue
c  return
c  end
c
c
c
c
c
  subroutine gtstr(pt,var,n)
c
c  gets a string from the terminal -- prompts w/ pt, var=string
c                                     var has length n<101
c
c  implicit none
c  character*(*) pt,var
c  integer n,i,nchrs
c  character*100 invar
c
c  i=min(len(var),index(var,' '))
c  write(6,100) pt,var          !! write prompt, default
100  format(' ',a,' (',a<i>,'):',,$)
c
c  read(5,200)nchrs,(invar(i:i),i=1,nchrs) !! read srting
200  format(q,100a1)
c
c  if (nchrs .eq. 0) return      !! return default
c  do 300 i=1,n
c  var(i:i)=' '
300  if (i .le. nchrs) var(i:i)=invar(i:i)  !! fill return variable
c  return
c  end
c
c
c
  subroutine gtint(pt,igr,mx,mn)
c
c  gets integer from terminal -- prompts user w/ pt, accepts
c                                     igr in range (mn,mx)
c
c
c

```

```

implicit none
character*10 itstr
integer igr,mx,mn,it,nchrs,i,lmn,lmx
character*(*)pt

i=2+max(1,int(log10(abs(float(igr))+.1)))
write(6,100)pt,igr          !! write prompt, default
100 format(' ',a,' (' ,i<i>,' ):',$)

200 read(5,400)nchrs,(itstr(i:i),i=1,10)    !! get string
400 format(q,10a1)

if (nchrs .eq. 0) return          !! take default if no
                                   !! entry
call s2i(it,itstr)                !! convert str-->int

if ((it .le. mx) .and. (it .ge. mn)) then    !! check range
    igr=it
    return
endif
lmn=2+max(1,int(log10(abs(floatj(mn))+.1)))
lmx=2+max(1,int(log10(abs(floatj(mx))+.1)))
write(6,300)mn,mx                !! not in range
300 format(' The (min,max)are (' ,i<lmn>,' ,i<lmx>,' ) -- reenter:',$)
go to 200
end

```

```

subroutine s2i(itr,str)

```

```

converts string -- str -- to integer -- itr.

```

```

implicit none
integer a,1
integer itr,i,j,temp,pt
character*(*) str

```

```

temp=0
pt=1
l=len(str)

```

```

do 100 i=0,l-1                    !! itr=sum(str(i)*10**i)
a=ichar(str(l-i:l-i))
if (a .eq. 48) go to 200           !! a='0'
if (a .eq. 45) go to 300           !! a='-'
if ((a .lt. 49) .or. (a .gt. 57)) go to 100 !! a not in 1--9
temp=temp+pt*(a-48)
200 pt=pt*10
100 continue
itr=temp
return

```

```

itr=-temp
return
end

```

```

c
c
c
c
c      subroutine gtrel(pt,rel,mx,mn)
c
c      gets real*4 from terminal -- prompts user w/ pt, accepts
c                                rel in range (mn,mx)
c
c
c
c      implicit none
c      character*10 rlstr
c      real*4 rel,mx,mn,rl
c      integer nchrs,i,lmx,lmn
c      character*(*)pt
c
c      write(6,100)pt,rel                !! write prompt, default
100  format(' ',a,' (' ,f<5+max(1,int(log10(abs(rel)+.1)))>.3,'):',,$)
c
c      read(5,400)nchrs,(rlstr(i:i),i=1,10)    !! get string
400  format(q,10a1)
c
c      if (nchrs .eq. 0) return            !! take default if no
c                                           !! entry
c      call s2r(rl,rlstr)                  !! convert str-->int
c
c      if ((rl .le. mx) .and. (rl .ge. mn)) then    !! check range
c          rel=rl
c          return
c      endif
c      lmx=5+max(1,int(log10(abs(mx)+.1)))
c      lmn=5+max(1,int(log10(abs(mn)+.1)))
c      write(6,300)mn,mx                    !! not in range
300  format(' The (min,max)are (' ,f<lmn>.3,' ,',f<lmx>.3,')
x      -- reenter:',,$)
c      go to 200
c      end
c
c
c
c      subroutine s2r(r,str)
c
c      converts string -- str -- to real -- r.
c
c      implicit none
c      integer a,l,i,j
c      real*4 r,temp,pt
c      character*(*) str
c
c      temp=0.
c      pt=1.
c      l=len(str)
c
c      do 100 i=0,l-1                        !! itr=sum(str(i)*10**i)
c          a=ichar(str(l-i:l-i))
c          if (a .eq. 45) go to 300            !! a='-'
c          if (a .eq. 48) go to 200            !! a='0'

```



```

if (a .eq. 46) then                                !! a='.'
    temp=temp/pt
    pt=1.
    go to 100
endif
if ((a .lt. 49) .or. (a .gt. 57)) go to 100  !! a not in 1--9
temp=temp+pt*float(a-48)
pt=pt*10.
continue
r=temp

return

r--temp

return
end

```

```

subroutine clrscrn

```

```

clears the screen

```

```

byte sbuf(4)

```

```

sbuf(1)=27 ! ESC
sbuf(2)=91 ! [
sbuf(3)=50 ! 2
sbuf(4)=74 ! J
write(6,100)(sbuf(i),i=1,4)
format(lh+,4al)

```

```

return
end

```

```

logical function gtyes(pt)

```

```

prompts user w/ pt, returns .true. if 'yes'

```

```

implicit none
character ystr
character*(*) pt

```

```

gtyes=.false.
write(6,100) pt                                !! write prompt
format(' ',a,$)
read(5,200) ystr                                !! get response
format(al)
if ((ystr .eq. 'y') .or. (ystr .eq. 'Y')) gtyes=.true.
return                                           !! true if first
end                                              !! character is y or Y

```

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```
subroutine merge ( merge_gate, rate_gate)
```

```
implicit none
```

```
real          merge_gate
```

```
real          rate_gate
```

```
integer       other_track
```

```
integer       track
```

```
include       'tracks.inc'
```

```

do track = 2, number_of_tracks

  do other_track = track - 1, 1, -1

    if ( t_frequency ( track) .lt. 0) goto 1000

    if ( t_frequency ( other_track) .lt. 0) then ! deleted track

    else if ((( t_type ( track) .eq. weak) .and.
1      ( t_type ( other_track) .eq. strong)) .or.
1      (( t_type ( track) .eq. strong) .and.
1      ( t_type ( other_track) .eq. weak))) then

    else if ( t_frequency ( track) - t_frequency ( other_track)
1      .gt. merge_gate) then

      goto 1000

    else if (( t_type ( track) .eq. edt) .and.
1      ( t_type ( other_track) .eq. edt)) then

      if (( t_age ( track) .eq. 1) .or.
1      ( t_age ( other_track) .eq. 1)) then

        call domerg ( track, other_track)

      else if ( abs ( t_frequency_rate ( track) -
1      t_frequency_rate ( other_track)) .le. rate_gate) then

        call domerg ( track, other_track)

      end if

    else

      call domerg ( track, other_track)

    end if

  end do

end do

1000  continue

end do

call compress

end

subroutine newtra ( fft_amplitude, fft_associated, max_fft_bin_number,
1  threshold)

implicit none

real          fft_amplitude ( 1)
logical*1     fft_associated ( 1)
integer       max_fft_bin_number
real          threshold ( 1)

```

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integer	bin
logical*1	looking_for_downslope
include	'tracks.inc'

```
looking_for_downslope = .false.

do bin = 1, max_fft_bin_number - 1
  if ( fft_amplitude ( bin) - fft_amplitude ( bin + 1) .gt. 0)
1    then
      if ( looking_for_downslope) then
          if ( fft_amplitude ( bin) .lt. threshold ( weak)) then
              else if ( fft_associated ( bin)) then
                  else if ( fft_amplitude ( bin) .gt. threshold ( strong))
1                    then
                        call maktra ( bin, fft_amplitude ( bin), strong)
                    else
                        call maktra ( bin, fft_amplitude ( bin), weak)
                    end if
                end if
            end if
        else
            looking_for_downslope = .true.
        end if
    end do
  call compress
end
subroutine smooth ( dynamic_tracking_threshold, faca, alpha, beta,
1  max_fft_bin_number)

implicit none

real          alpha ( 0:*)
real          beta ( 0:*)
real          dynamic_tracking_threshold
real          faca
integer       max_fft_bin_number

integer       i
integer       track

include       'tracks.inc'
```

```

do track = 1, number_of_tracks

    i = faca * t_adaptive_amplitude ( track)

    if ( i .lt. 0) then
        i = 0
    else if ( i .gt. 31) then
        i = 31
    end if

    if ( t_dcell ( track) .ne. 0) then
        t_frequency ( track) = t_frequency ( track) +
1         alpha ( i) * t_dcell ( track)

        if ( t_adaptive_amplitude ( track) .ge.
1         dynamic_tracking_threshold) then

            t_frequency_rate ( track) = t_frequency_rate ( track) +
1            beta ( i) * t_dcell ( track)
        end if
    end if

    t_frequency (track) = t_frequency ( track) +
1    t_frequency_rate ( track)

    if (( t_frequency ( track) .gt. max_fft_bin_number) .or.
1    (t_frequency ( track) .lt. 1.)) call deltra ( track)

end do

call compress

end
subroutine sort

implicit none

integer      track1
integer      track2

include      'tracks.inc'

do track1 = 1, number_of_tracks - 1
    do track2 = track1 + 1, number_of_tracks

        if ( t_frequency ( track1) .gt. t_frequency ( track2)) then

            call swap_real ( t_adaptive_amplitude ( track1),
1            t_adaptive_amplitude ( track2))

            call swap_integer ( t_age ( track1), t_age ( track2))

            call swap_real ( t_associated_amplitude ( track1),
1            t_associated_amplitude ( track2))

            call swap_real ( t_associated_cell ( track1),
1            t_associated_cell ( track2))

```

```
      call swap_real ( t_dcell ( track1), t_dcell ( track2))

      call swap_logical ( t_detection_flag ( track1),
1         t_detection_flag ( track2))

      call swap_real ( t_frequency ( track1),
1         t_frequency ( track2))

      call swap_real ( t_frequency_rate ( track1),
1         t_frequency_rate ( track2))

      call swap_integer ( t_id ( track1), t_id ( track2))

      call swap_real ( t_log_likelihood ( track1),
1         t_log_likelihood ( track2))

      call swap_integer ( t_type ( track1), t_type ( track2))

    end if

  end do

end do

end
```



```
subroutine swap_real ( x, y)
```

```
real    x
```

```
real    y
```

```
real    z
```

```
z = x
```

```
x = y
```

```
y = z
```

```
end
```

```
subroutine swap_integer ( x, y)
```

```
integer x
```

```
integer y
```

```
integer z
```

```
z = x
```

```
x = y
```

```
y = z
```

```
end
```

```
subroutine swap_logical1 ( x, y)
```

```
logical*1    x
```

```
logical*1    y
```

```
logical*1    z
```

```
z = x
```

```
x = y
```

```
y = z
```

```
end
```

```
subroutine update ( amplitude_smoothing_constant, detection_threshold,  
1    display_threshold, drop_threshold, log_likelihood_max)
```

```
implicit none
```

```
real          amplitude_smoothing_constant
```

```
real          detection_threshold
```

```
real          display_threshold
```

```
real          drop_threshold
```

```
real          log_likelihood_max
```

```
real          log_likelihood_ratio
```

```
real          tll
```

```
real          temp_real
```

```
integer       track
```

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include 'tracks.inc'

```

do track = 1, number_of_tracks

    t_log_likelihood ( track) = t_log_likelihood ( track) +
1      log_likelihood_ratio ( t_type ( track),
1      t_associated_amplitude ( track))

    t_log_likelihood ( track) =
1      min ( t_log_likelihood ( track) , log_likelihood_max)

    tll = t_log_likelihood ( track)

    if ( tll .le. drop_threshold) then

        call deltra ( track)

    else if ( tll .lt. display_threshold) then

        t_detection_flag ( track) = .false.
        if ( t_type ( track) .eq. edt)
1          t_age ( track) = t_age ( track) + 1

    else if ( tll .lt. detection_threshold) then

        if ( t_detection_flag ( track)) then

            t_age ( track) = t_age ( track) + 1

        else

            if ( t_type ( track) .eq. edt)
1              t_age ( track) = t_age ( track) + 1

        end if

    else

        if ( t_type ( track) .eq. edt) then

            t_detection_flag ( track) = .true.
            t_age ( track) = t_age ( track) + 1

        else

            t_type ( track) = edt
            t_age ( track) = 1
            t_detection_flag ( track) = .true.

        end if

    end if

    temp_real = t_associated_amplitude ( track) -
1      t_adaptive_amplitude ( track)

```

```
t_adaptive_amplitude ( track) = t_adaptive_amplitude ( track) +
1    temp_real / amplitude_smoothing_constant
```

```
end do
```

```
end
```

```
subroutine writestuff ( k, fft_amplitudes,thr,pct,nop,fnam)
```

```
writestuff calculates and displays several track parameters
```

```
declarations
```

```
implicit none
```

```
real          fft_amplitudes(512),level
```

```
real          thr,pct,dif
```

```
integer*4     fl,fh,nom,noh,nmr,i,j,k,lun,nop
```

```
include       'tracks.inc'
```

```
character*80   fnam
```

```
set up output file if k=1
```

```
if (k.eq.1) then
```

```
    lun=1
```

```
    open(unit=lun,file=fnam,status='new',carriagecontrol='list')
```

```
endif
```

```
calculate average signal+noise level
```

```
level=0.
```

```
do i=1,512
```

```
level=level+fft_amplitudes(i)
```

```
enddo
```

```
level=level/512.
```

```
print header
```

```
type 1000, k, number_of_tracks
```

```
C1000 format ( /'0Track table dump at line ',i3, ' contains ' i3,
1    ' tracks.'/)
```

```
type 1005
```

```
C1005 format ( ' track det   freq   freq   amp   ass   ass   fl'
1    '      fh   diff level' /
1    '      #           rate           freq   amp' /)
```

```
if (number_of_tracks.ge.1) write(lun,891) k  
format('(',i4)
```

```
main loop
```

```
do 100 i = 1, number_of_tracks
```

```
find fl,fh,diffusion
```

```
fh first
```

```
j=t_associated_cell(i)
```

```
nmr=0
```

```
noh=1
```

```
nom=0
```

```
j=j+1
```

```
if (fft_amplitudes(j).ge.thr*level) then
```

```
noh=noh+1
```

```
nmr=0
```

```
else
```

```
nom=nom+1
```

```
nmr=nmr+1
```

```
if ((nmr.ge.2).and.(pct.ge.(float(noh)/float(noh+nom))))
```

```
go to 777
```

```
endif
```

```
go to 776
```

```
continue
```

```
j=j-1
```

```
if ((fft_amplitudes(j).lt.thr*level).and.(j.ne.t_associated_cell(i)))
```

```
go to 777
```

```
fh=j
```

```
do fl
```

```
j=t_associated_cell(i)
```

```
nmr=0
```

```
noh=1
```

```
nom=0
```

```
j=j-1
```

```
if (fft_amplitudes(j).ge.thr*level) then
```

```
noh=noh+1
```

```
nmr=0
```

```
else
```

```
nom=nom+1
```

```
nmr=nmr+1
```

```
if ((nmr.ge.2).and.(pct.ge.(float(noh)/float(noh+nom))))
```

```
go to 779
```

```
endif
```

```
go to 778
```

```
continue
```

```

      j=j+1
      if ((fft_amplitudes(j).lt.thr*level).and.(j.ne.t_associated_cell(i)))
x      go to 779
      fl=j

c
c
c      find diffusion
c
c
      dif=0
      do j=fl,fh
      dif=fft_amplitudes(j)+dif
      enddo
      dif=dif/(float(fh-fl+1))

C      type 1001, i,
C      1      t_detection_flag ( i),
C      1      t_frequency ( i),
C      1      t_frequency_rate(i),
C      1      t_adaptive_amplitude (i),
C      1      t_associated_cell ( i),
C      1      t_associated_amplitude ( i),
C      1      fl,
C      1      fh,
C      1      dif,
C      1      level
C
C1001      format ( i4,15,f8.2,f8.2,f7.2,f8.0,f8.2,i7,i7,f7.2,f7.2)
c
c
c
c      write stuff to output file
c

      write(lun,889) t_detection_flag ( i),
      1      t_frequency ( i),
      1      t_frequency_rate(i),
      1      t_adaptive_amplitude (i),
      1      t_associated_cell ( i),
      1      t_associated_amplitude ( i),
      1      fl,
      1      fh,
      1      dif,
      1      level
889      format ( '(' ,15,f8.2,f8.2,f7.2,f8.0,f8.2,i7,i7,f7.2,f7.2,')')

c
c
c
c
c
c100      continue
c

      if (number_of_tracks.ge.1) write(lun,890)
890      format('')
c
c

```

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close output file

if (j.eq.nop) close(unit=lun,status='keep')

end

c JHJLIB.INC

```
integer*4      ap_max_address
parameter      ( ap_max_address = 16383 )

integer*4      array_processor
parameter      ( array_processor = 2 )

integer*4      askflt_l
parameter      ( askflt_l = 1 )

integer*4      askflt_luv
parameter      ( askflt_luv = 7 )

integer*4      askflt_lv
parameter      ( askflt_lv = 5 )

integer*4      askflt_lu
parameter      ( askflt_lu = 3 )

integer*4      askflt_nodfault
parameter      ( askflt_nodfault = 0 )

integer*4      askflt_u
parameter      ( askflt_u = 2 )

integer*4      askflt_uv
parameter      ( askflt_uv = 6 )

integer*4      askflt_v
parameter      ( askflt_v = 4 )

integer*4      askint_l
parameter      ( askint_l = 1 )

integer*4      askint_luv
parameter      ( askint_luv = 7 )

integer*4      askint_lv
parameter      ( askint_lv = 5 )

integer*4      askint_lu
parameter      ( askint_lu = 3 )

integer*4      askint_nodfault
parameter      ( askint_nodfault = 0 )

integer*4      askint_u
parameter      ( askint_u = 2 )

integer*4      askint_uv
parameter      ( askint_uv = 6 )

integer*4      askint_v
parameter      ( askint_v = 4 )

integer*4      complex_floating
parameter      ( complex_floating = 3 )
```



```
integer*4      complex_integer
parameter      ( complex_integer = 4 )

integer*4      memory
parameter      ( memory = 1 )

integer*4      read_access
parameter      ( read_access = 1 )

integer*4      real_floating
parameter      ( real_floating = 1 )

integer*4      real_integer
parameter      ( real_integer = 2 )

integer*4      write_access
parameter      ( write_access = 2 )

real           amplitude_smoothing_constant
real           association_gate_min ( 3)
real           association_gate_max
real           association_gate_slope ( 3)
real           association_threshold
real           detection_threshold
real           display_threshold
real           drop_threshold
real           dynamic_tracking_threshold
real           faca
real           log_likelihood_max
integer        max_fft_bin_number
real           merge_gate
real           new_track_threshold ( 3)
real           rate_gate
```

```
common / param /
1      amplitude_smoothing_constant,
1      association_gate_min,
1      association_gate_max,
1      association_gate_slope,
1      association_threshold,
1      detection_threshold,
1      display_threshold,
1      drop_threshold,
1      dynamic_tracking_threshold,
1      faca,
1      log_likelihood_max,
1      max_fft_bin_number,
1      merge_gate,
1      new_track_threshold,
1      rate_gate
```

tracks.inc

```
integer        edt
parameter      ( edt = 3)
integer        max_tracks
parameter      ( max_tracks = 400)
```

```
integer      strong
parameter    ( strong = 2)
integer      weak
parameter    ( weak = 1)

integer      free_entry
integer      number_of_tracks
real         t_adaptive_amplitude ( max_tracks)
integer      t_age ( max_tracks)
real         t_associated_amplitude ( max_tracks)
real         t_associated_cell ( max_tracks)
real         t_dcell ( max_tracks)
logical*1    t_detection_flag ( max_tracks)
real         t_frequency ( max_tracks)
real         t_frequency_rate ( max_tracks)
integer      t_id ( max_tracks)
real         t_log_likelihood ( max_tracks)
integer      t_type ( max_tracks)
```

common / tracks/

```
1  free_entry,
1  number_of_tracks,
1  t_adaptive_amplitude,
1  t_age,
1  t_associated_amplitude,
1  t_associated_cell,
1  t_dcell,
1  t_detection_flag,
1  t_frequency ,
1  t_frequency_rate,
1  t_id,
1  t_log_likelihood,
1  t_type
```

8.0	amplitude_smoothing_constant
3.0	association_gate_min
3.0	association_gate_max
0.0	association_gate_slope (weak)
0.5	association_gate_slope (strong)
0.5	association_gate_slope (edt)
2.25	association_threshold
0.5	old_track_pd
1e-4	old_track_pfa
0.0	delta_display_threshold_from_detection_threshold
2.25	dynamic_tracking_threshold
4.0	faca
10.017	log_likelihood_max
512	max_fft_bin_number
5.0	merge_gate
0.5	rate_gate
0.03	new_track_pfa

END

Dtic

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